

Passivity Control for Hybrid Simulations of Satellite Docking

Rainer Krenn, Klaus Landzettel, Toralf Boge, Melak Zebenay

Institute of Robotics and Mechatronics & German Space Operations Center
German Aerospace Center (DLR), Oberpfaffenhofen, D-82234 Wessling

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Contents of Workshop Contribution

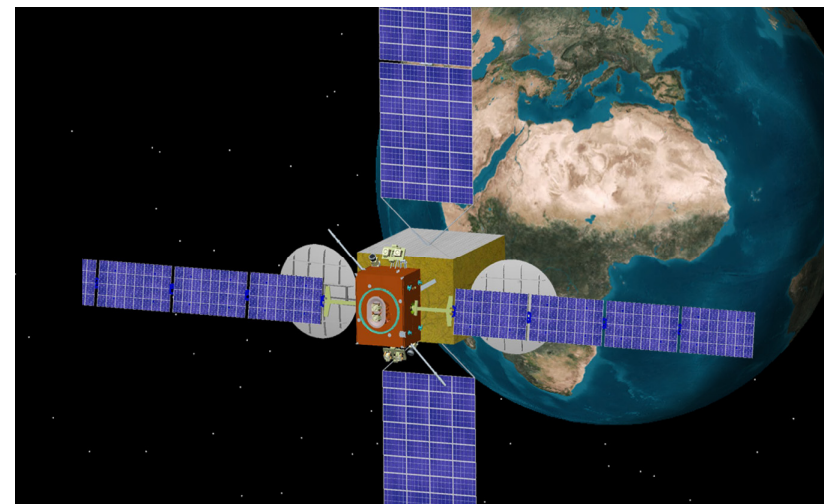
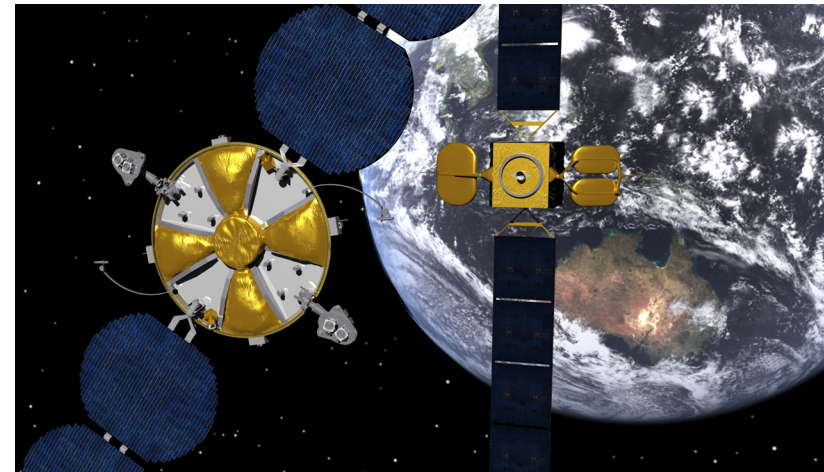
Simulation activities in the context of On-Orbit Servicing
Focus: Contact dynamics simulation

- On-orbit servicing projects and contributions
 - CX-OLEV & Smart-OLEV
- Modeling and simulation in software
 - Contact dynamics modeling
 - Docking simulation results
- Hybrid simulation using EPOS RvD facility
 - Introduction of hybrid simulation method
 - Introduction of EPOS facility
 - Contact dynamics simulation with EPOS
 - Numerical stability aspects
 - Passivity control

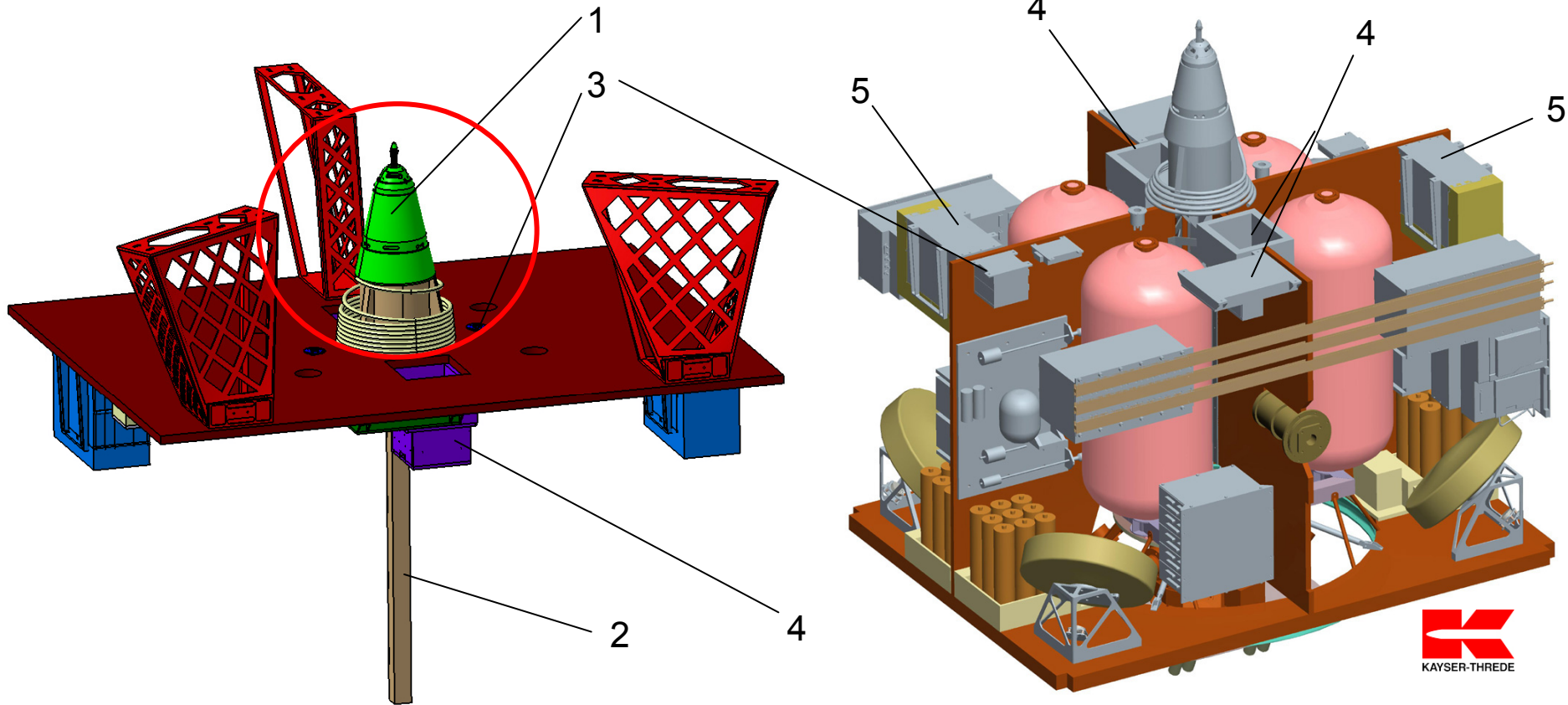


On-Orbit Servicing Projects – OLEV Type Missions (Orbital Live Extension Vehicle)

- Projects involved:
 - CX-OLEV (ESA, Dutch Space & contractors)
 - Smart-OLEV (Kayser-Threde, SSC, Sener & contractors)
- Clients: Telecom satellites in GEO
- Objectives: Offer commercial services
 - Satellite operators (Eutelsat, Optus)
 - Satellite live extension
 - Fleet management
- DLR contributions
 - Robotic docking tool (Capture Tool)
 - Rendezvous and docking control algorithms (image processing)
 - Docking simulations (S/W)



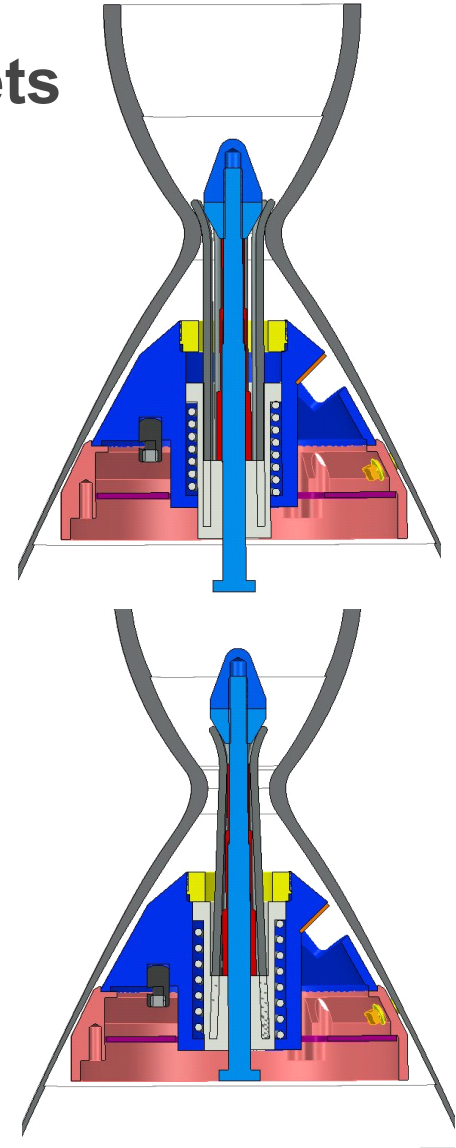
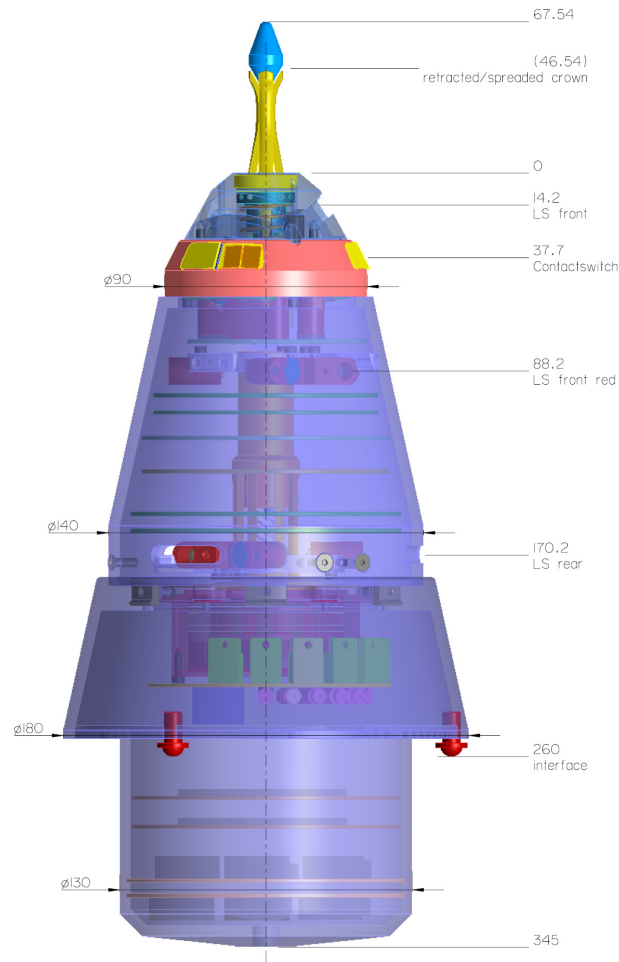
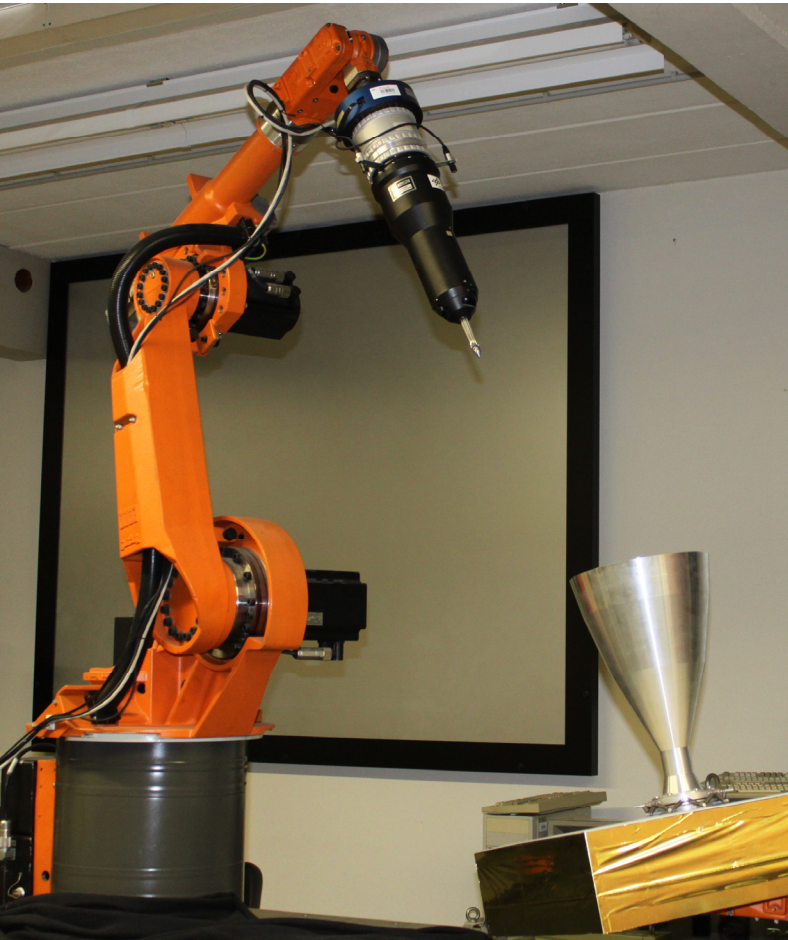
OLEV Servicing Satellite & Docking Payload (Smart)



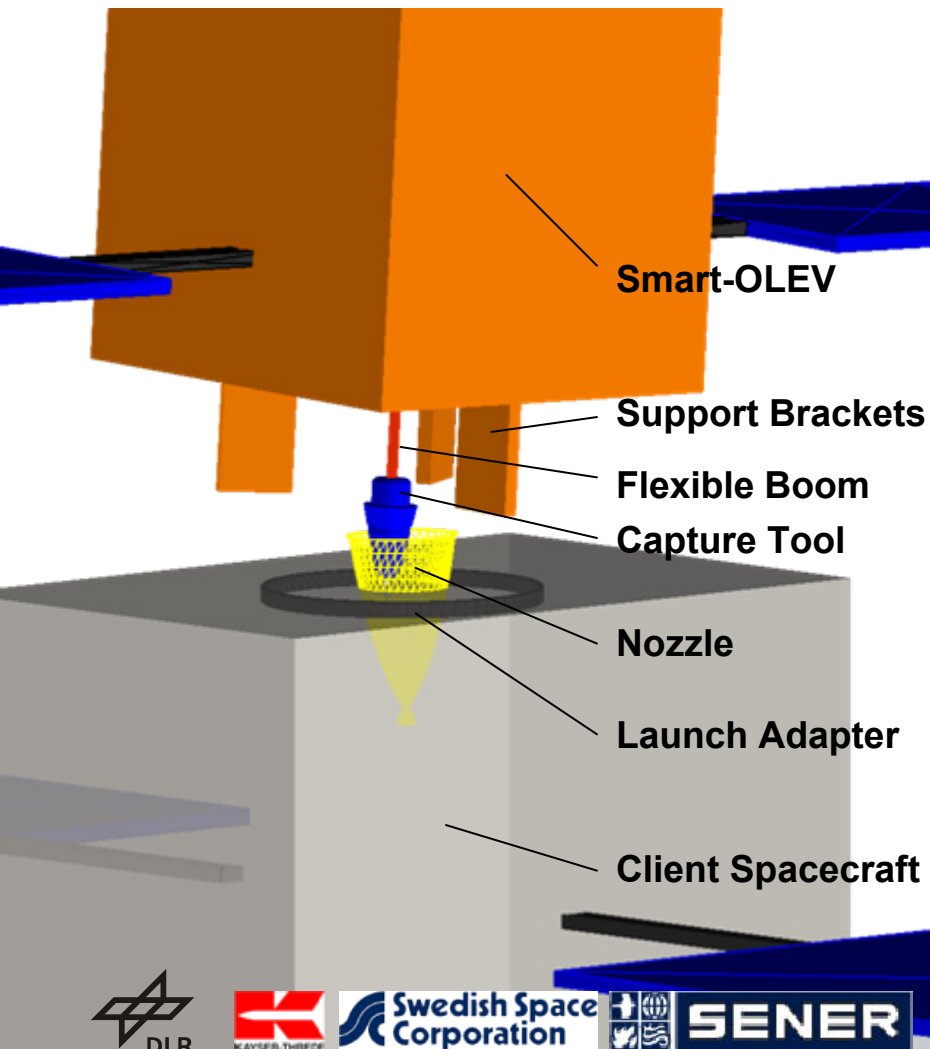
- 1) Capture Tool (CT)
- 2) CT Deployment Mechanism (CDM)
- 3) Target Illumination System (TIS) (2x)

- 4) Camera System (Far-, Mid-, Near-Range Cameras with Electronics) (2x)
- 5) Docking Payload Control Unit (2x)

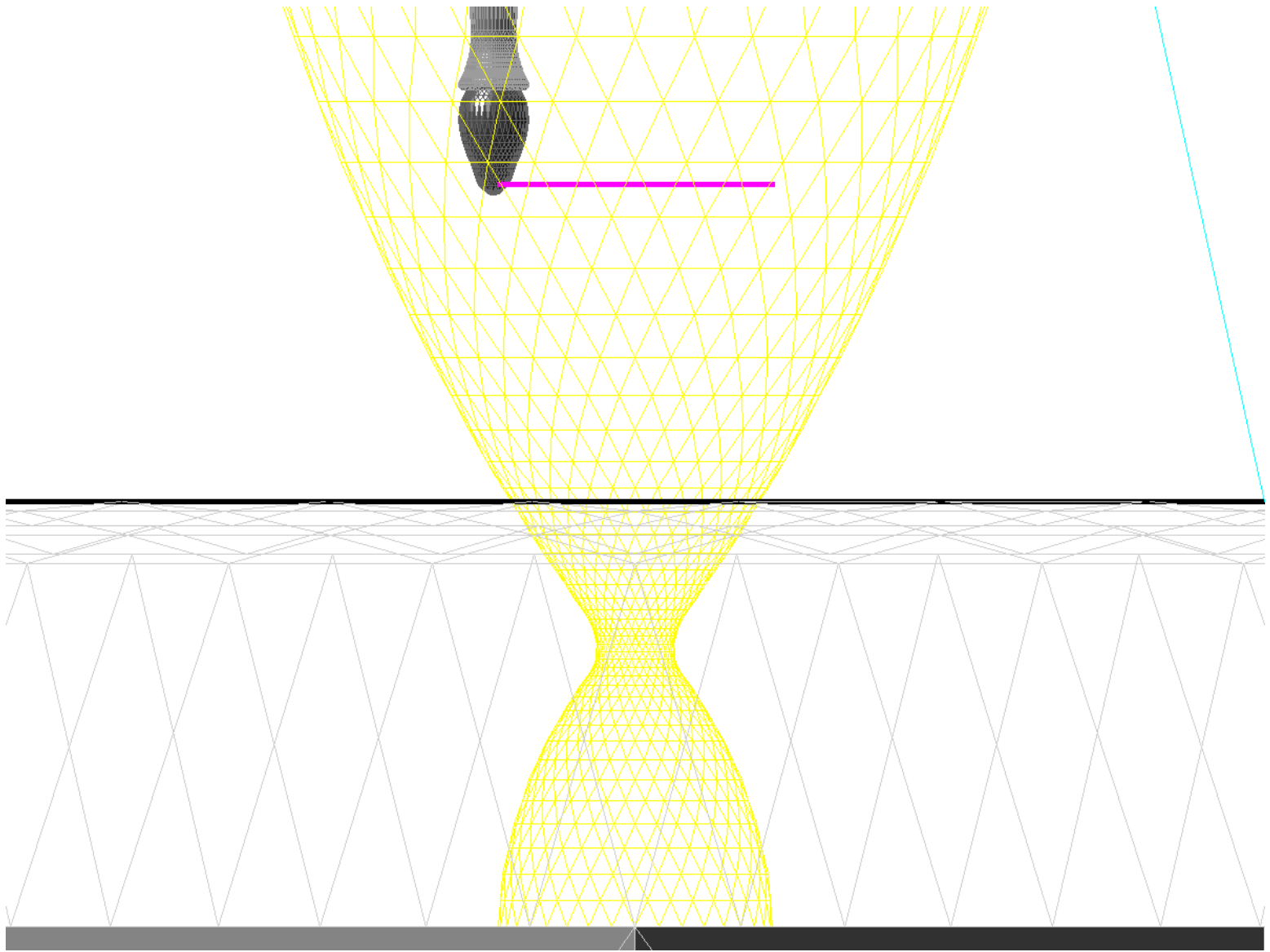
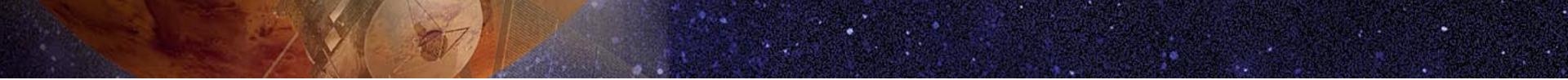
Capture Tool for Non-Cooperative Targets



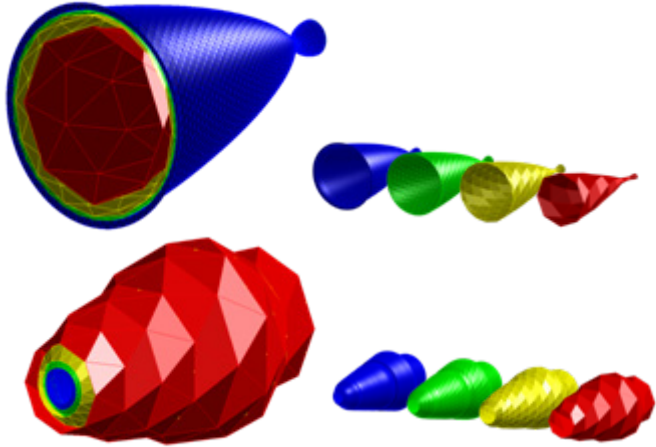
Docking Scenario for Multi-Body System Simulation



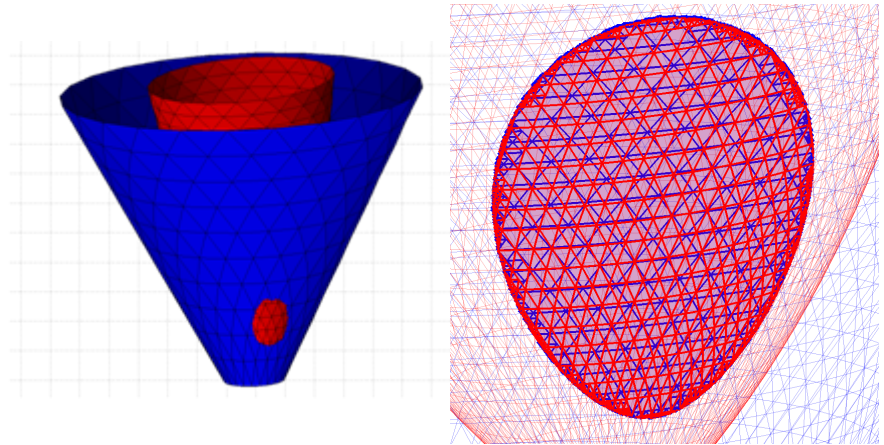
- Client
 - Hot Bird series, with flexible solar wings
 - Orbit: GEO
 - AOCS deactivated, momentum wheels loaded
 - Aerojet/Marquardt R4D nozzle, **slightly tilted**
 - 1194 mm launch adapter
- Smart-OLEV
 - Orbit: GEO + 2.178 m (R-bar)
 - AOCS active
 - 75 mm **lateral misalignment**,
2° **attitude error** in all axes
- Flexible Capture Tool deployment mechanism
 - $|v| \leq 4$ mm/s deployment/retraction velocity
- Capture Tool
 - Radial laser distance sensor
 - Contact switches
 - Operational Locking Crown
- Contact sensitive bodies:
 - Nozzle vs. Capture Tool + Locking Crown
 - Launch adapter vs. Client Support Brackets



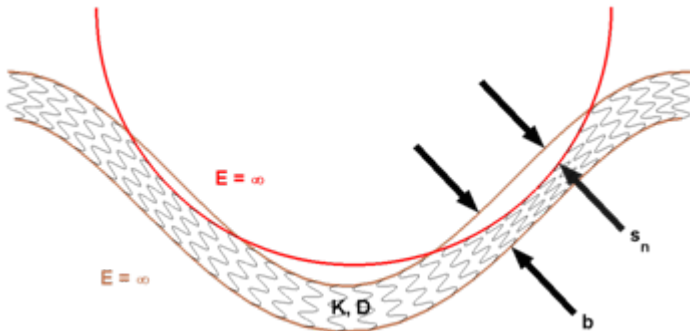
Contact Dynamics Model (3D, Multi-Point)



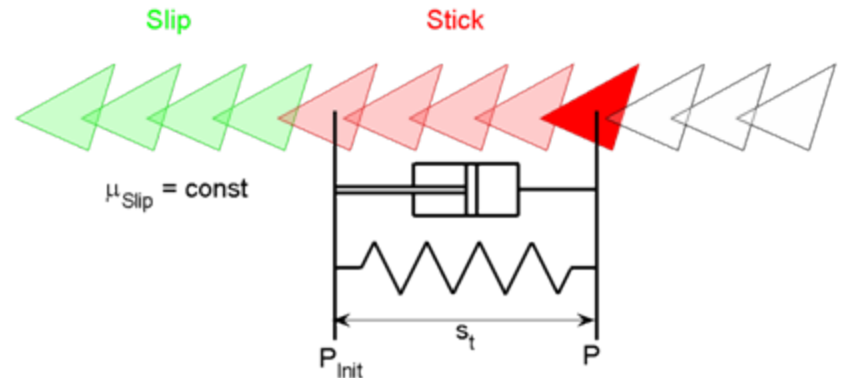
- Surface meshing
- Bounding volume tree generation



- Contact area detection algorithm

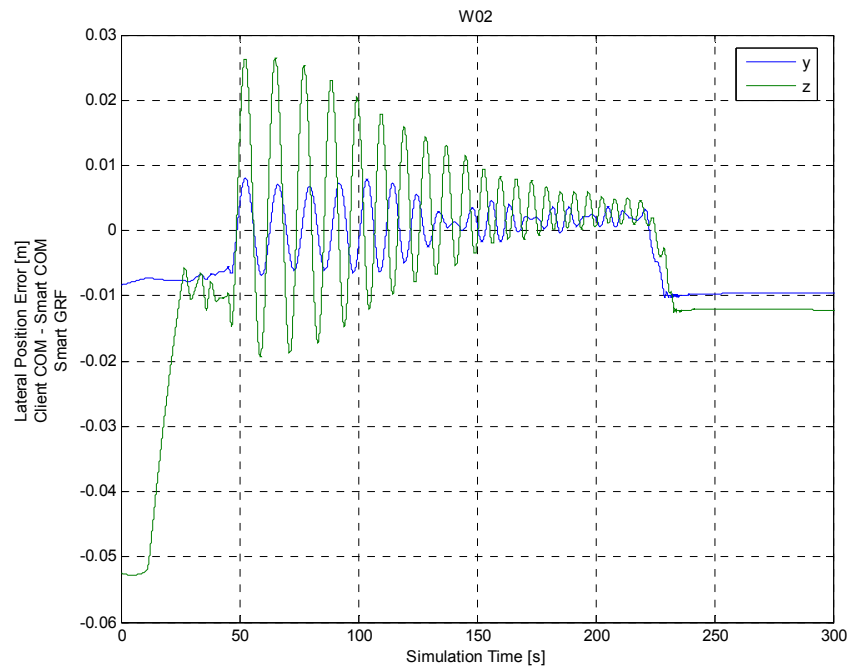
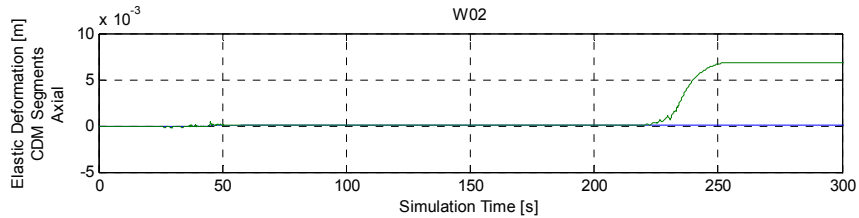
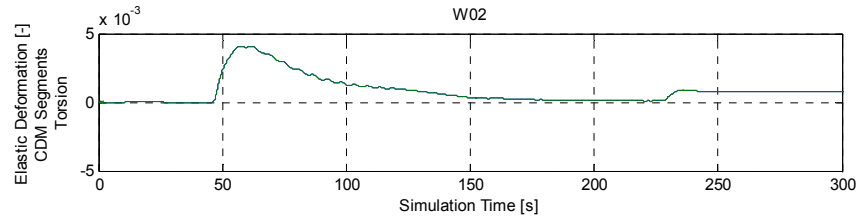
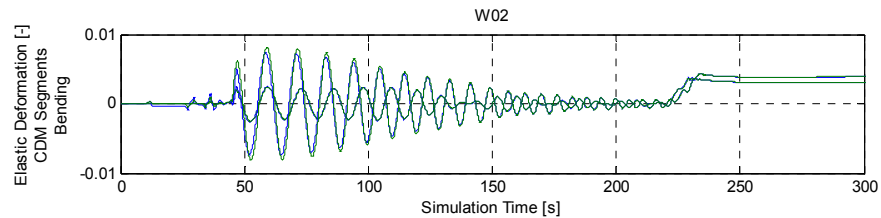
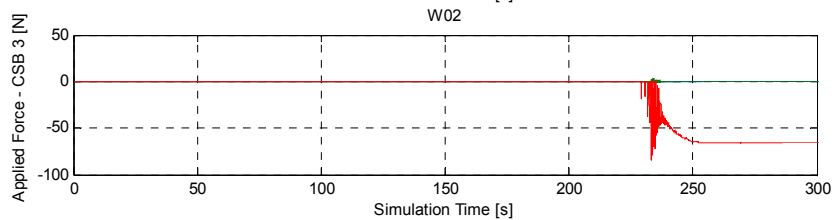
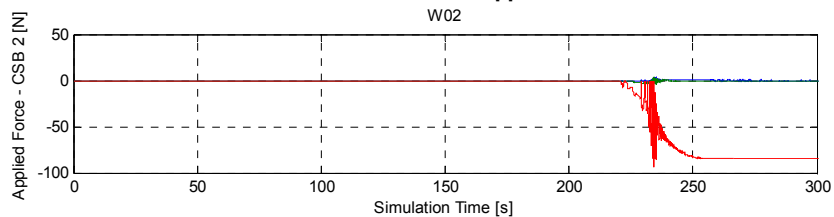
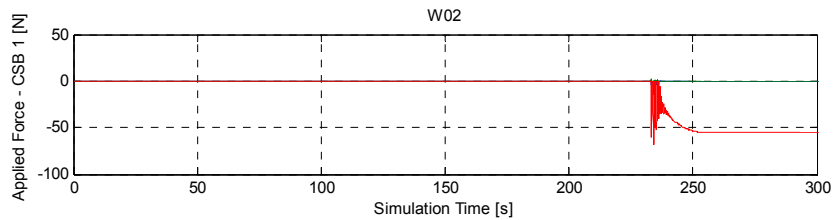
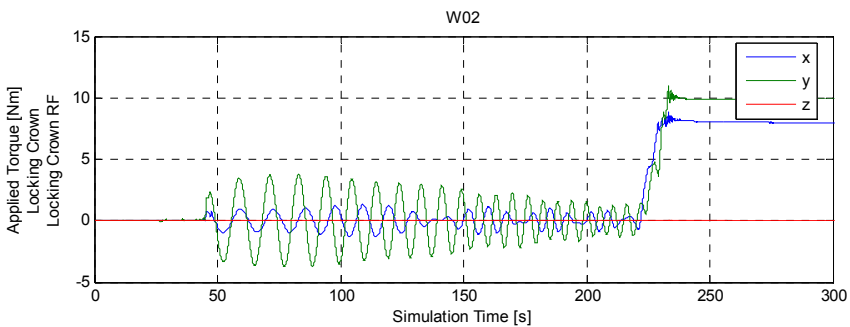
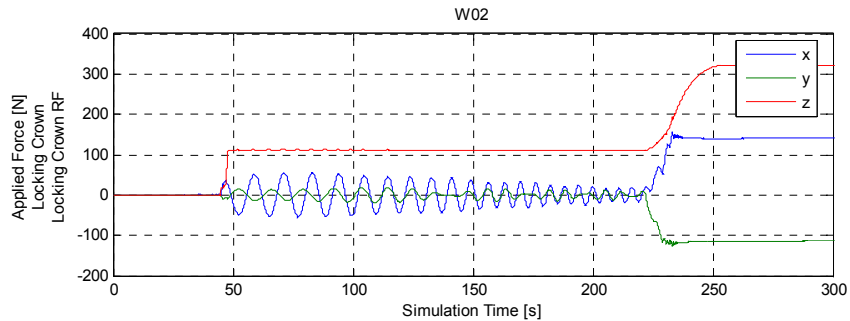


- Elastic foundation model for contact force computation



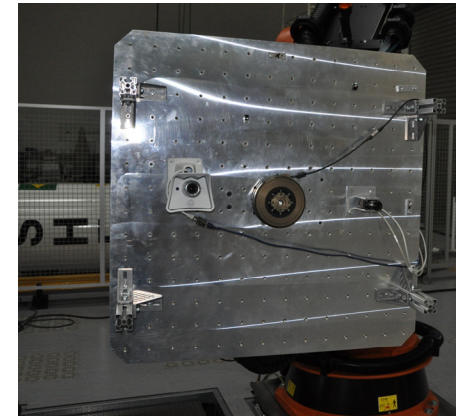
- Friction model with stick-slip





Hybrid Simulation Method

1. Numerical simulation of satellite trajectory (S/W)
 - Free floating dynamics of satellites, 6 DOF
 - Micro-gravity / 0-gravity conditions
 - Large flexible structures, solar panels
 - Momentum wheels, reaction wheels, thrusters
2. Physical-mechanical display of computed trajectory using industrial robots
 - Attachment of satellite mockups
 - Perform physical contact (capture tool, nozzle)
 - Use of missions specific mechanisms, actuators and sensors (capture tool, GNC-sensors)
3. Sensor data feedback from facility specific sensors
 - Robot joint sensors → actual trajectory
 - Force torque sensors → contact dynamics purposes



Hybrid Simulation Facility

EPOS (European Proximity Operations Simulator)

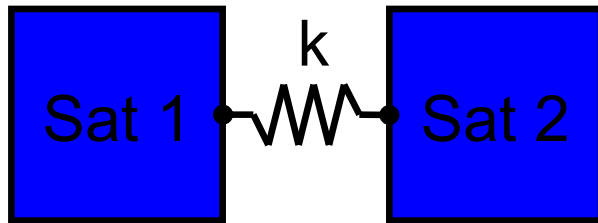
1. Development system for dynamics models: Matlab/Simulink
Real-time target for numerical simulation: VxWorks
2. Robotic system for trajectory emulation: (Kuka, RSI, position controlled)
3. Force/torque sensor feedback: Schunk/DLR FTS (“Compliance”)



EPOS has a long history as open-loop satellite rendezvous simulator (ATV sensor verification).

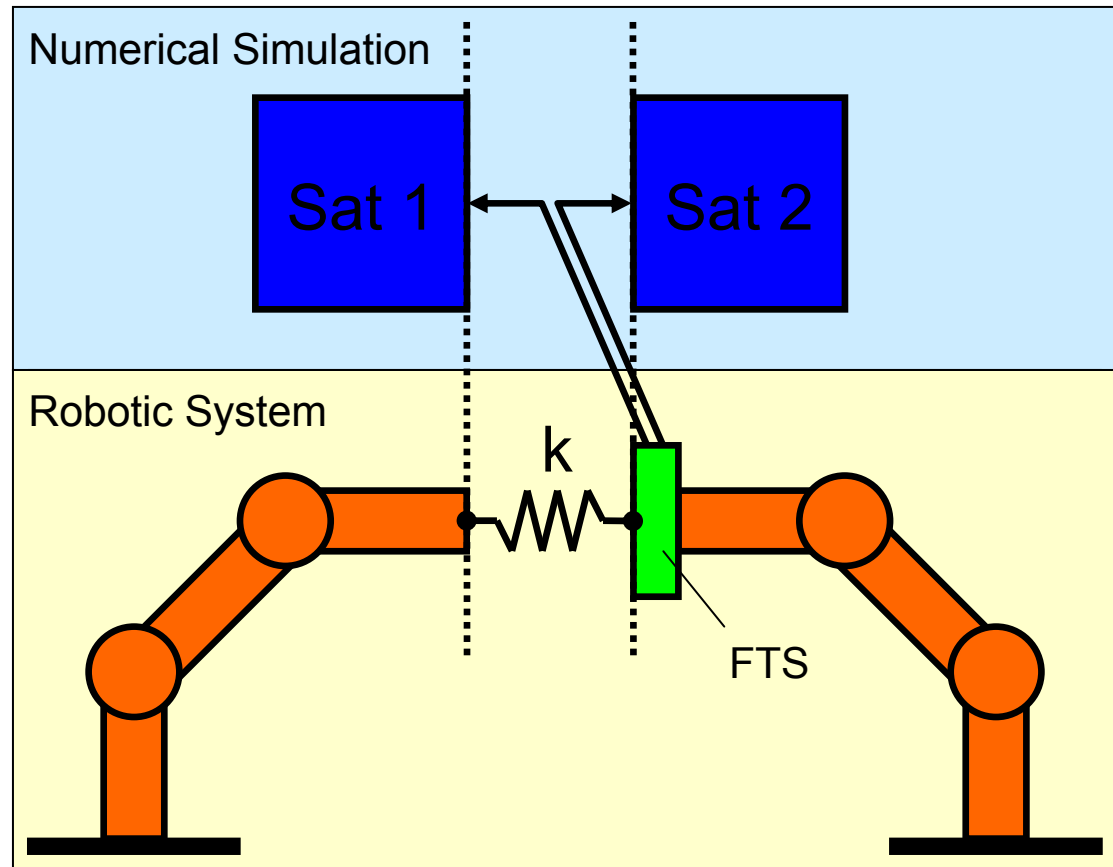
But: Is EPOS applicable for closed-loop contact dynamics simulations?

Hybrid Simulation of Docked Configuration



System to be simulated
“Ideal System”

- Free floating rigid bodies
- Spring at natural length
- $v = 0$

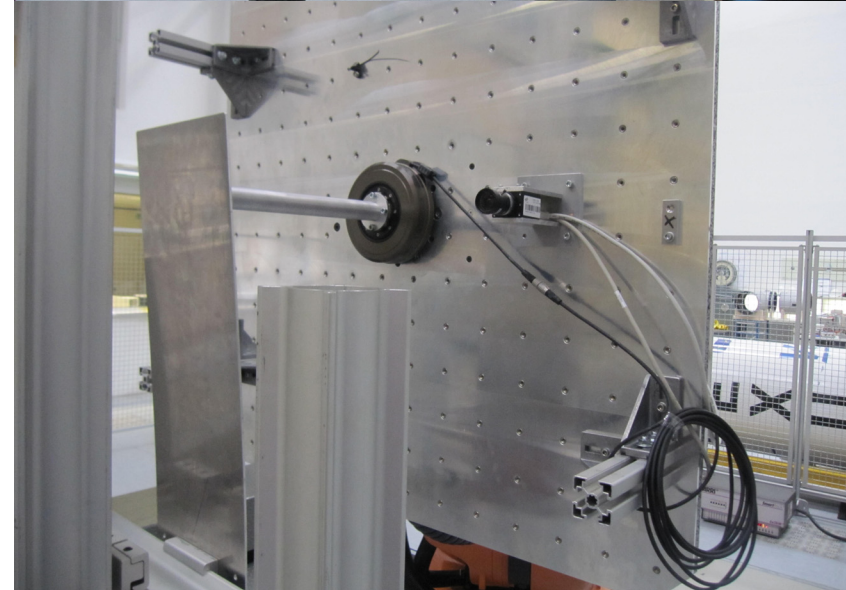


Hybrid simulation setup

Experimental Setup “Docked Configuration”

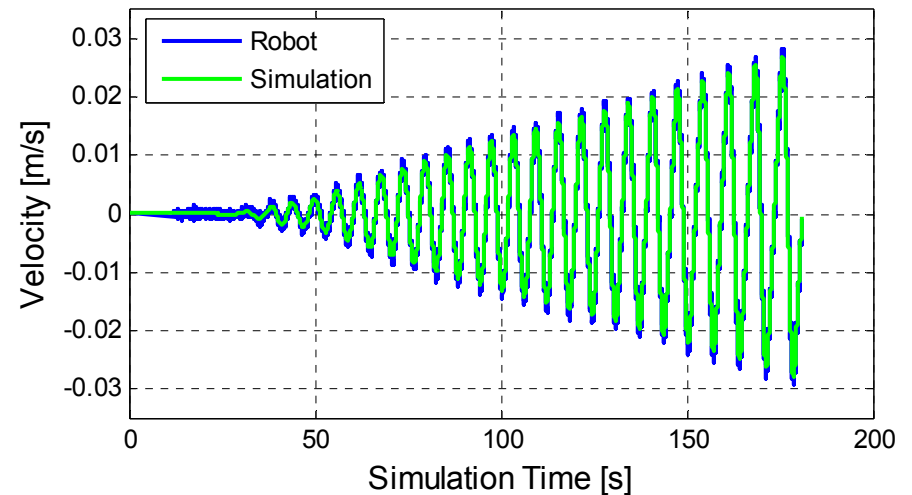
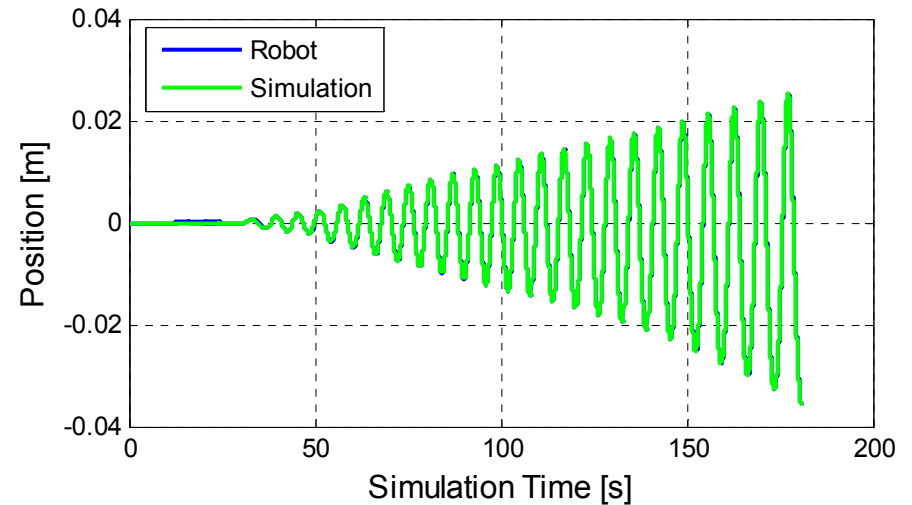
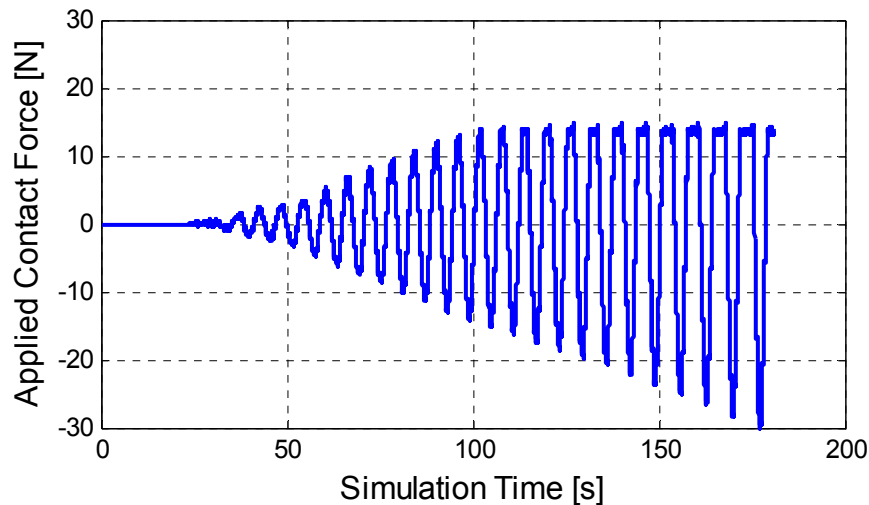
- Simulating the elastically fixed configuration (1 DOF) using single robot and one-end supported aluminum sheet metal
 1. Open hybrid simulation loop
 2. Initial robot/satellite position with bent beam
 3. Sensor calibration/reset ($F = 0$)
 4. Close hybrid simulation loop again

- Easy mechanical setup
- Nearly linear stiffness and low damping
- Easy stiffness adaptation by changing contact point distance from support point (1500 N/m ... 3000 N/m)
- Low risk of mechanical damage during experiment

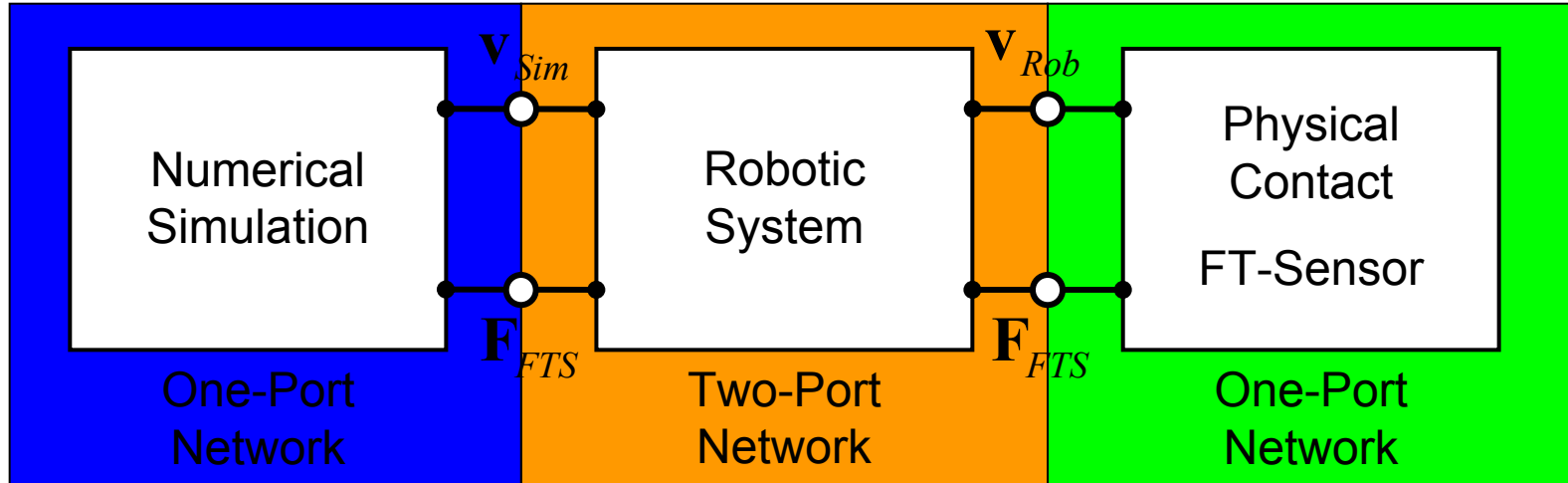


Observations

- Expected: Stationary system at rest
- Observed: Unstable system
 - Oscillating system
 - Increasing amplitudes



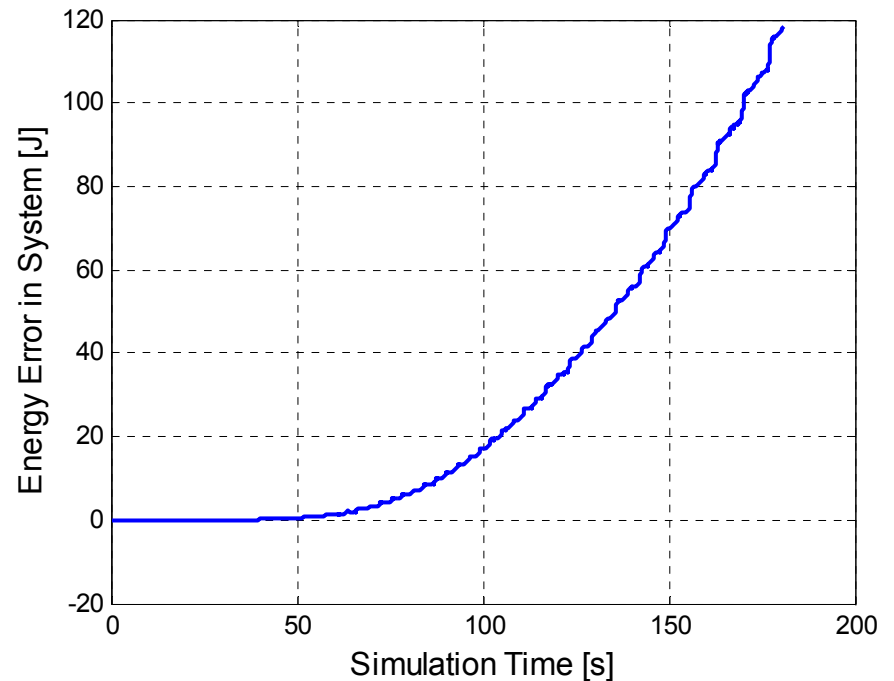
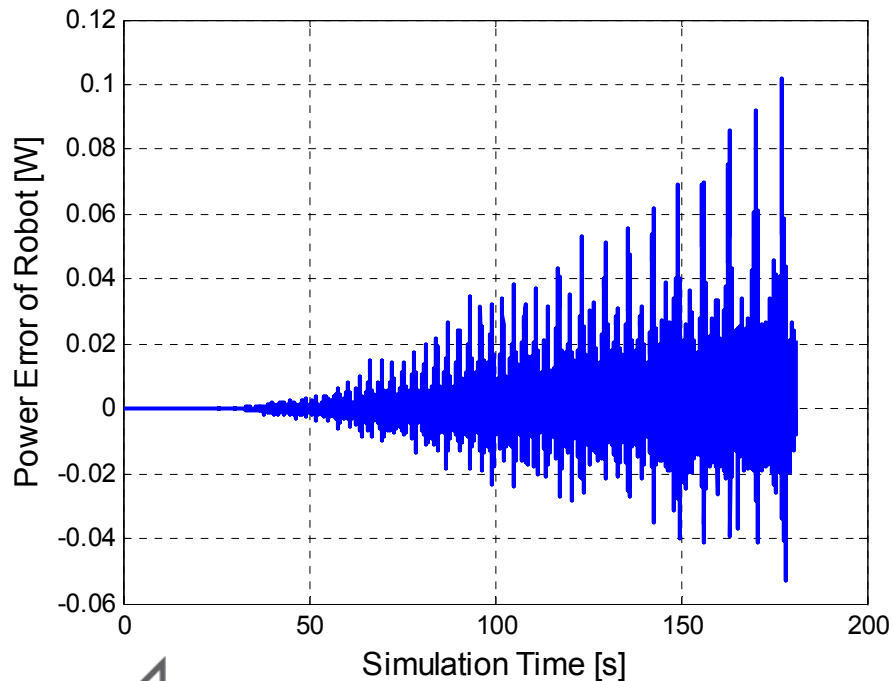
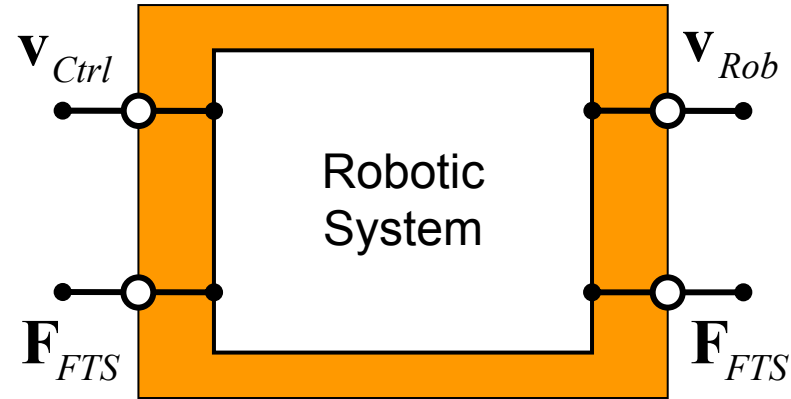
Sources of Excitation? --- Active Elements?



- Simulation sampling rate not adequate for system dynamics?
 - 250 Hz \gg eigen-frequency of contact dynamics problem
- Force-Torque sensor errors and noise?
 - Calibration error may cause change of static equilibrium position
 - Mean of noise is zero
 - But: May initiate system instability if active elements are in the loop
- Passivity of robot system to be investigated

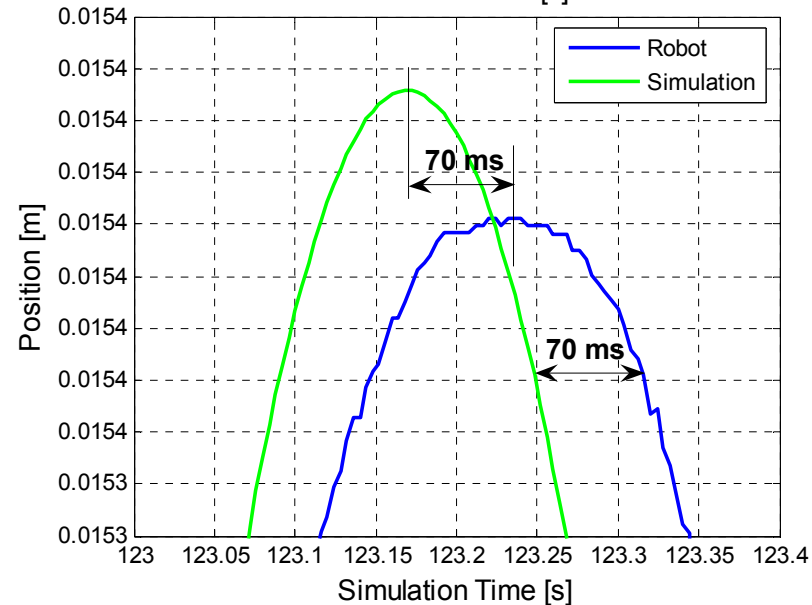
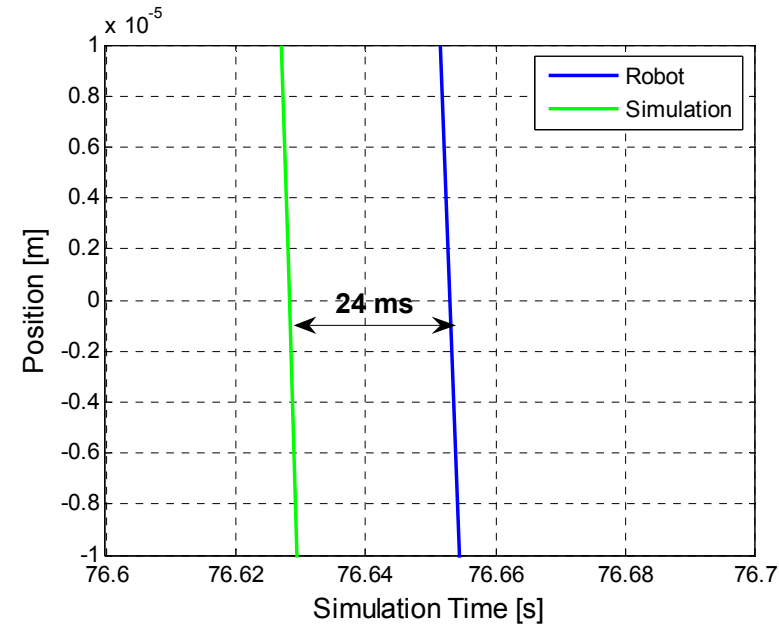
Observed Energy Error

$$\begin{aligned}
 E_{Error} &= dt \sum_{i=0}^k P_{out}(t_i) - P_{in}(t_i) \\
 &= dt \sum_{i=0}^k F_{FTS}(t_i)(v_{Rob}(t_i) - v_{Ctrl}(t_i))
 \end{aligned}$$



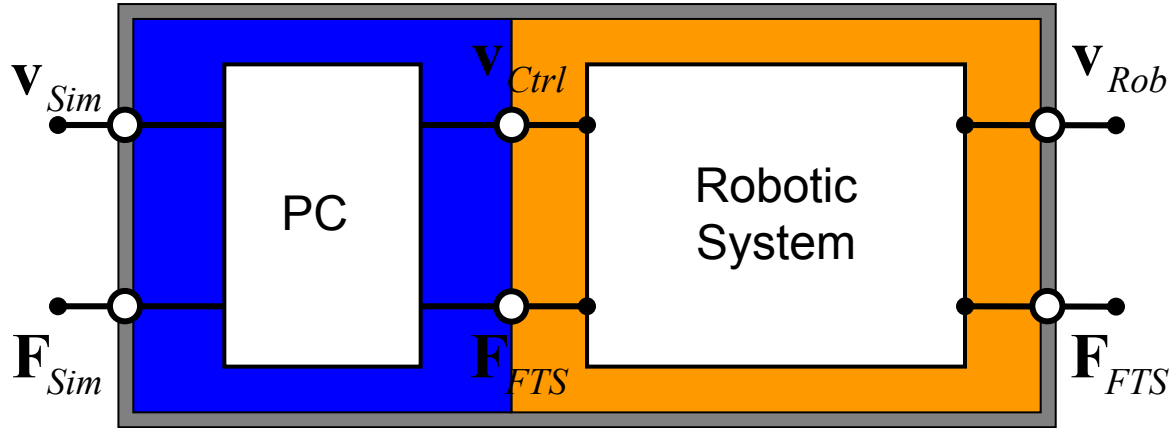
Transfer Function of Robot System

- Electro-mechanical system
 - Amplitude response of robot arm
 - Phase response of robot arm
- Robot control system with preprocessing of external commands
 - Latency
 - Smoothing of input signals



Passivity Control

- Dissipate energy error
- Maintain system dynamics



Impedance causality:

$$F_{Sim}(t_i) = F_{FTS}(t_i) - \alpha(t_i)v_{Sim}(t_{i-1}); \quad \alpha(t_i) = \begin{cases} k_v E_{Error}(t_{i-1}); & E_{Error}(t_{i-1}) > 0 \\ 0; & E_{Error}(t_{i-1}) \leq 0 \end{cases}$$

Admittance causality:

$$v_{Ctrl}(t_i) = v_{Sim}(t_i) - \beta(t_i)F_{FTS}(t_{i-1}); \quad \beta(t_i) = \begin{cases} k_F E_{Error}(t_{i-1}); & E_{Error}(t_{i-1}) > 0 \\ 0; & E_{Error}(t_{i-1}) \leq 0 \end{cases}$$

PID type Energy Control

Hybrid simulation of space robot applications

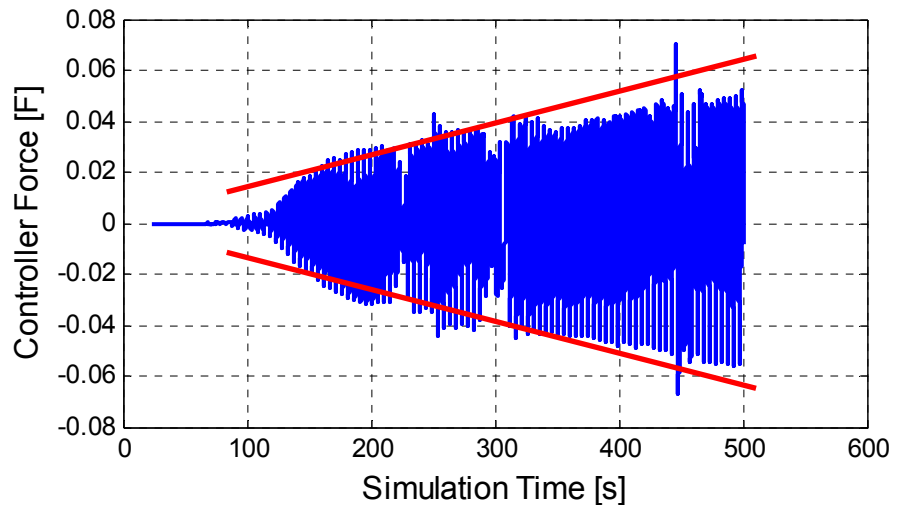
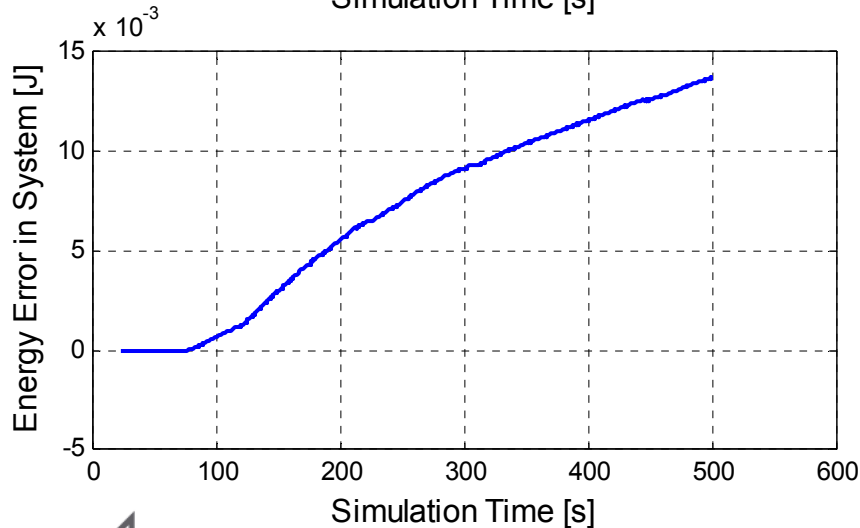
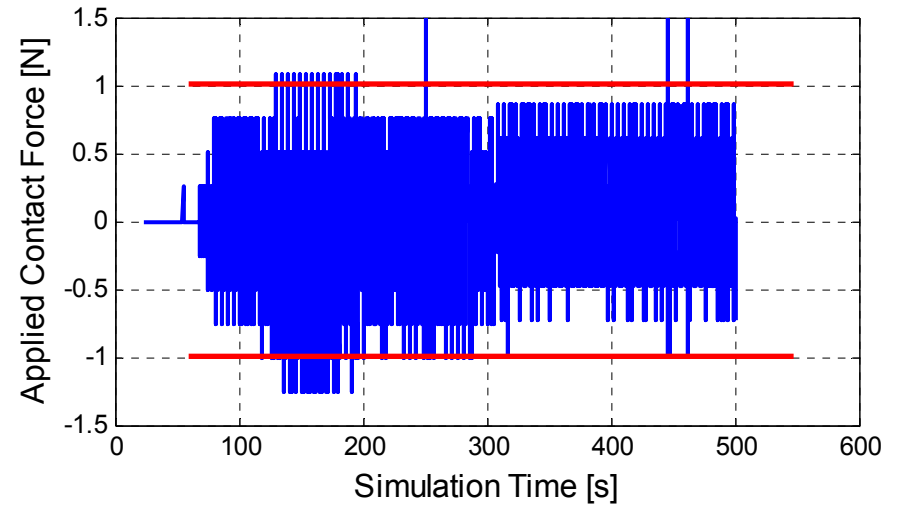
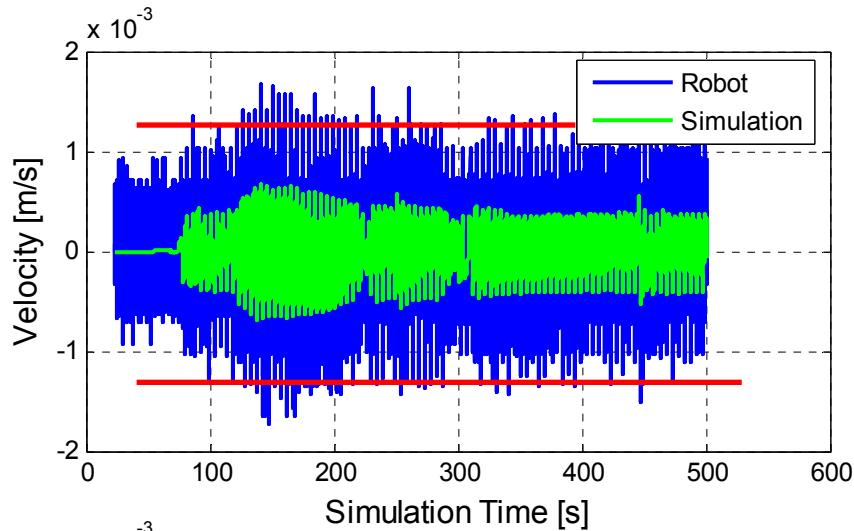
[Krenn, Schäfer, AIAA GNC 1999]

Time Domain Passivity Control

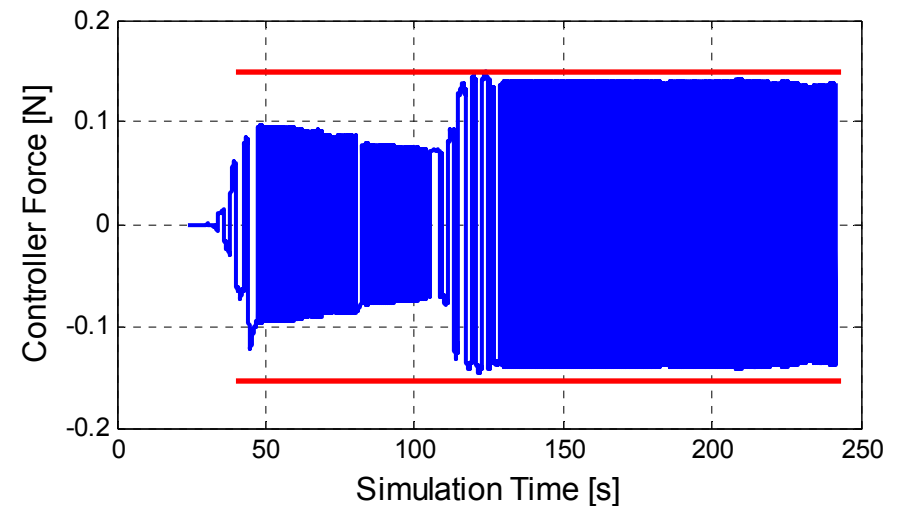
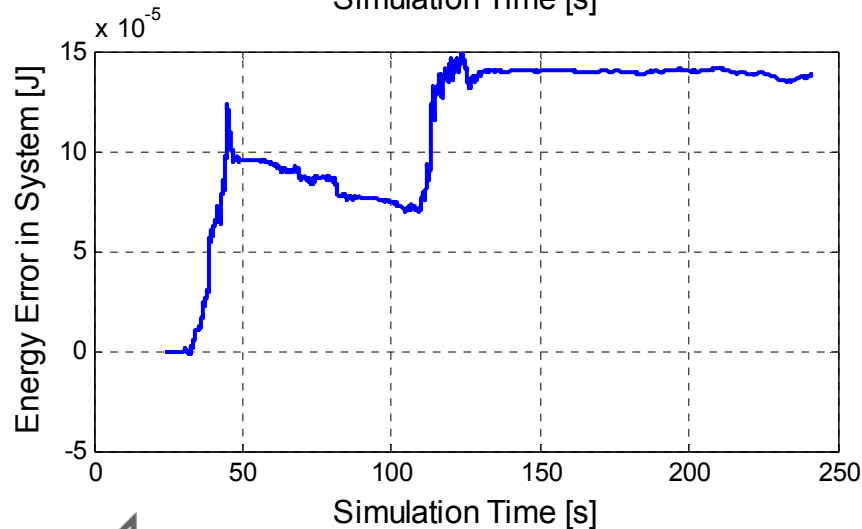
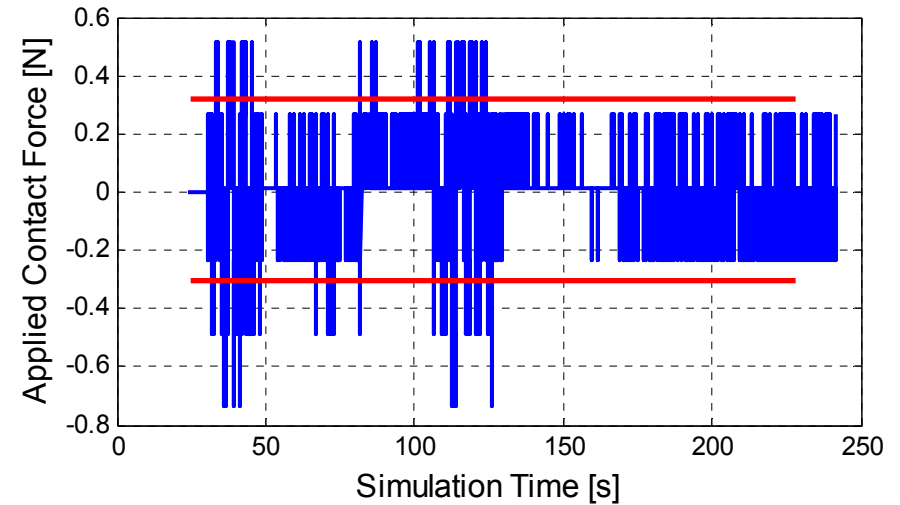
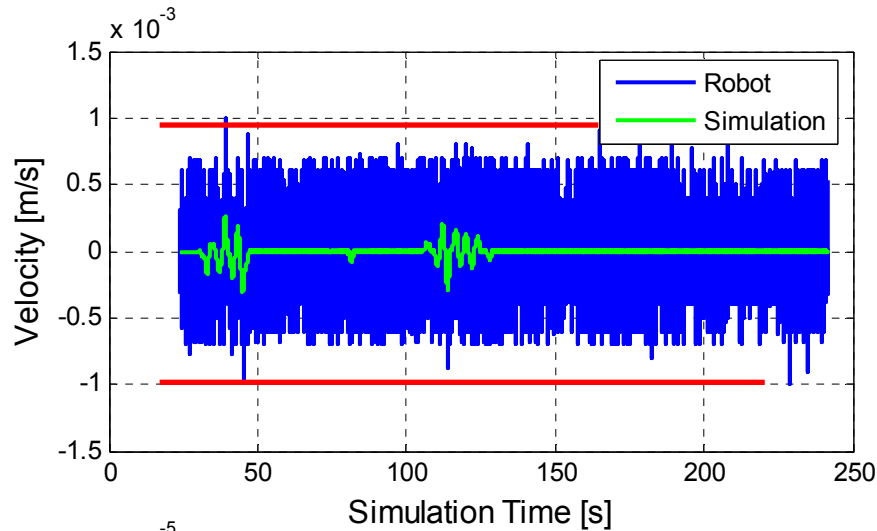
Haptic devices

[Hannaford, Ryu, ICRA 2001]

Experiment Results Using PID Type Energy Control



Experiment Results Using Time Domain Passivity Control



Conclusion & Future Work

- Meaningful results for design phases A/B using software simulation.
- Hybrid simulation required for phases C/D/E
 - Real-time simulation requirement
 - Hardware-in-the-loop simulation requirements
- Robotic systems are not passive → Numerical instabilities of closed-loop simulation
- Passivity control solutions successfully implemented and tested at EPOS
 - PID energy control approach
 - Time domain passivity control
- Future work:
 - Passivity tests at higher contact stiffness
 - Test of system transparency (accuracy of contact dynamics simulation)

