

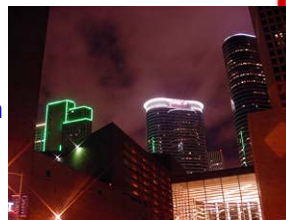


EMC/EMI in Wireless Communications

Ji Chen
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Houston, TX 77204
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UH: close to downtown of Houston
35,066 students



ECE Department: 35 faculty members, 250 graduate students

Electromagnetic Research at University of Houston:

NSF Center For Electromagnetic Compatibility Research

Areas:

Computational Electromagnetics

Antennas

High-Speed Signal Propagation

Bioelectromagnetics

Nano-devices

Wireless Propagation

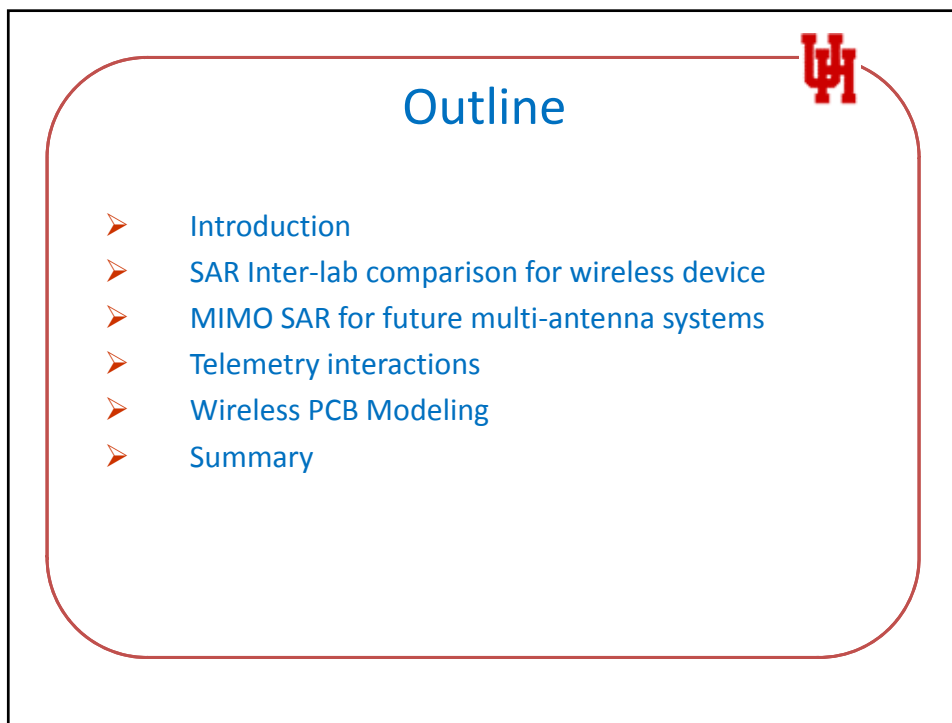
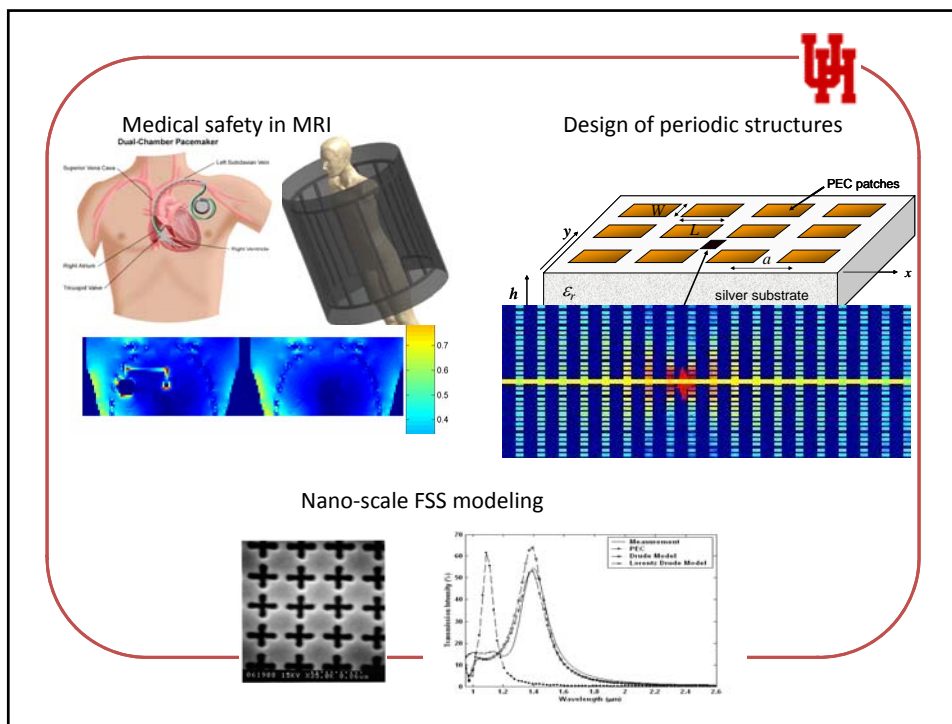
Faculty Members:

6 faculty members

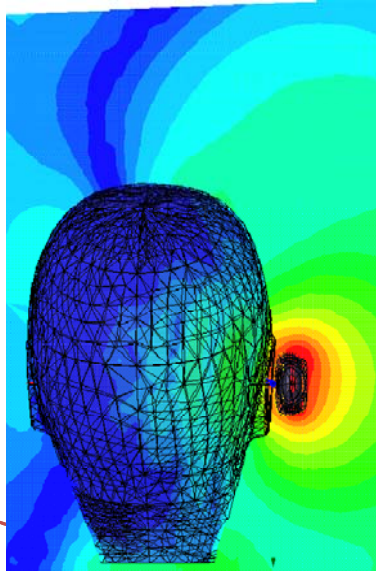
IEEE Board of Directors

past president of AP society

4 IEEE Fellows



Electric fields produced by cell phone near SAM head.



$$SAR = \frac{\sigma |E|^2}{2\rho}$$

	USA	Europe	Japan
	ANSIC95 .1	ENV5016 6	TTC/MPT
Whole Body	0.08 W/kg	0.08 W/kg	0.04 W/kg
Spatial Peak	1.6 W/kg	2 W/kg	2 W/kg

Commercial SAR measurement systems



UPH

IEEE 1528 - Body modeling

- Purpose
 - Must result in conservative over-estimate of SAR compared to real person
- Development of head model
 - Anthropomorphic vs. simplified
 - Large head gives higher SAR
 - Dimensions from US Army data
 - Compressed lossless ear model
 - CAD model available
- No hand model
 - Hand absorbs energy

UPH

IEEE 1528 - Tissue equivalent liquid

- Dielectric parameters
 - Representative of human tissue
 - Selected to result in conservative exposure
 - Consistent over time and temperature
 - Homogeneous to allow movement of E-field probe
- Other parameters
 - Low viscosity to allow easy probe movement
 - Safe to use
 - Not reactive with phantom or probe materials



ICES – TC34 – SC2 - Computational Standards

- IEEE 1528.1: Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Body from Wireless Communications Devices, 30 MHz - 6 GHz: **General Requirements for using the Finite Difference Time Domain (FDTD) Method for SAR Calculations**
- IEEE 1528.2: Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Body from Wireless Communications Devices, 30 MHz - 6 GHz: **Specific Requirements for Finite Difference Time Domain (FDTD) Modeling of Vehicle Mounted Antennas**
- IEEE 1528.3: Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Body from Wireless Communications Devices, 30 MHz - 6 GHz: **Specific Requirements for Finite Difference Time Domain (FDTD) Modeling of Mobile Phones/Personal Wireless Devices**
- IEEE 1528.4: Recommended Practice for Determining the Peak Spatial Average Specific Absorption Rate (SAR) in the Human Body from Wireless Communications Devices, 30 MHz – 6 GHz: **Requirements for Using the Finite-Element Method for SAR Calculations**

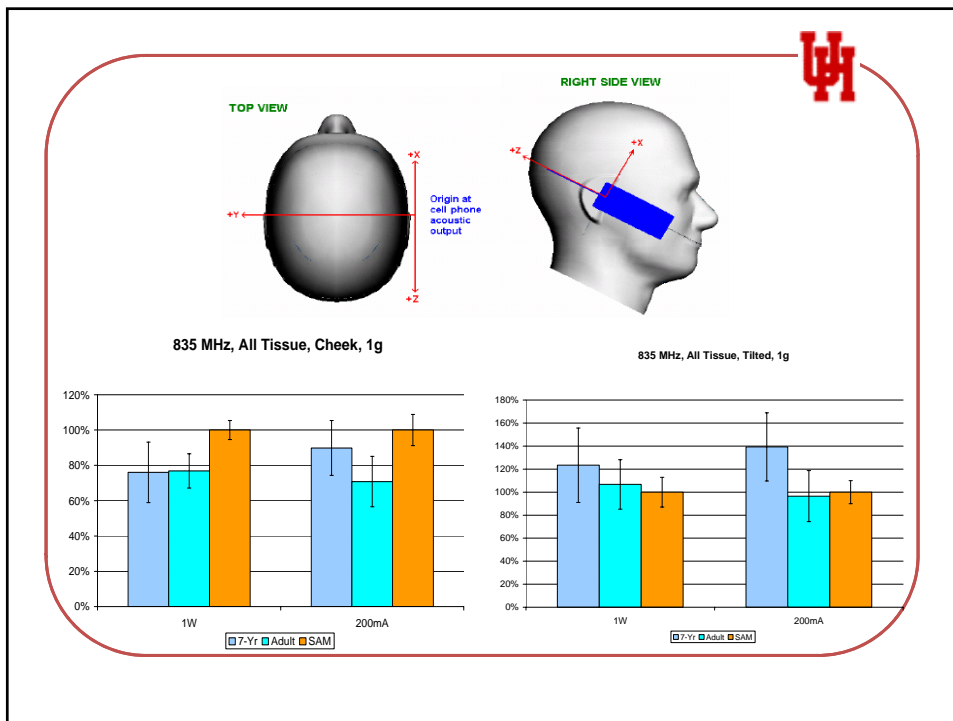
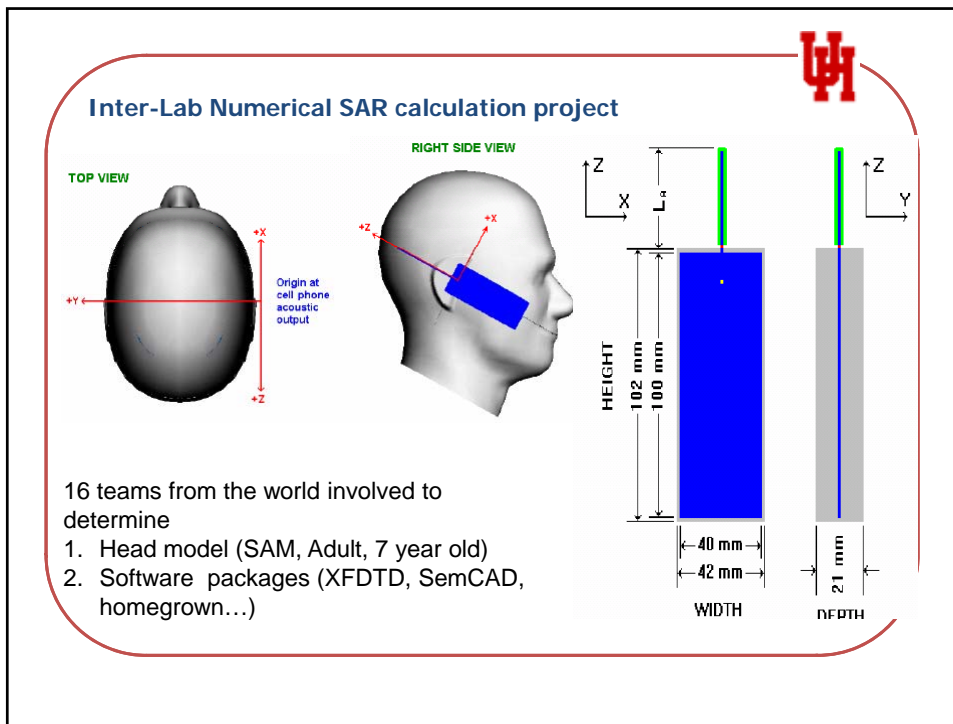


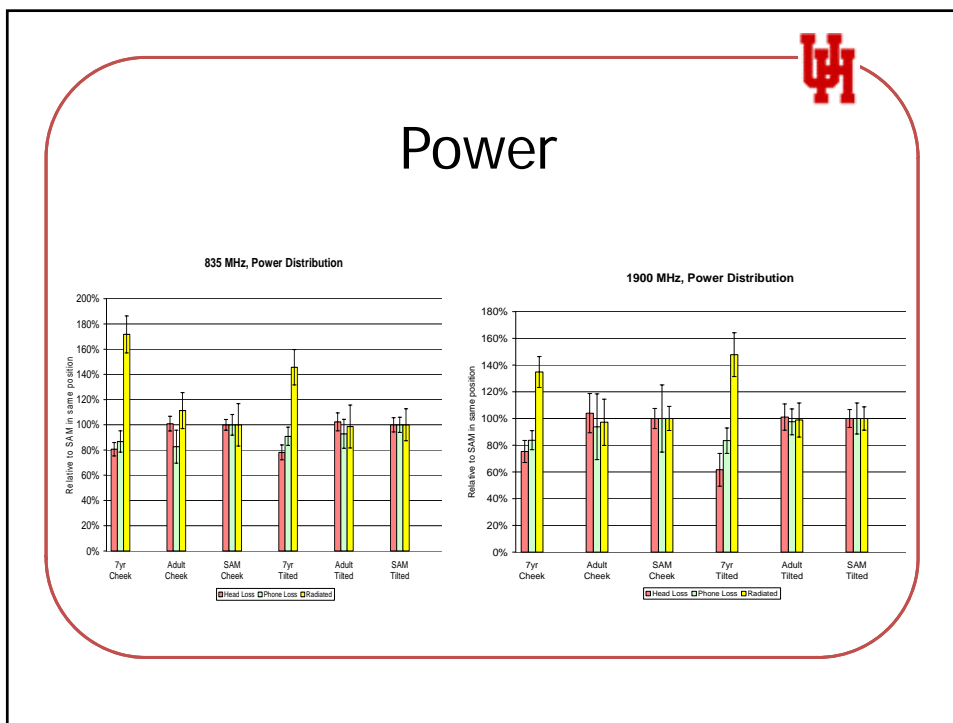
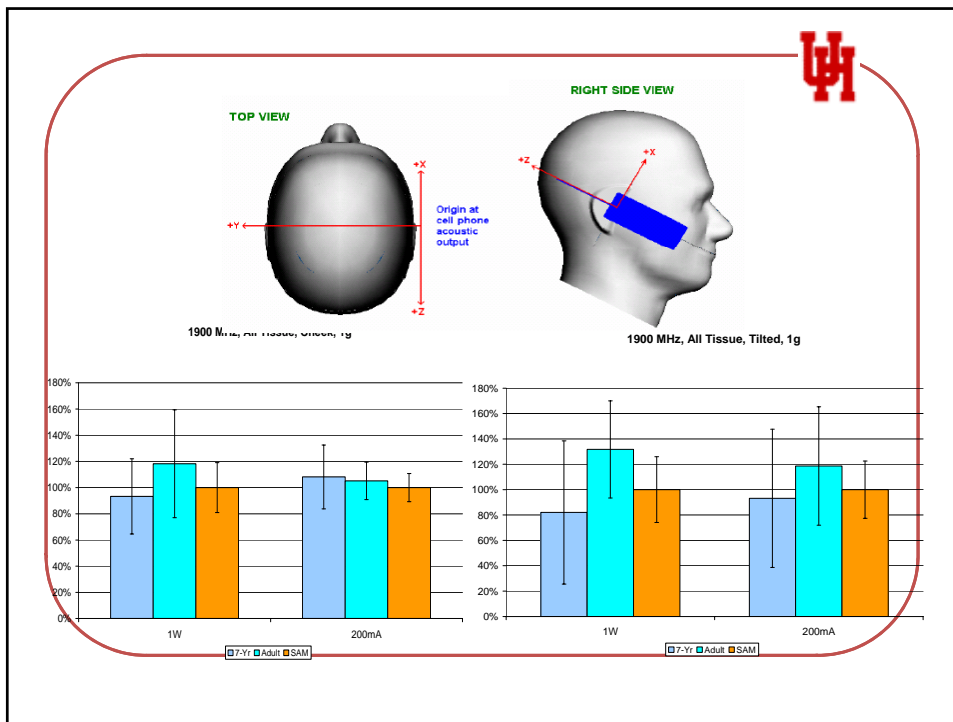
IEEE 1528.1 - General Requirements for using the Finite Difference Time Domain (FDTD) Method for SAR Calculations

Purpose: ... is to describe the **concepts, anatomical models** for compliance assessments, **techniques, validation procedures, uncertainties and limitations** of the **FDTD** method when used for determining the **spatial-peak SAR** in standardized human anatomical models exposed to wireless communication devices. 1528.1 recommends and provides **standardized anatomical models** and provides **general benchmark data** for these models. 1528.1 will **not recommend specific SAR values** since these are found in other documents, e.g., IEEE C95.1-1999.

CONTENTS

- 1. Overview
- 2. Definitions
- 3. Basic FDTD requirements
- 4. Special techniques
 - 4.1 CAD import and meshing of the device under test
 - 4.2 Non-uniform mesh and sub-grids
 - 4.3 Conformal dielectric
 - 4.4 Conformal conductor
 - 4.5 Thin wires
 - 4.6 Thin sheets
 - 4.7 Convergence testing
 - 4.8 Frequency dependent materials/tissues
 - 4.9 Running DFT for multiple frequency calculations
 - 4.10 Far zone results
 - 4.11 ADI-FDTD and FDTD meshing of dielectric materials







SAR Sensitivity:

SAR sensitivity on spacing and user effects provides information of what SAR change can be expected due to small variation of environment

Definition of Sensitivity:

$$S(x) = \frac{\partial \text{SAR}}{\partial x} \cdot \frac{x}{\text{SAR}}$$

Example:

Sensitivity: $S(\varepsilon) = 0.4$

Dielectric constant change: $\varepsilon \pm 5\%$

SAR = SAR(ε) $\pm 2\%$

Evaluation

$$\frac{\partial \text{SAR}}{\partial x} = \frac{\text{SAR}(x + \Delta x) - \text{SAR}(x - \Delta x)}{2\Delta x} = \frac{2}{3!} dx^2 \text{SAR}'''|_x + \dots$$

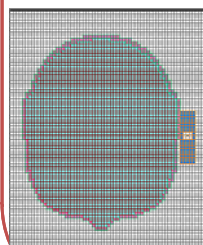


SAR Sensitivity Analysis




Spacing Effect


Distance from Head	Peak SAR	1g SAR average(normalized)	Absorption power
d = 0 mm	1	0.66	68%
d = 3 mm	0.58	0.39	52%



User effect :Head_Size_

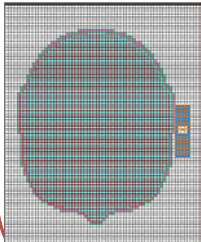
Head Size	Peak SAR (normalized)	1g average SAR (normalized)	Absorption power
Small	0.96	0.64	67%
Regular	1	0.66	68%
Large	0.96	0.64	71%






User effect : materials effect_

Dielectric	Peak SAR (normalized)	1g average SAR (normalized)	Absorption power
36	1	0.65	69%
40	1	0.65	68%
44	0.99	0.65	68%

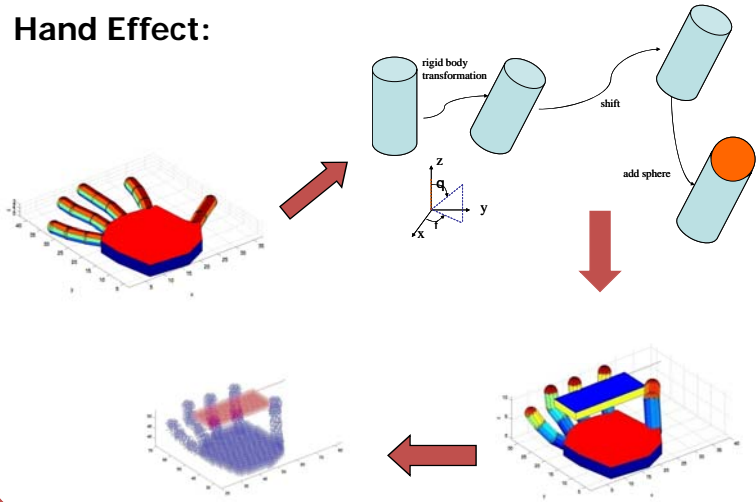


User effect : materials effect_

Conductivity	Peak SAR (normalized)	1g average SAR (normalized)	Absorption power
1.26	0.92	0.63	67%
1.4	1	0.66	68%
1.56	1.08	0.68	71%

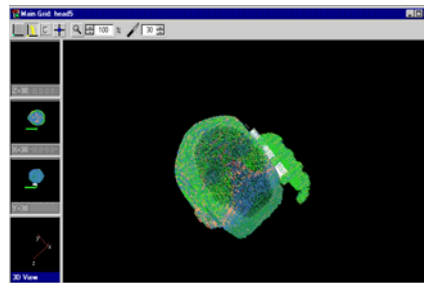
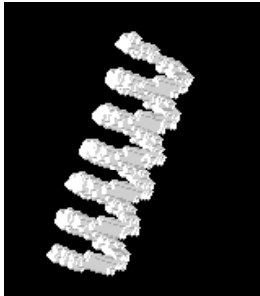


Hand Effect:

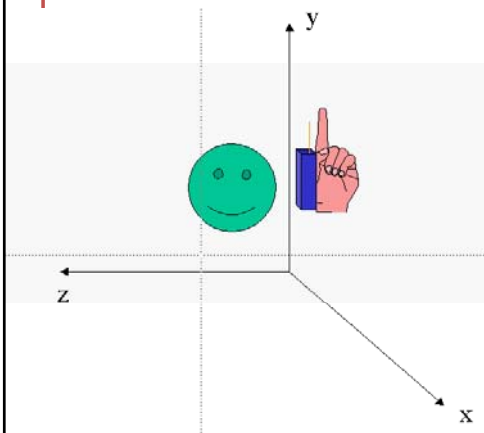




Sub-grid (helical Antenna)

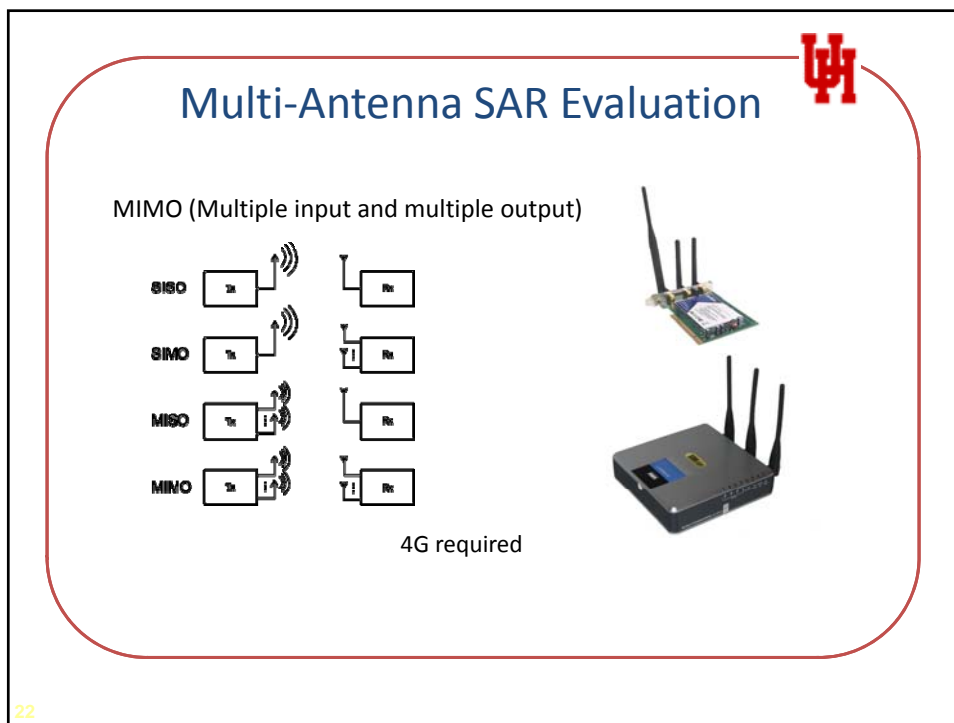
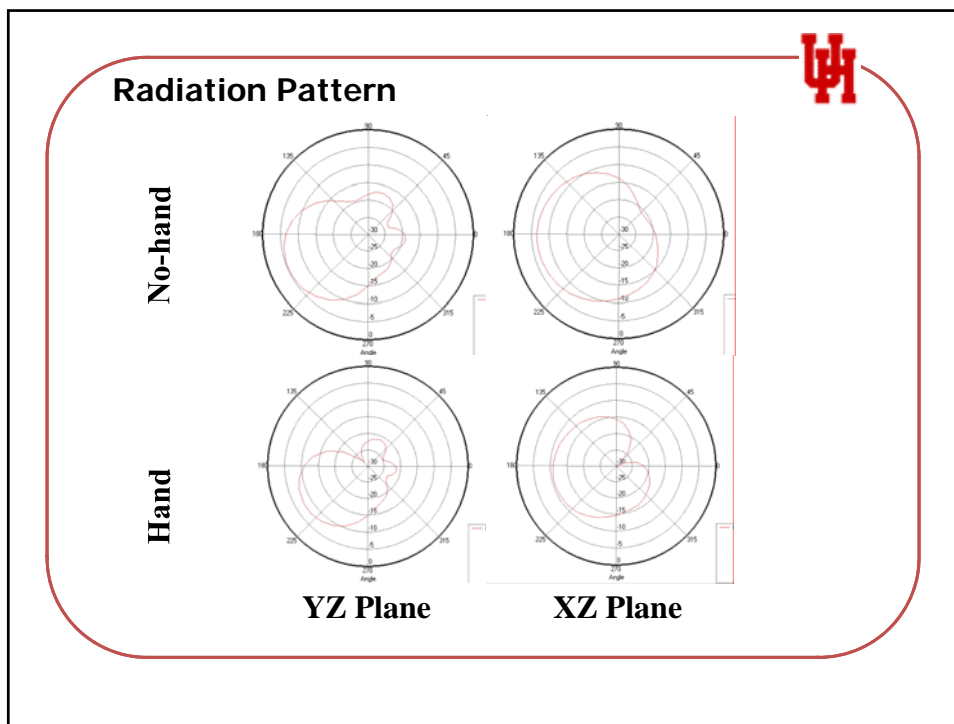


Radiation Pattern



yz plane ($\phi=90^\circ$, θ changes from $0^\circ - 360^\circ$)

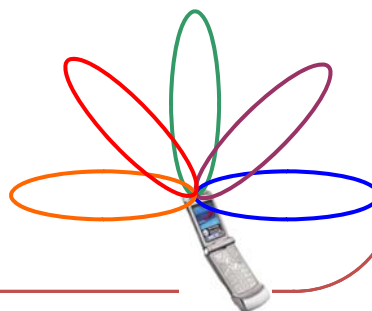
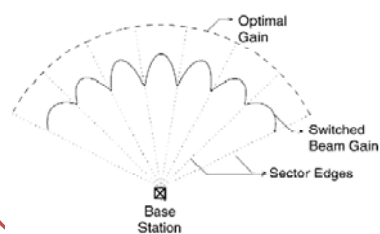
xz plane ($\phi=0^\circ$, θ changes from $0^\circ - 360^\circ$)



Challenges in SAR estimations

- 1) For fast switching multi-transmitter systems, how to simulate these SAR distributions when SAR patterns are changing
- 2) How to effectively measure all possible SAR patterns generated by these new technologies

Gain Patterns for Switched-beam and Ideal Systems



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Decomposition and Superposition Approach

Technique

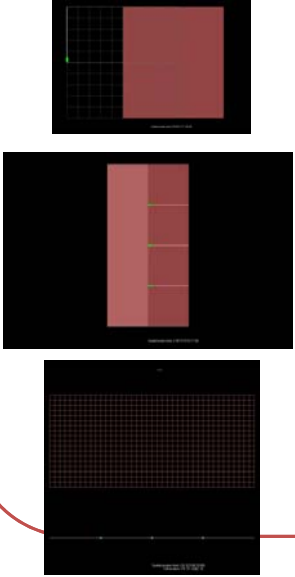
1. Electric field/SAR simulation from each antenna with unit excitation
2. Superposition results from individual simulation

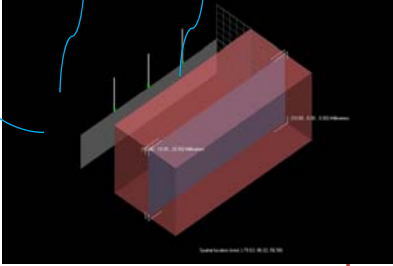
Advantage:

1. Minimum measurement required
2. Worst SAR estimation

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Modeling





Antenna Sampling volume

plate


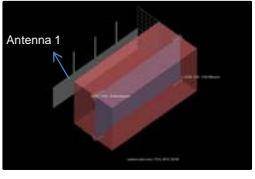
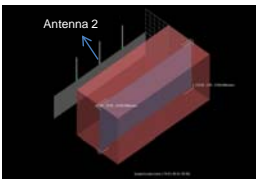
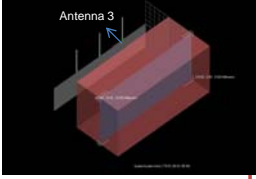

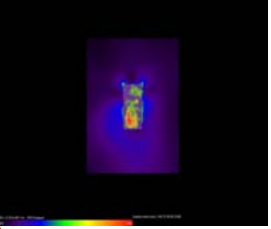
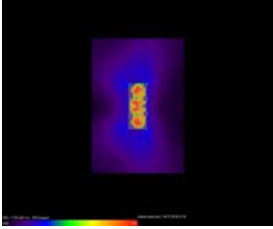
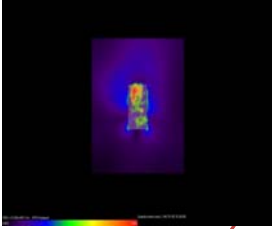


Plate: 5*20mm
 Antenna length: 5mm
 Sampling volume:
 relative dielectric constant : 40
 conductivity : 0.1s/m
 Feeding: sinusoid, frequency: 1.5GHz,
 magnitude: 1V

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Simulation Results

Electric field excited by each individual antenna

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Electric Field Optimization

$$\vec{E}_{total}(x, y, z) = \sum_{i=1}^N w_i \vec{E}_i(x, y, z)$$

$$\text{Constraint: } \sum_{i=1}^N |w_i|^2 = P_{in}$$

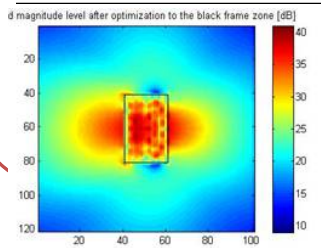
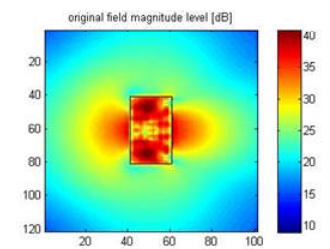
$$w_i = R_i \angle \theta_i$$

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Electric Field-Compare The Results

The minimization of the summation of E field in the region



The minimized summation of field is less than 25.78% of the original one.

Complex coefficient

$$w_1 = 0.8918 \angle -29^\circ$$

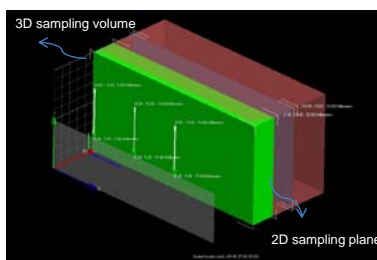
$$w_2 = 1.1887 \angle 43.5^\circ$$

$$w_3 = 0.88974 \angle -30^\circ$$

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SAR minimization

- 1) Electric field available only
- 2) SAR available only



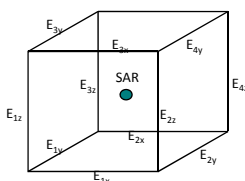
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Electric Field Available Only

$$\vec{E}_{total}(x, y, z) = \sum_{i=1}^N w_i \vec{E}_i(x, y, z)$$

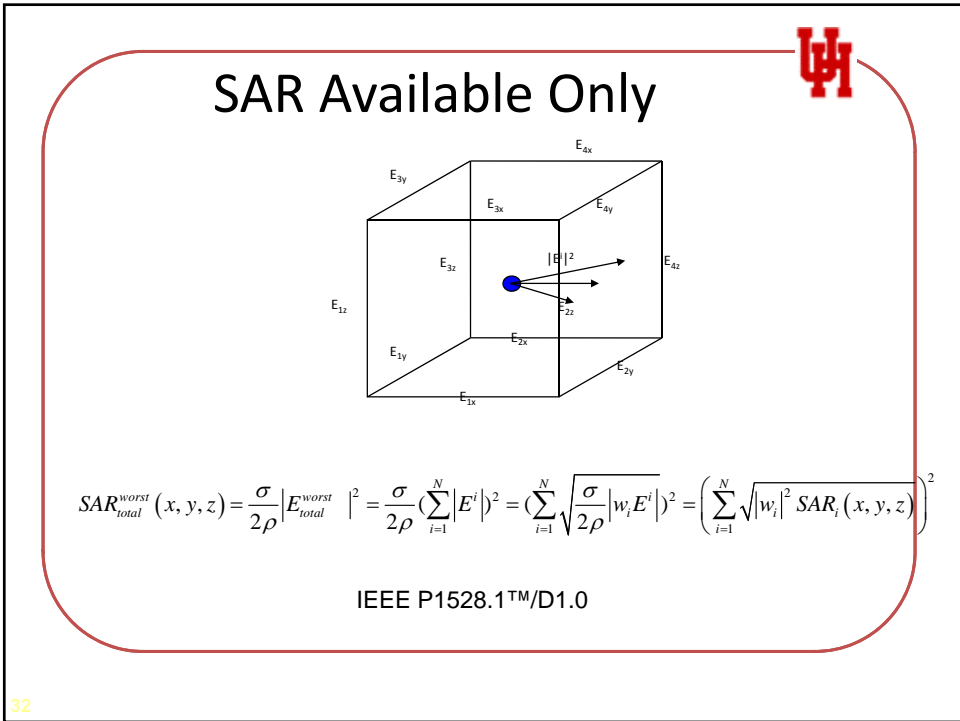
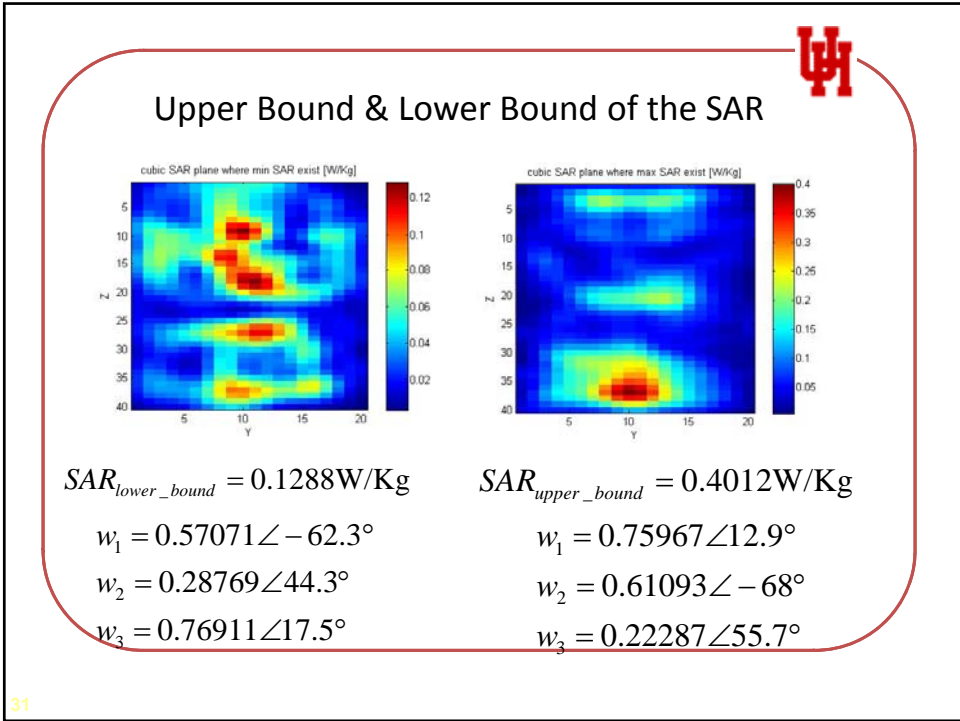
$$SAR_x = \frac{1}{4} \left(\frac{\sigma_{1x} |E_{1x}|^2}{2\rho_{1x}} + \frac{\sigma_{2x} |E_{2x}|^2}{2\rho_{2x}} + \frac{\sigma_{3x} |E_{3x}|^2}{2\rho_{3x}} + \frac{\sigma_{4x} |E_{4x}|^2}{2\rho_{4x}} \right)$$


$$SAR = SAR_x + SAR_y + SAR_z$$



IEEE P1528.1™/D1.0

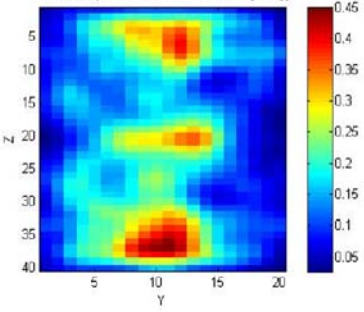
30





Worst SAR

cubic SAR plane where max SAR exist [W/kg]



$$SAR_{total}^{worst}(x, y, z) = \left(\sum_{i=1}^N \sqrt{|w_i|^2 SAR_i(x, y, z)} \right)^2$$

$$|w_i|^2 = R_i^2 = W_i (0 \leq W_i \leq 1)$$

$$\sum_{i=1}^N W_i = P_{in}$$


$$SAR_{worst_case_bound} = 0.4511 \text{ W/Kg}$$

$$W_1 = 0.5170$$

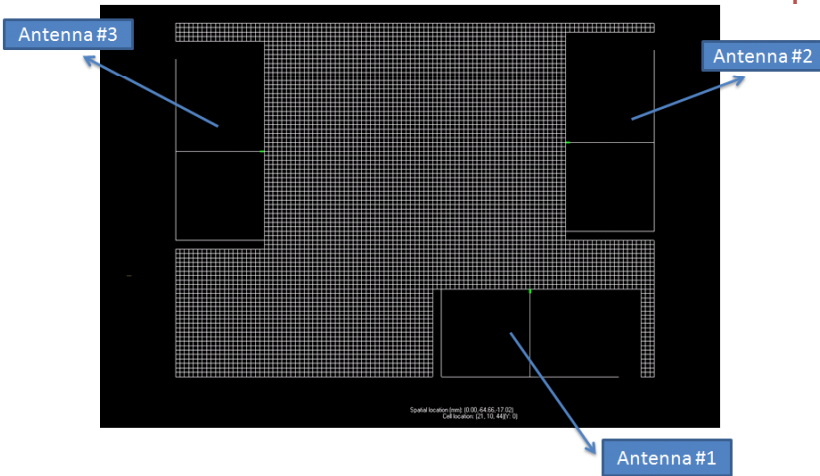
$$W_2 = 0.3533$$

$$W_3 = 0.1297$$

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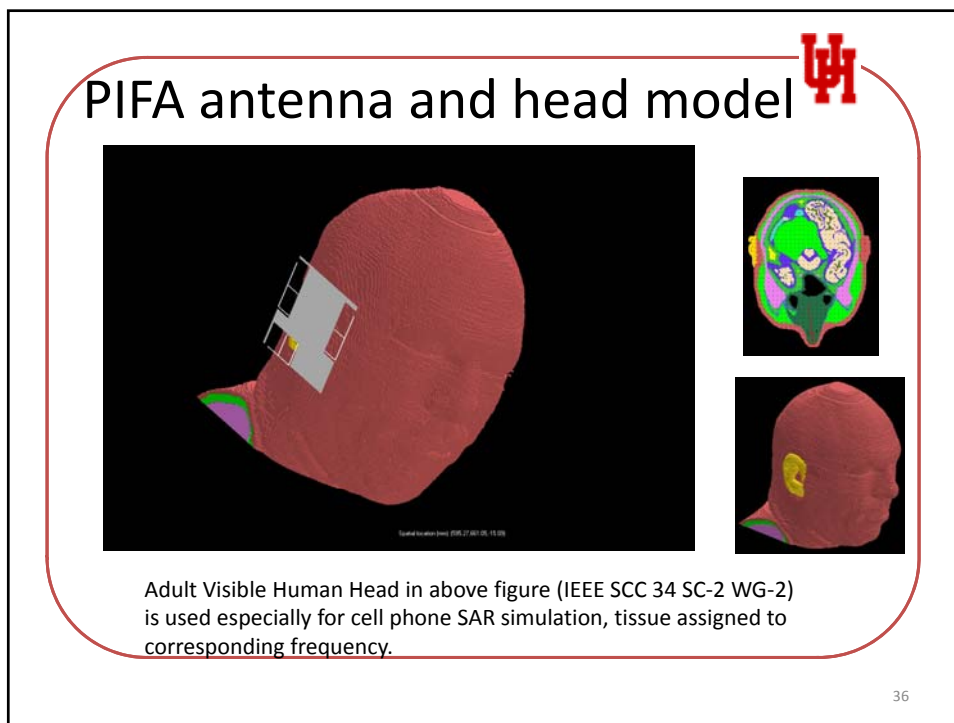
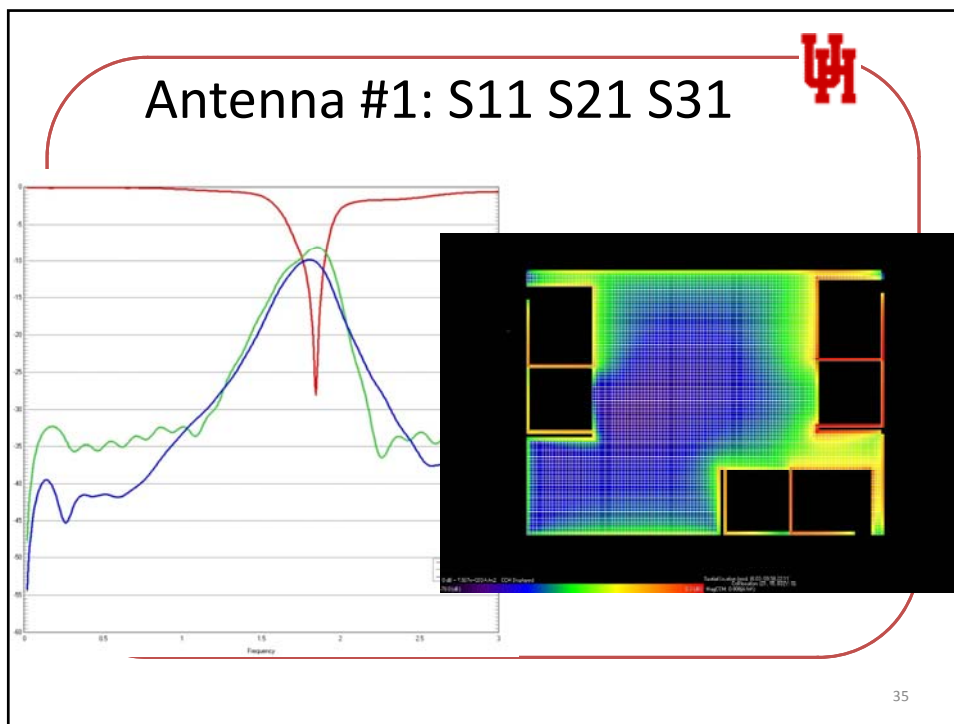


Multi-PIFA antenna model

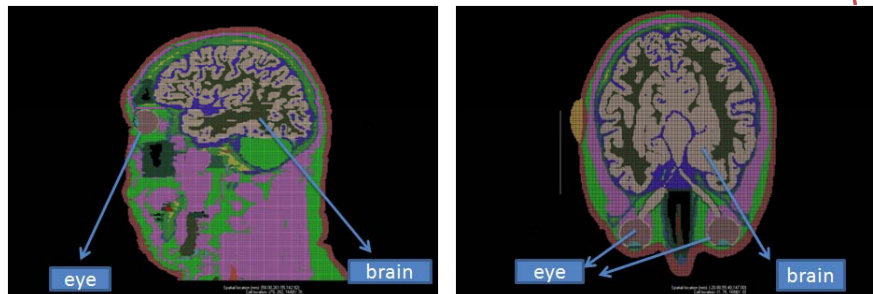


Spatial location (mm) (0.00, 04.00, 17.00)
Cell location (0.1, 10, 4487, 0)

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1 mm head model

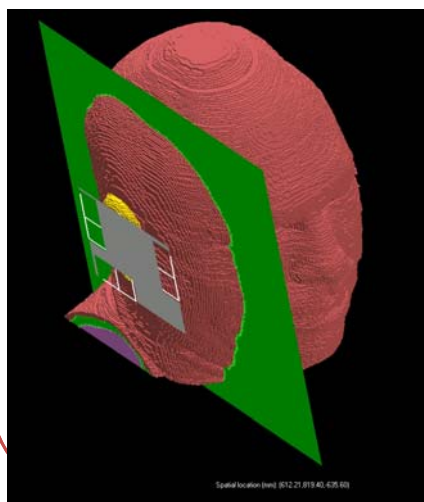


The figures above give two slices of the human head model (IEEE SCC 34 SC-2 WG-2).

The resolution of this head model is 1 mm. The different colors in the figures indicate the different tissues in human body.

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Optimize the SAR close to the MIMO PIFA antenna



Optimize the SAR near the antenna, on the left side of the green plane.

Results:

$$w1 = 0.5283 + 0.2833i$$

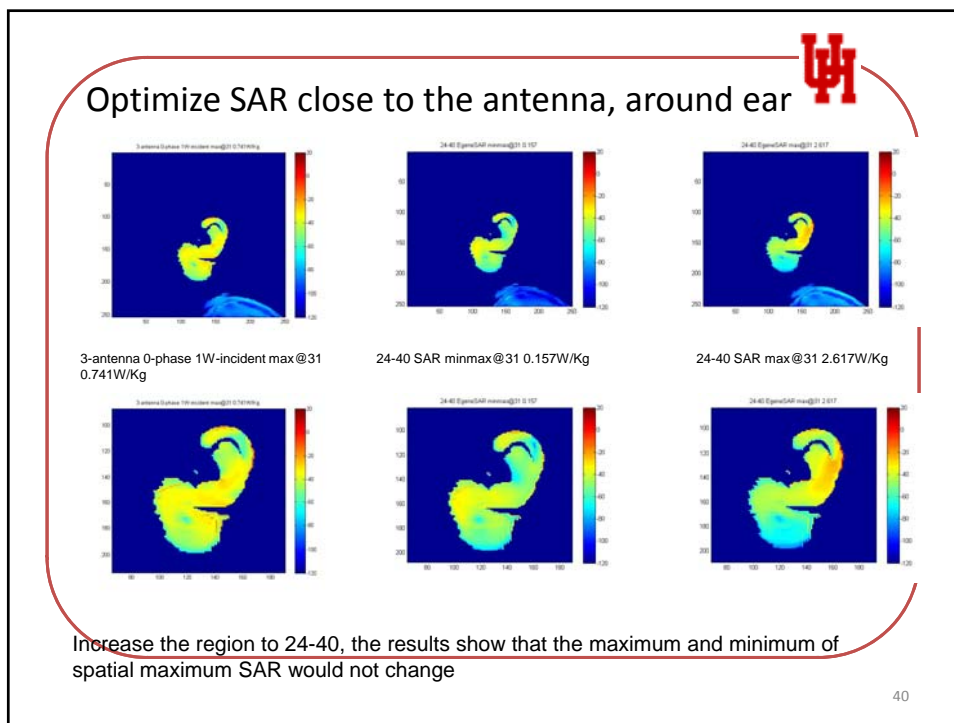
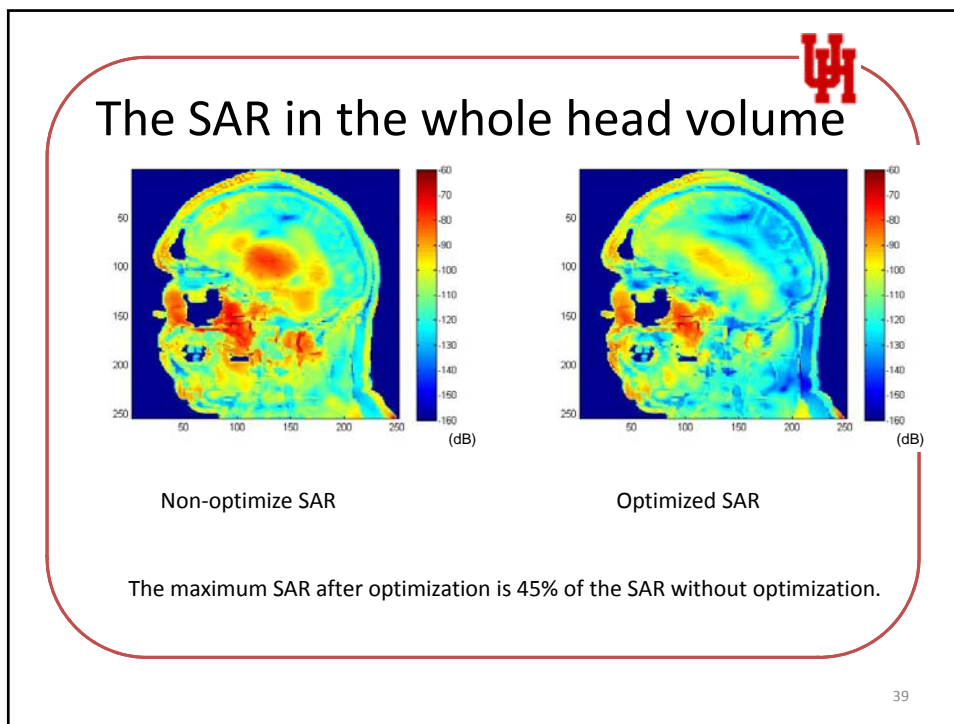
$$w2 = 0.1607 + 0.0235i$$

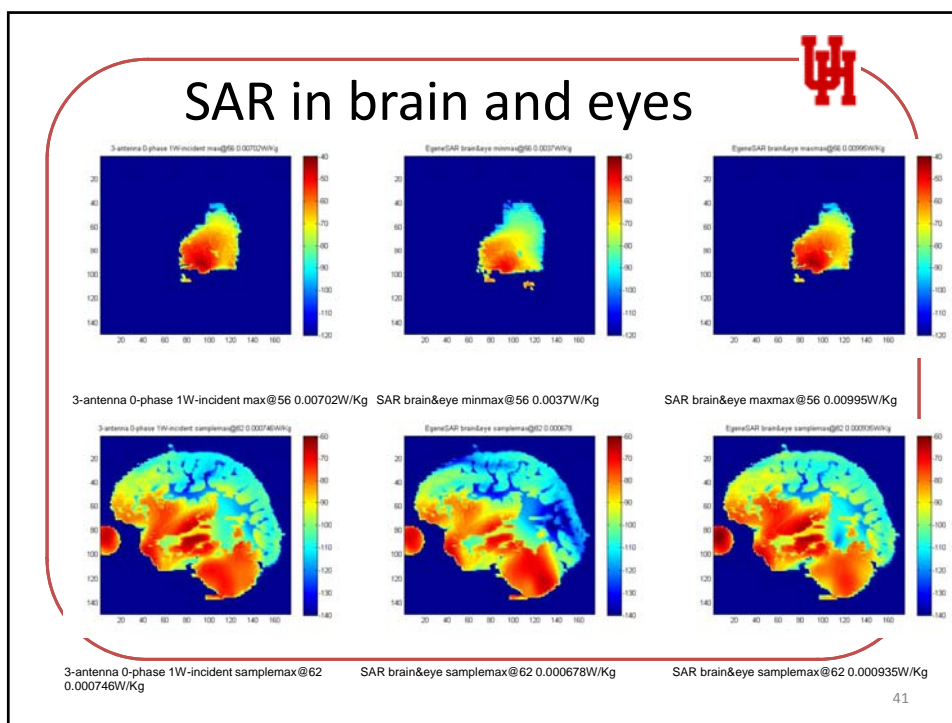
$$w3 = 0.6298 - 0.4665i$$

SAR before optimize is 0.3850 W/Kg

SAR after optimize is 0.2095 W/Kg, which is 45% smaller.

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Telemetry EMC/EMI

www.ecri.org • Printed from Health Devices Alerts on Friday, February 13, 2009 Page 1

H0053 - High Priority Medical Device Alert

Medical Device Hazard Report
 Updated: February 5, 2009

UMDNS Terms:

- Programmer/Testers, Implantable Cardiac Pacemaker [15993]
- Testers, Implantable Defibrillator/Cardioverter [17577]
- Transmitter/Receiver Systems, Telephone [17602]

Suggested Distribution:

- Cardiology/Cardiac Catheterization Laboratory
- Clinical/Biomedical Engineering
- CSR/Materials Management


Interference with Wireless Programming of Boston Scientific Implantable Cardiac Devices


Product Identifier: (1) Model 3120 Zoom Latitude Programmers; (2) Cardiac Resynchronization Therapy Defibrillators; (3) Implantable Cardioverter Defibrillators [Capital Equipment, Consumable]

Manufacturer: Boston Scientific Cardiac Rhythm Management Group [451637], One Boston Scientific Pl, Natick, MA 01760-1537, United States

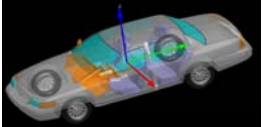
Problem: An ECRi Institute member hospital reports having difficulty establishing a wireless communication link between 2 Boston Scientific devices: an implantable cardioverter-defibrillator (ICD) and a Zoom Latitude programmer (Model 3120). The hospital's investigation concluded that the problem occurred because of radio-frequency (RF) interference from the hospital's Polycom SpectraLink 6000 wireless telephone system (formerly known as the SpectraLink Link Wireless Telephone System).

No patient harm was reported. Neither the programmer nor the defibrillator itself was affected by the interference, nor was the SpectraLink system. The interference was limited to the wireless communication link between the defibrillator and the programmer. This interference occurs when the Zoom Latitude programmer is using a technology called Zip wandless telemetry to communicate with certain Boston Scientific devices—specifically, some of its ICDs and cardiac resynchronization therapy defibrillators (CRT-Ds). It does not occur if Zip wandless telemetry is not used.

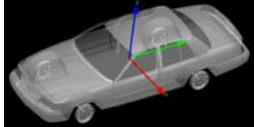





A typical police car (Ford Crown Victoria)



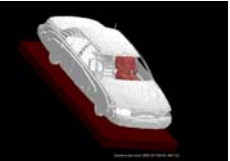
CAD model of the car



Car with metal parts only
According to IEEE P1528.2



Bystander




Passenger

Ground is 30cm thick slab, with relative permittivity 8 and conductance 0.01 S/m, extend 10cm in x and y Direction beyond the car/bystander.

According to IEEE 1528.3 On the Ground Modeling Implementation

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Antenna

- 1/4 30 MHz
- 1/4 75 MHz
- 1/4 150 MHz
- 1/4 450 MHz
- 1/4 900 MHz
- 5/8 150 MHz
- 5/8 450 MHz
- 5/8 900 MHz

d-distance

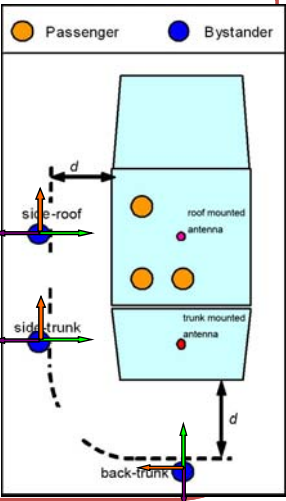
- 20cm away
- 100cm away

Three facing direction:

- ↑ Bystander model 1 --> facing the car
- ↑ Bystander model 2 --> facing front
- ↑ Bystander model 3 --> face off the car

Four seat modeling:

- Passenger no additional parts
- Passenger model 1 --> with metal seat
- Passenger model 2 --> with spring coils
- Passenger model 3 --> with both seat & coils

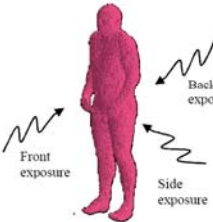


Legend: ● Passenger, ● Bystander


Antenna locations: roof mounted antenna, trunk mounted antenna

Exposure directions: side-roof, side-trunk, back-trunk

Distance: d

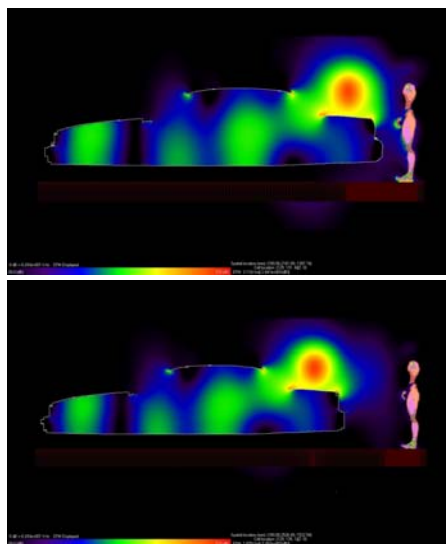
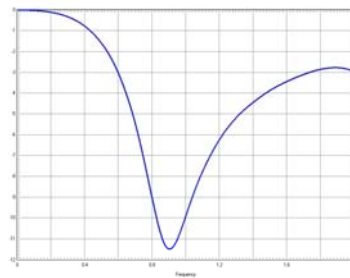


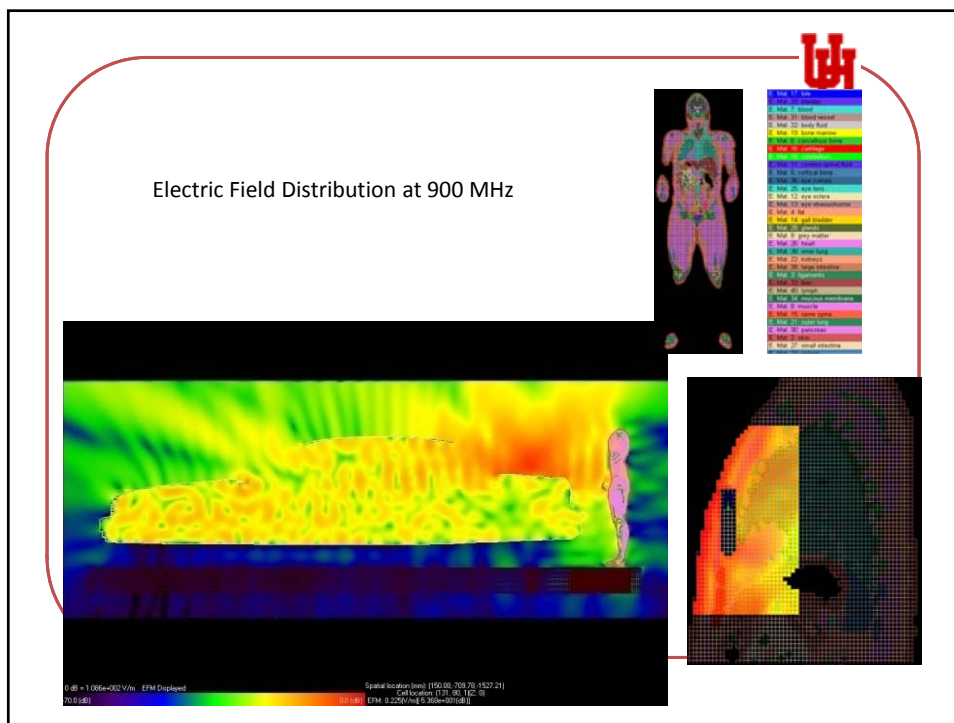
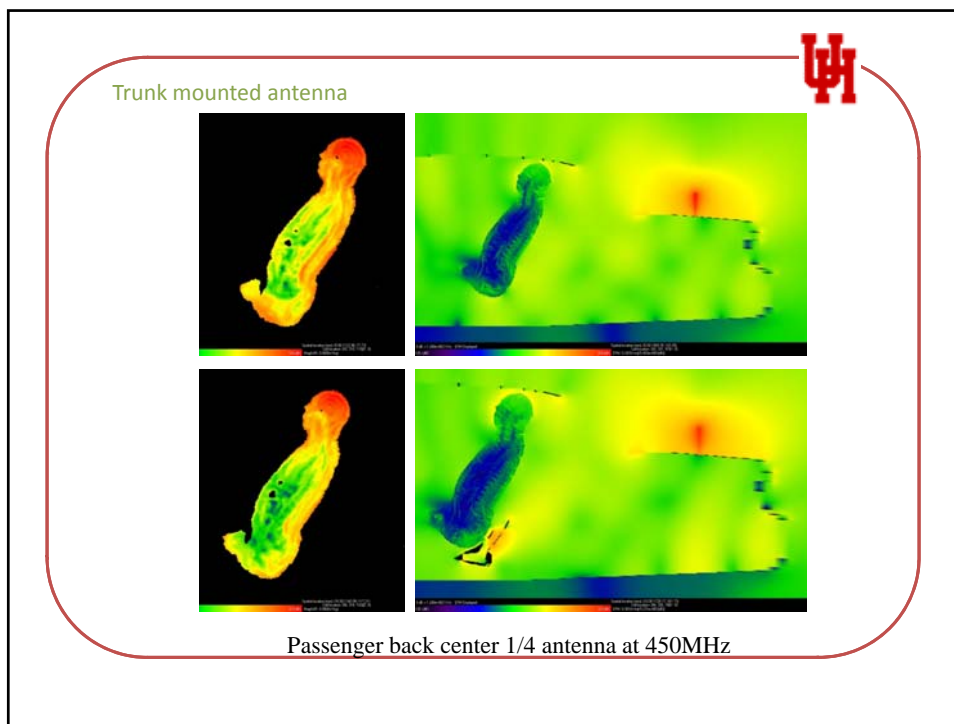
Front exposure
Back exposure
Side exposure





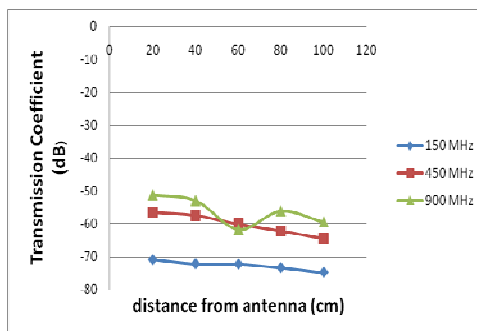
Design of Implantable Antenna



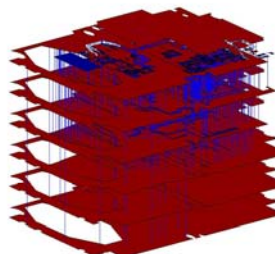
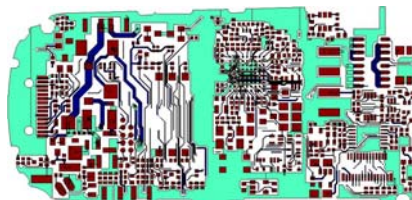




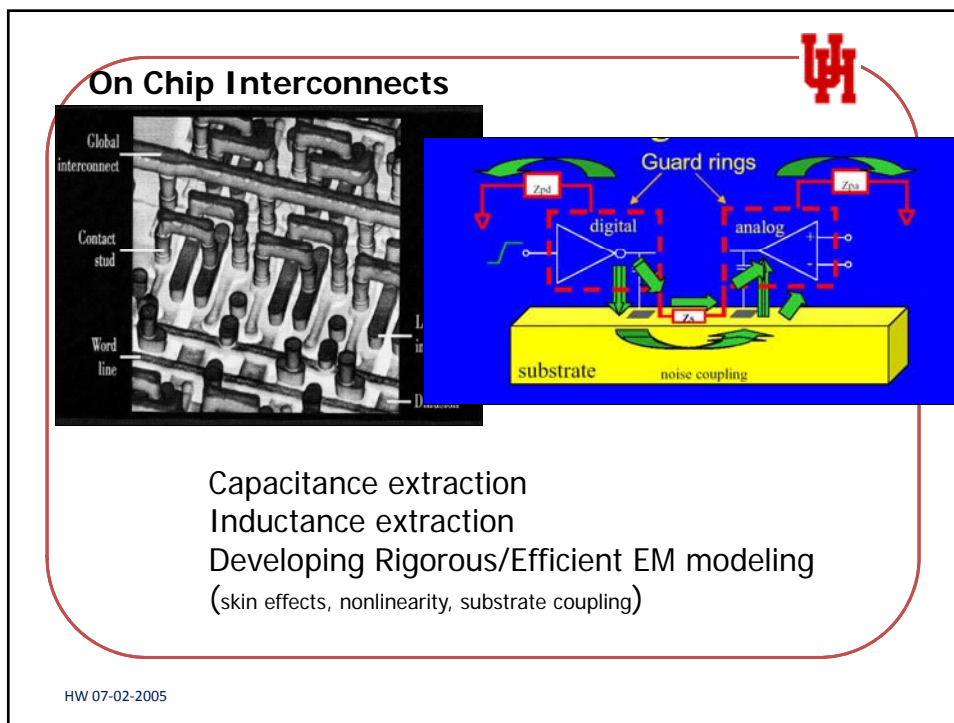
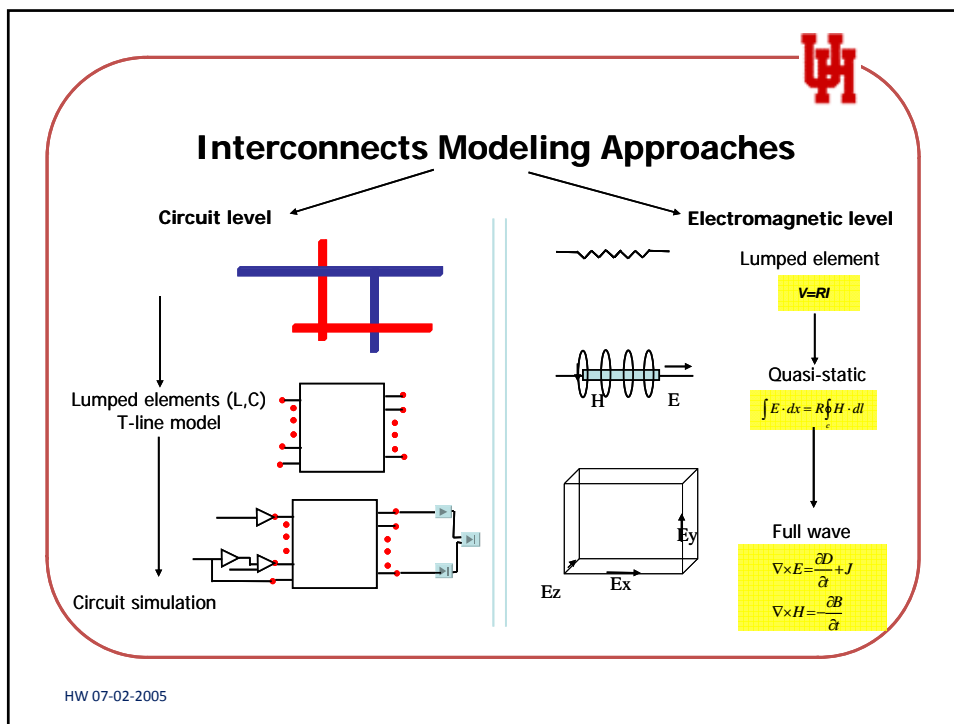
	SAR with Device (W/kg)	SAR W/O Device (W/kg)
150 MHz	0.0028	0.0020
450 MHz	0.0041	0.0034
900 MHz	0.0077	0.0067




Interconnect Modeling



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Silicon to package interconnects

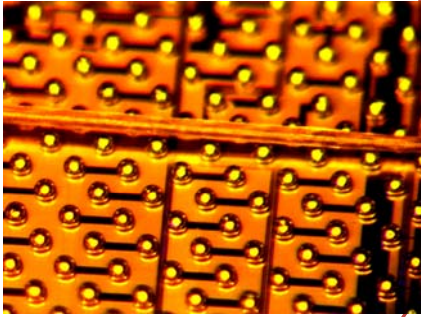


Flip Chip interconnect

Underfill

Silicon

Package




Effects of solder bumps with full-wave simulation

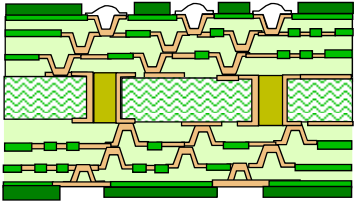

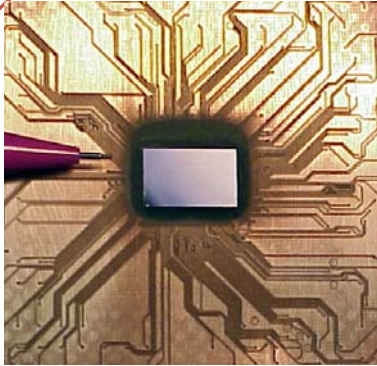
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Detailed description: This slide illustrates silicon to package interconnects. It features a schematic diagram on the left showing a yellow 'Silicon' chip on a blue 'Package' substrate, with a red arrow pointing to the 'Flip Chip interconnect' and another red arrow pointing to the 'Underfill' material. To the right is a microscopic photograph of a flip chip assembly, showing a grid of gold solder bumps connecting the silicon chip to the package substrate. Below the schematic, the text 'Effects of solder bumps with full-wave simulation' is present. The slide is dated 'HW 07-02-2005' and includes a red 'UH' logo in the top right corner.

On package interconnects



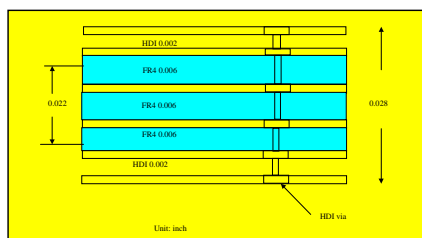
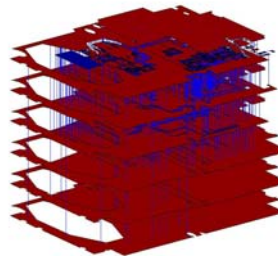
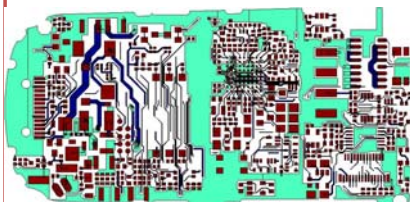
T-line via- inductance



HW 07-02-2005

Detailed description: This slide focuses on on-package interconnects. It contains three images: a top-left photograph of a chip with a central square pad and radiating circuit traces; a top-right photograph showing a close-up of a T-junction in a circuit trace; and a bottom-right cross-sectional diagram of a T-junction on a package, illustrating the inductance associated with the via. The text 'T-line via- inductance' is positioned below the top-left image. The slide is dated 'HW 07-02-2005' and includes a red 'UH' logo in the top right corner.

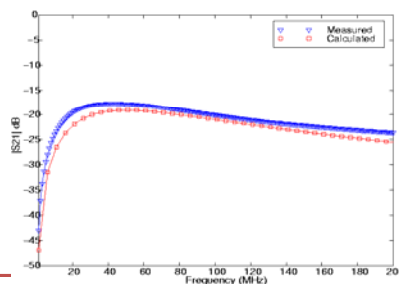
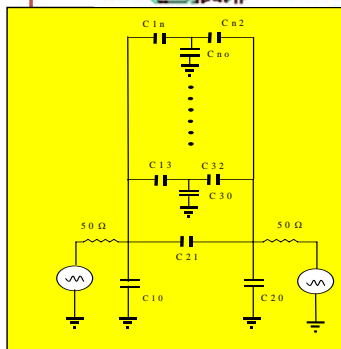
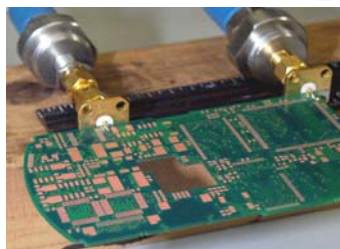
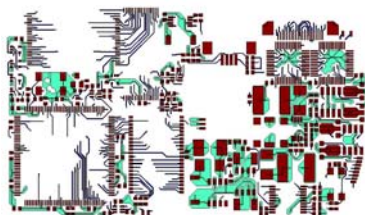
System board interconnects



Low frequency → lumped
 Higher freq. → T-line
 Extreme freq. → full wave

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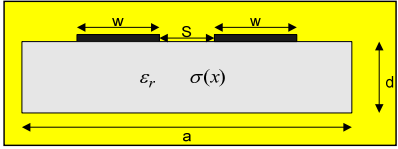
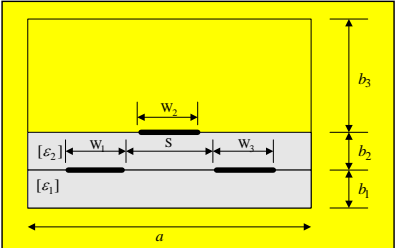
Examples




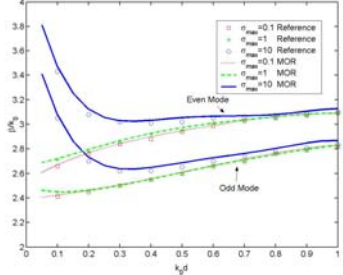
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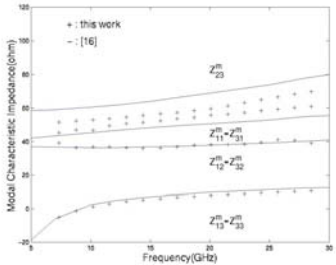
Examples

T-line parameter extraction (RLGC)

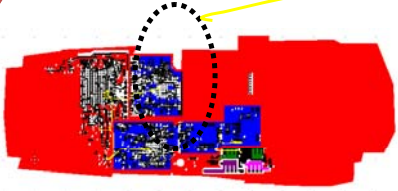




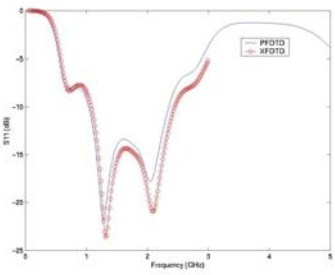


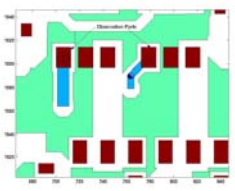
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Examples → full wave

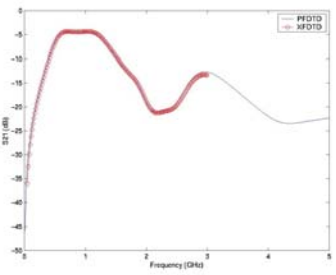



Reflection





Transmission





HW 07-02-2005



Summary

1. Various challenges EMC/EMI Issues in the design of wireless products
2. Accurate EM modeling techniques may help understanding these issues
3. Many challenges