



---

Product Safety Engineering Society  
**Taipei Chapter**

# High Frequency Voltage Stress

Presented by: Flore Chiang

Date: March 30, 2012



### 2.10.1.1 Frequency

The insulation requirements given in 2.10 are for frequencies up to 30 kHz. It is permitted to use the same requirements for insulation operating at frequencies over 30 kHz until additional data is available.

### 10 Insulation requirements

The insulation requirements given in this standard are for frequencies up to 30 kHz. It is permitted to use the same requirements for insulation operating at frequencies over 30 kHz until additional data are available.

**Now the additional data is available!**





---

Product Safety Engineering Society  
**Taipei Chapter**

## ground rules:

1. intro to PD.
2. experimental results.
3. comparison with current practice.
4. **why** different?
5. **how** air and **solid** dielectrics behave under high frequency stress?



## IEC 60664-4:2005 (2nd Ed.)

- Any type of periodic voltages with a **fundamental frequency** ( $f_0$ ) above 30 kHz and up to 10 MHz

Key phenomenon = **partial discharge (PD)**

- Its deteriorating effect is aggravated roughly in proportionally to the frequency

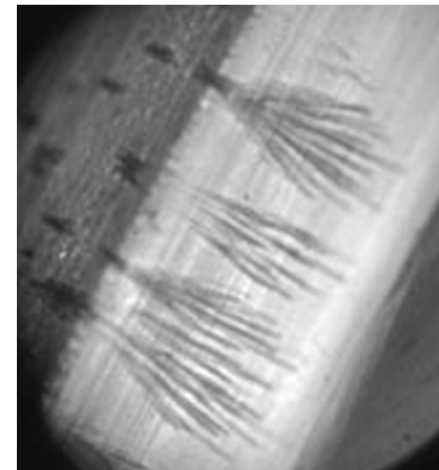
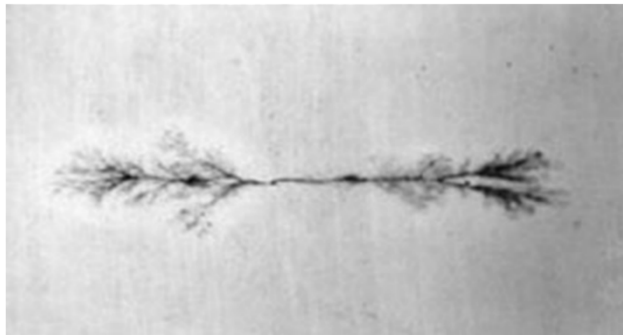




## partial discharge (PD)

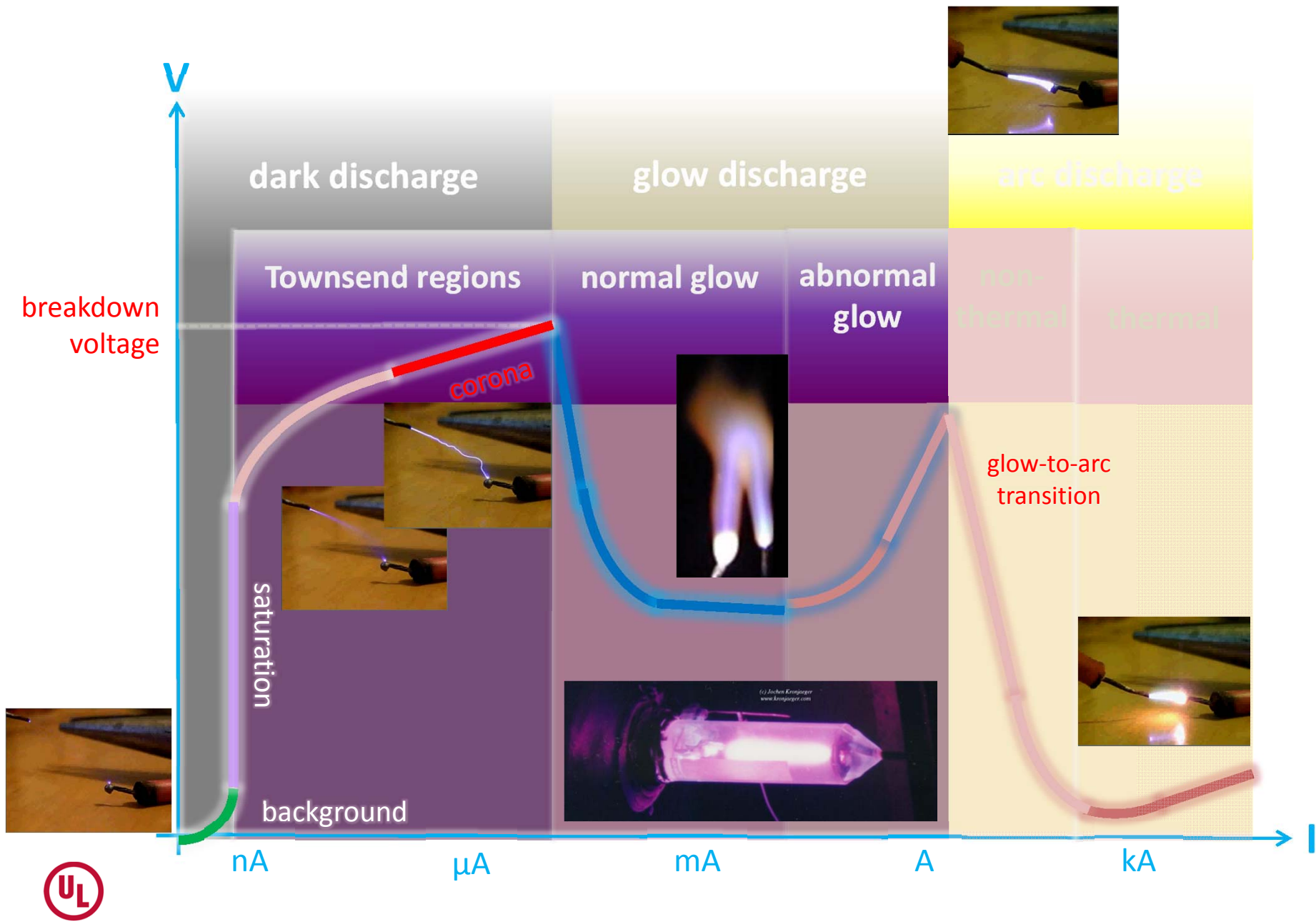
is a localized discharge within a solid or fluid dielectric system, restricted to only a part of dielectric material thus *only partially bridging the electrodes*, and is typically observed:

- in cavities, voids (bubbles) or gaps;
- between interfaces of different dielectric properties;
- at sharp electrode edges or protrusions.



Electric arc video





Slow motion video of lightning

© **Tom A. Warner**  
**ztresearch.com**



# CLEARANCES



# field homogeneity

inhomogeneous field (point-to-plane).....Case A

homogeneous field (plane-to-plane)..... Case B

**approximately** homogeneous field

- when the radius of curvature of the conductive parts is equal or greater than **20 %** of the associated clearance.

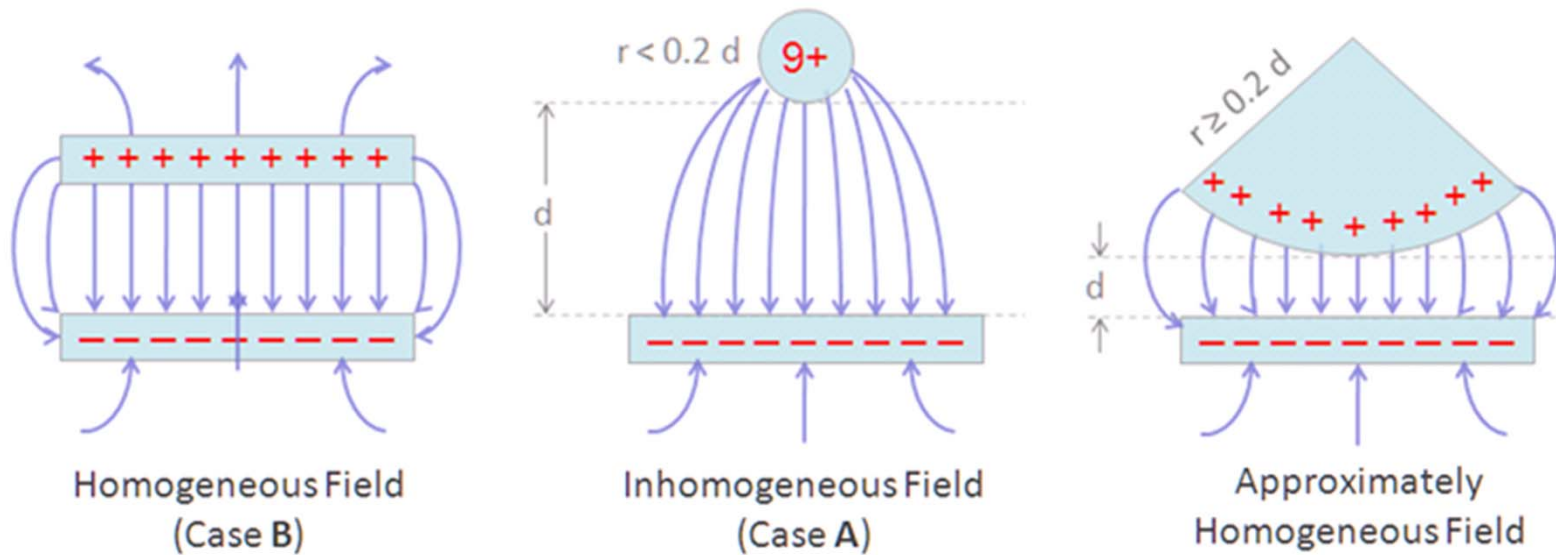




figure A.1 — breakdown at high frequency in air at atmospheric pressure, homogeneous field, 50 Hz – 25 MHz

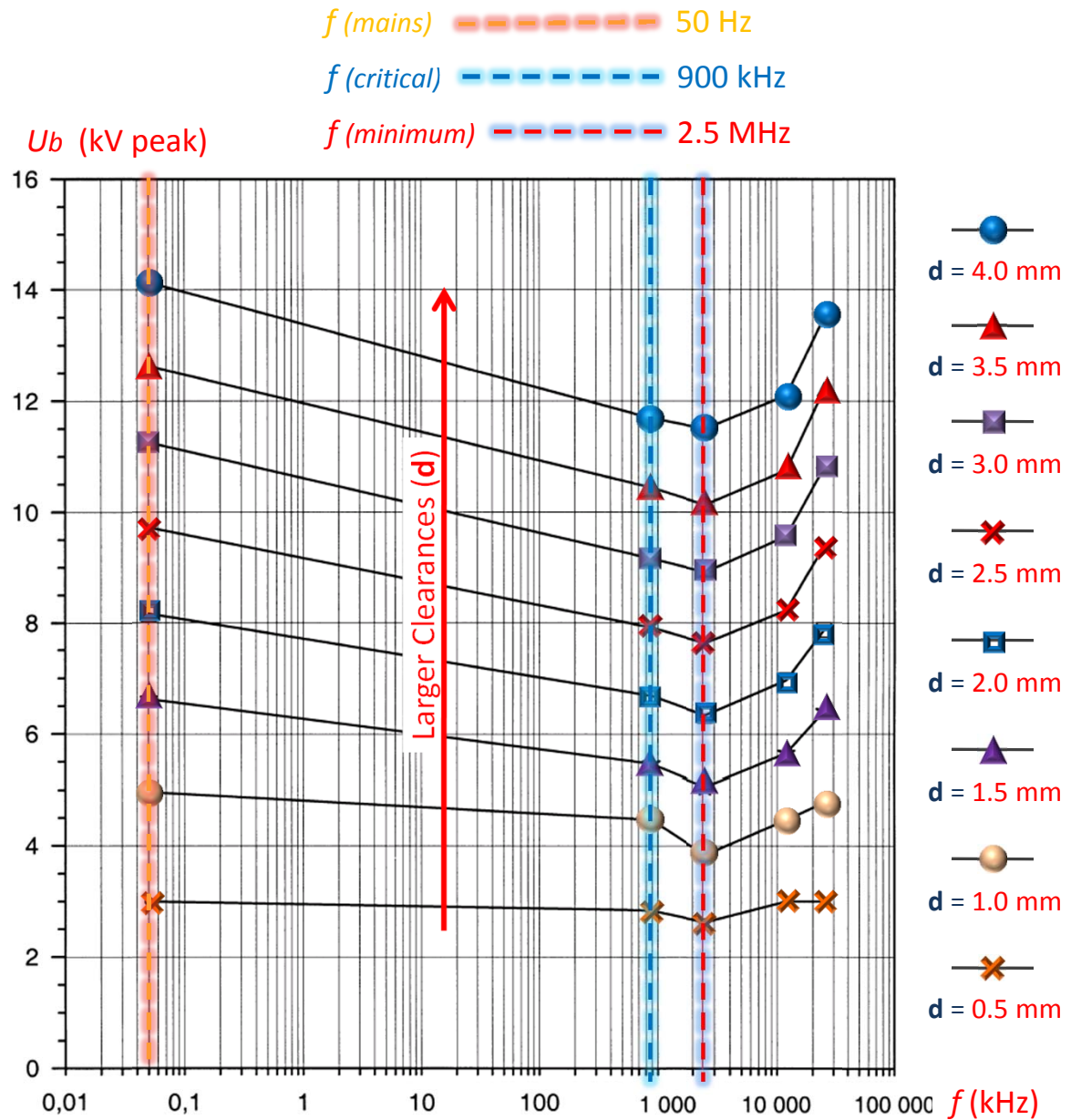
breakdown voltage ( $U_b$ ) is frequency-dependent.

$U_b$  degrades at 900 kHz, i.e., critical frequency.

worst-case scenario at 2.5 MHz, i.e.,  $f_{(min)}$

**~80% retention rate**

little effect on small clearances.



## inhomogeneous field distribution

- the corona discharge phenomenon in inhomogeneous fields (point-to-plane) is much more intense than homogeneous (plane-to-plane) that can be observed by naked eye.
- the worst-case  $U_b$  is about **50%** of that at power frequency.

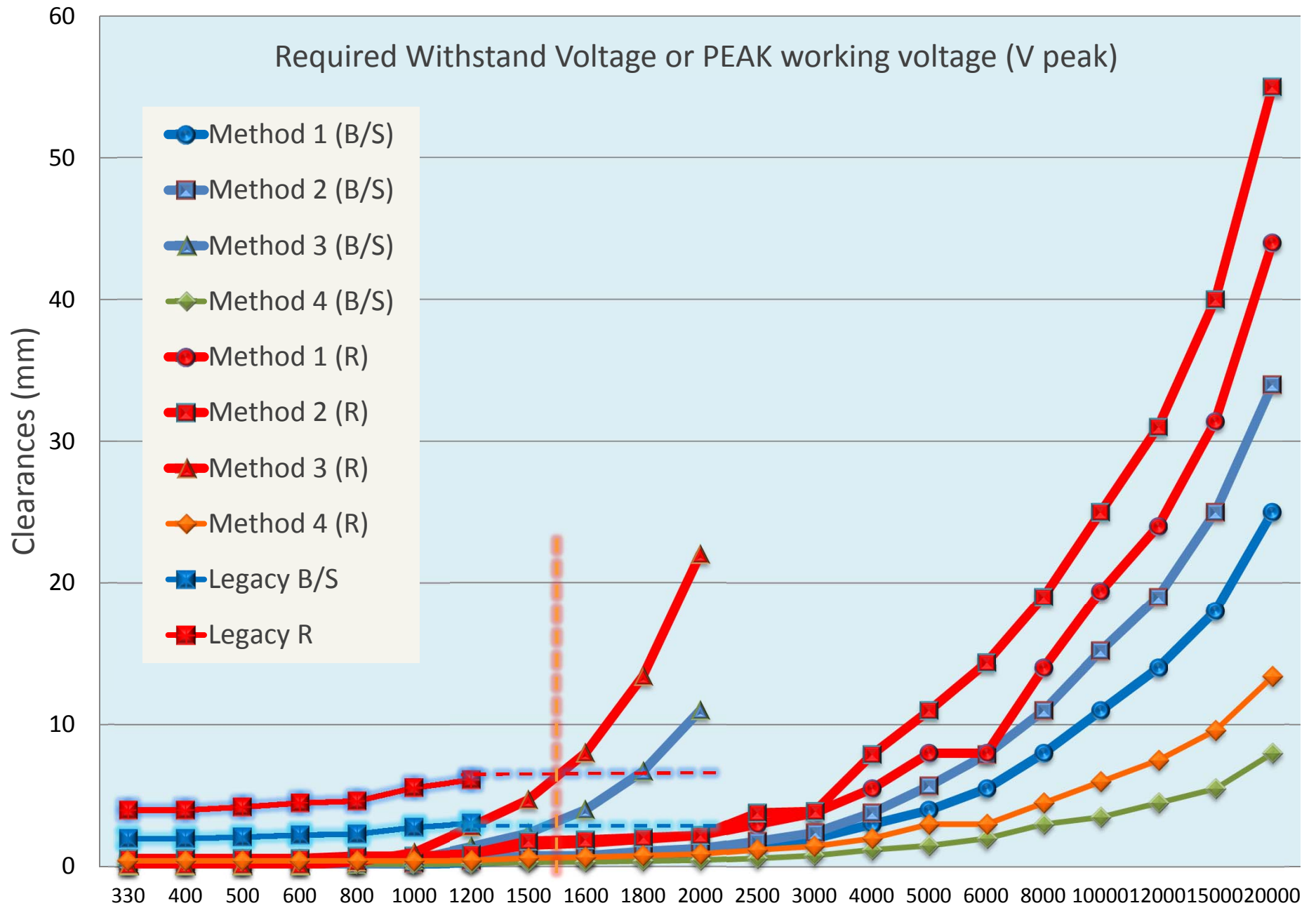
half off everything!

50%  
off

sitewide details

the ultimate sale!

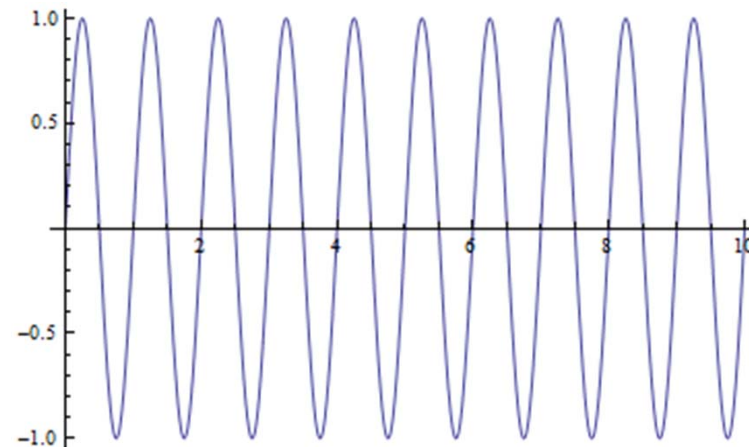
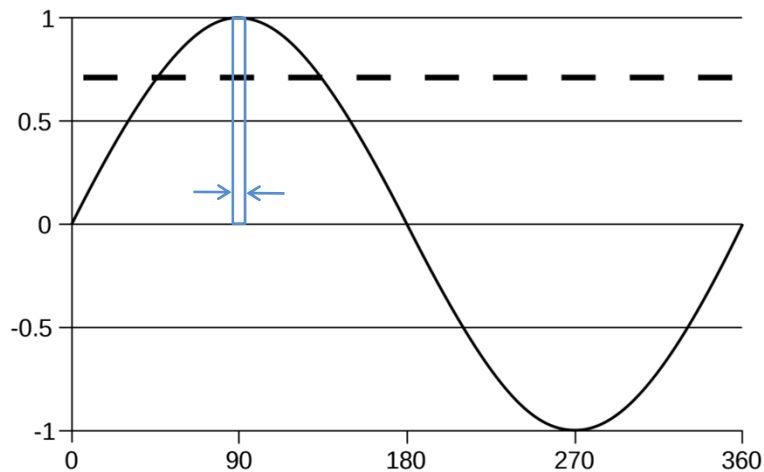


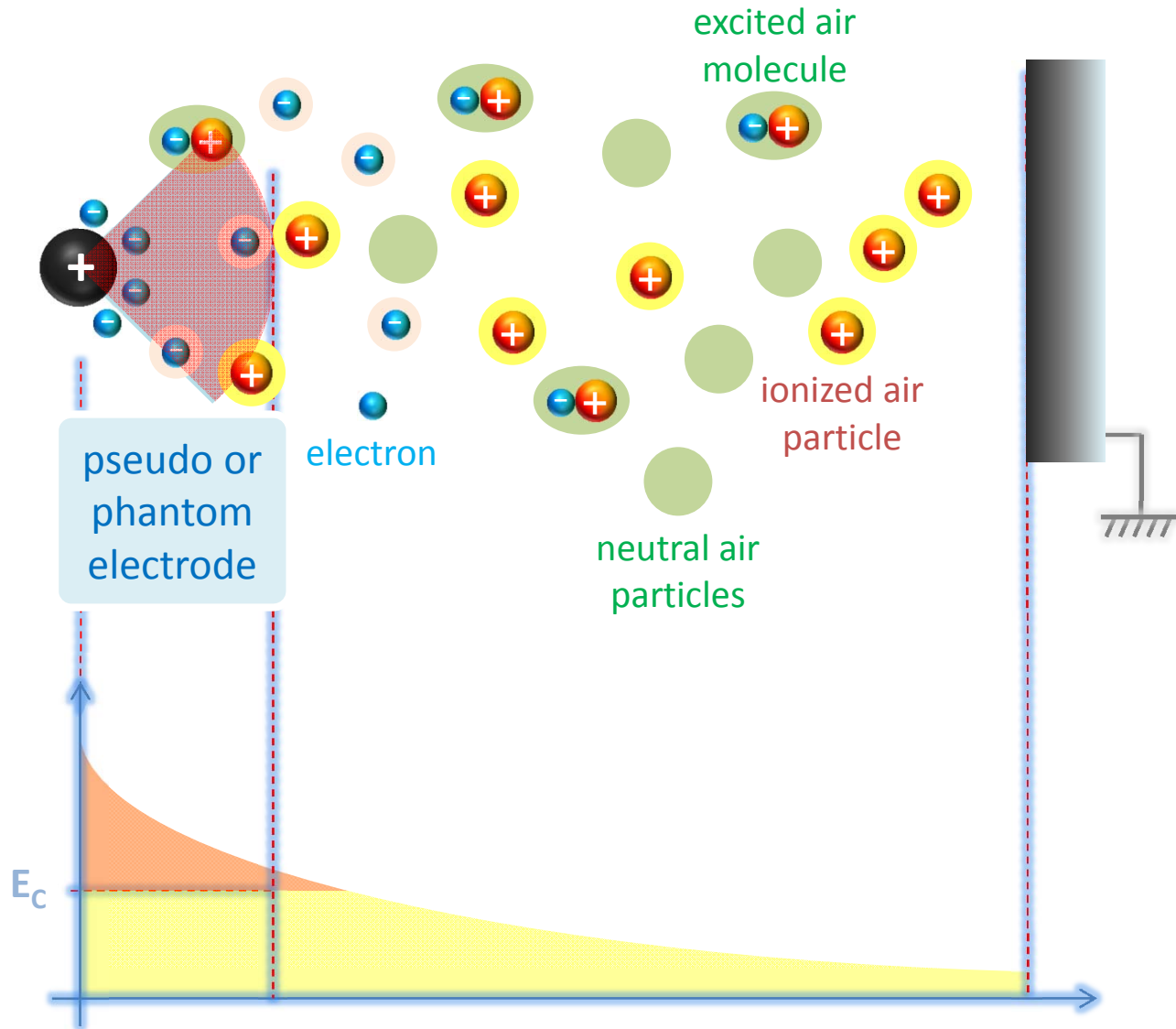


# electrical breakdown in gases, i.e., clearances

typically takes more than  $100 \mu\text{s}$  to develop.

- power frequency (10 ms):
  - a.c. (peak) and d.c. are virtually identical (98.77%).
- high frequencies ( $16.7 \mu\text{s}$ ):
  - insufficient time to constitute complete breakdown.





if the clearances are large or at high frequencies, the ions might get trapped, resulting in the gradient distortion and consequent field strength weakening.

# SOLID INSULATION





figure C.3 — breakdown at high frequency, solid insulation;  $d = 0.75$  mm; comparison on short-time breakdown field strength  $E_b$ :

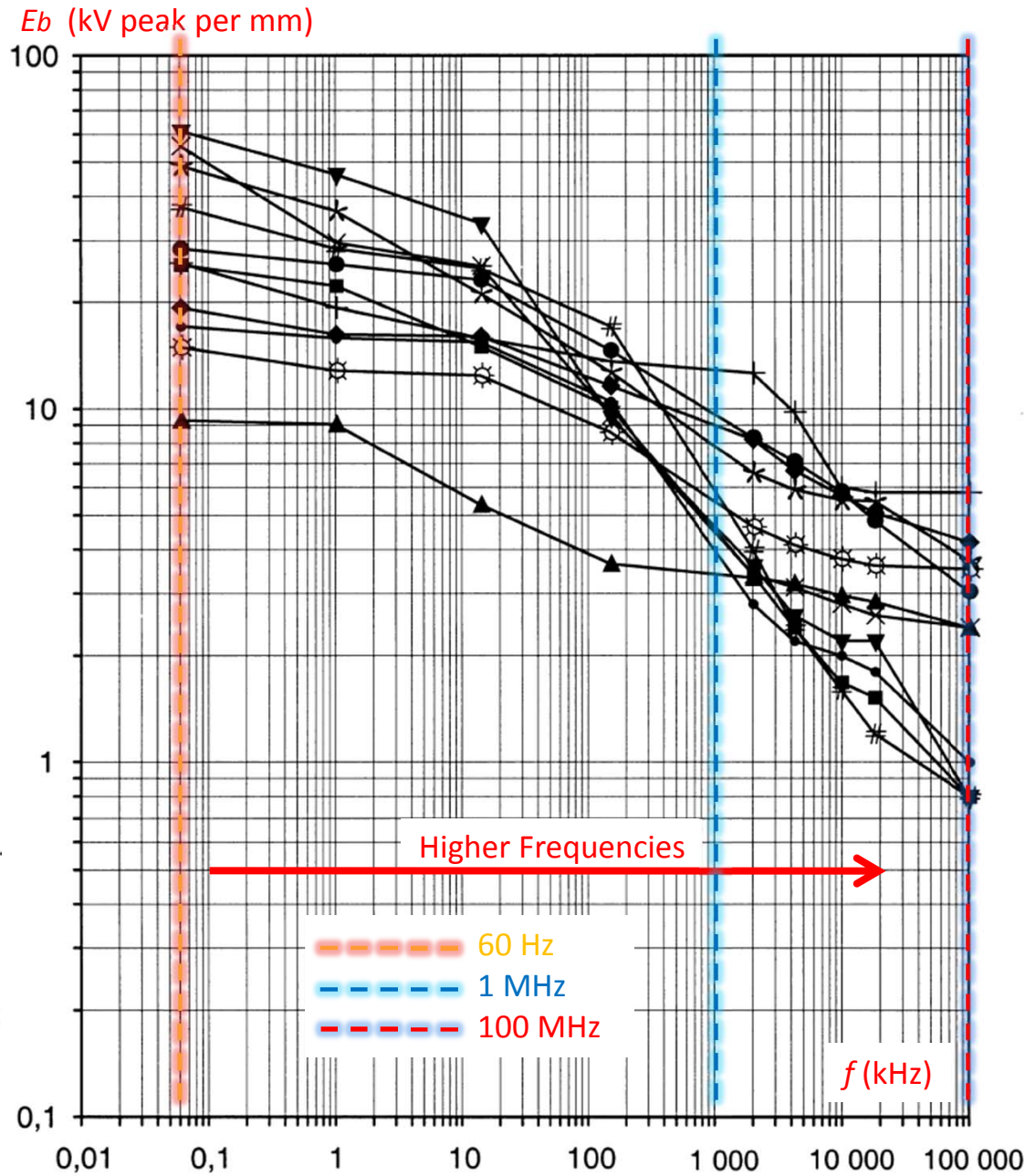
50/60 Hz = 1

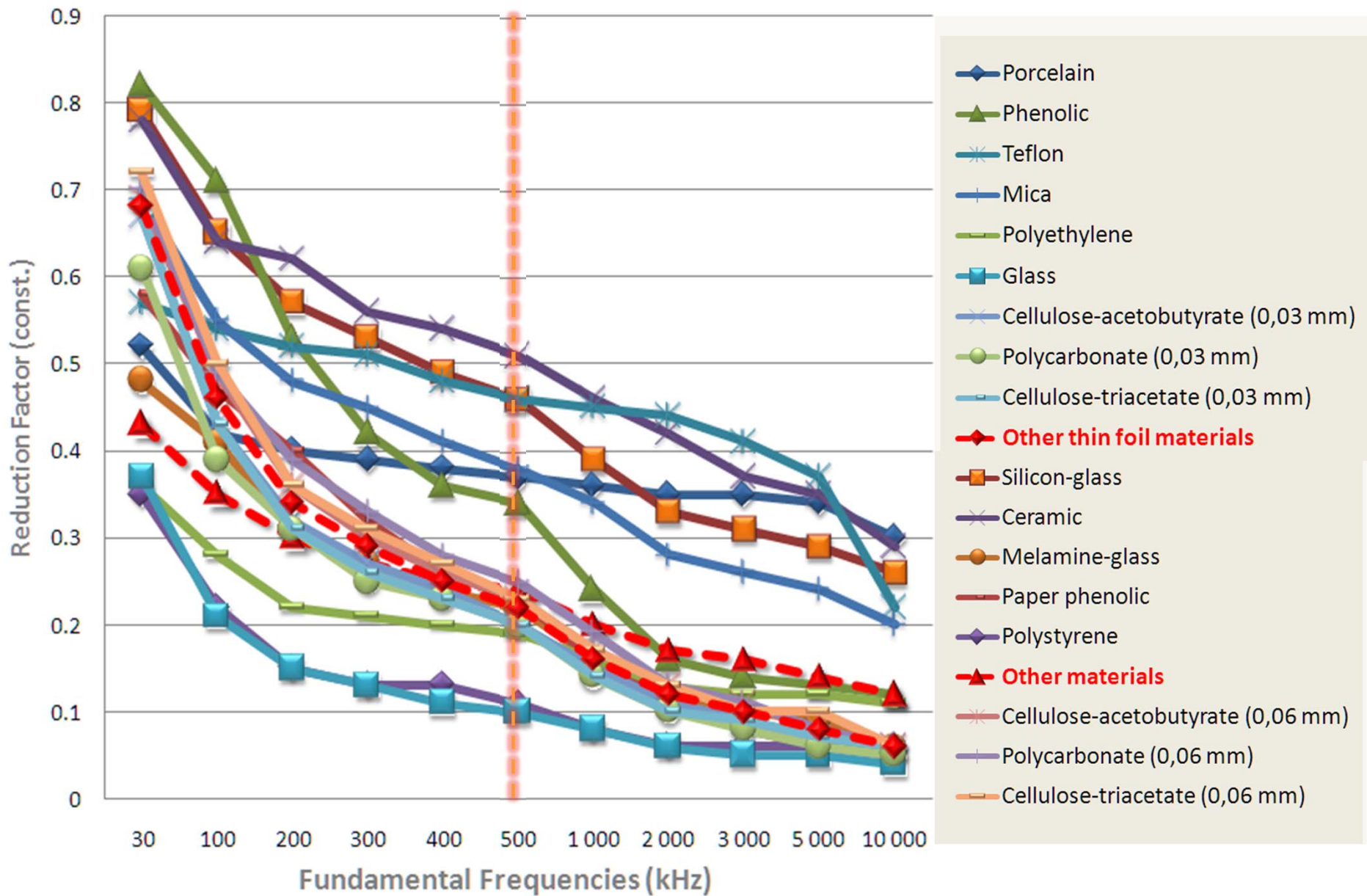
1 MHz = 0.66

100 MHz = 0.013

the bottom has not yet been reached!?

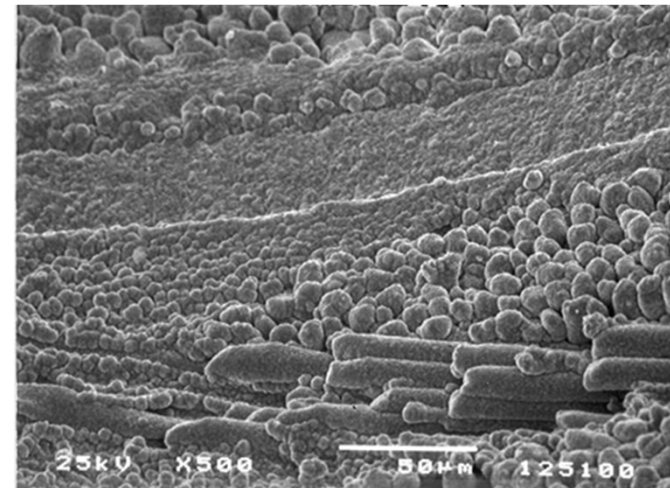
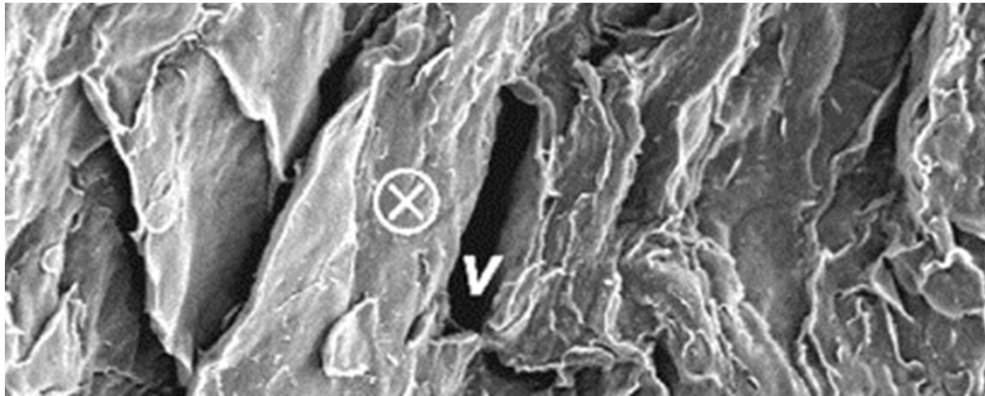
- PHENOLIC      ▮ TEFLON      ✱ POLYETHYLENE
- MICA          ▽ GLASS      ☼ SILICONE-GLASS
- ✕ POLYSTYRENE   ▾ CERAMIC   ▴ PORCELAIN
- ▮ MELAMINE-GLASS   # PAPER-PHENOLIC





# solid insulation

- compared to air insulation, solid insulation provides at least a **ten-fold** increase in electric strength.
- however, in practice, a PD can occur in embedded voids or air gaps in solid dielectrics at a PD-inception voltage **far below** its breakdown voltage, reducing its voltage withstand ability, and likely resulting in the complete destruction of most solid dielectrics.



# modeling a gas-filled void

$$C = \epsilon_r \epsilon_0 \frac{A}{d}$$

- $\epsilon_r$  (air) = 1.0006;
- $\epsilon_r$  (PC, polycarbonate) = 2.3;
- $\epsilon_r$  (FR-4) = 4.4;

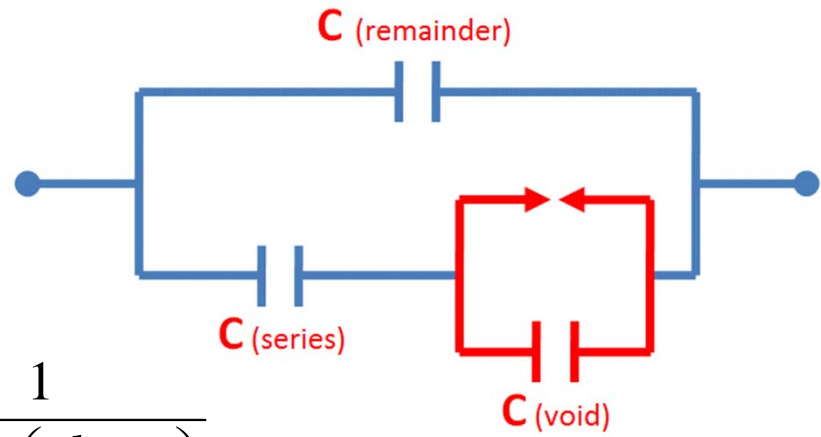
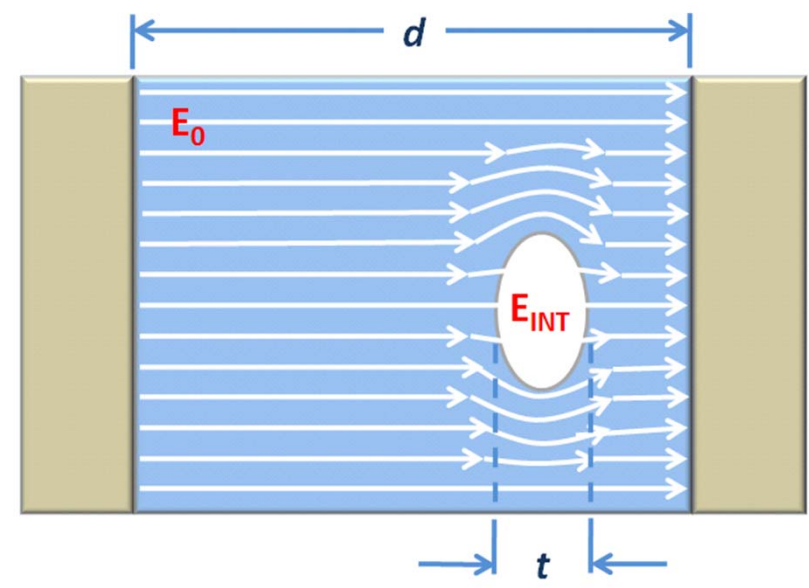
$$C_{(remainder)} \gg C_{(void)}$$

$$C_{(void)} \gg C_{(series)}$$

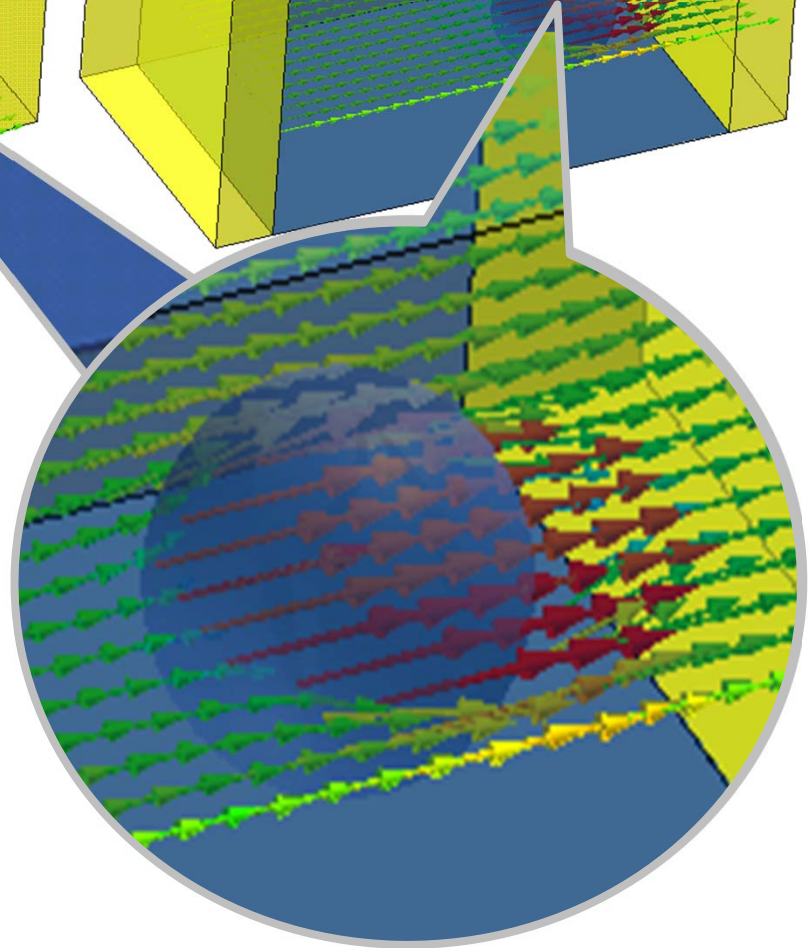
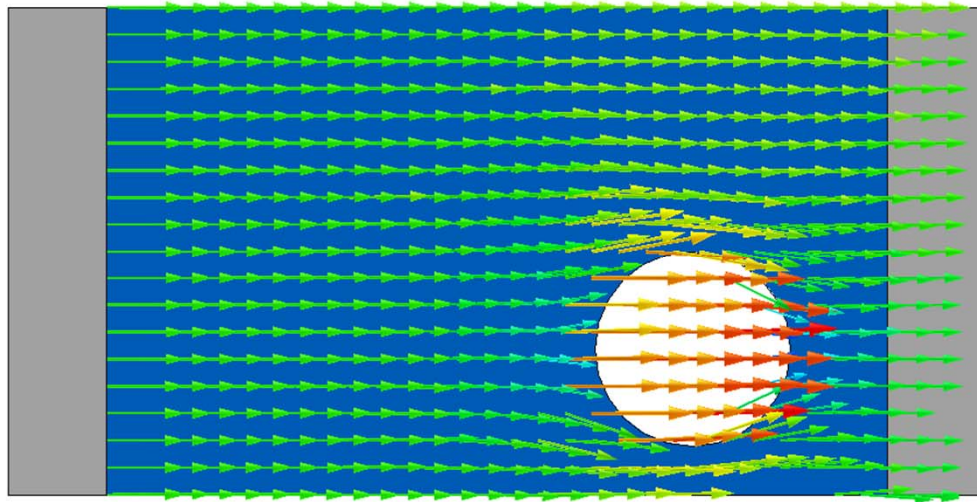
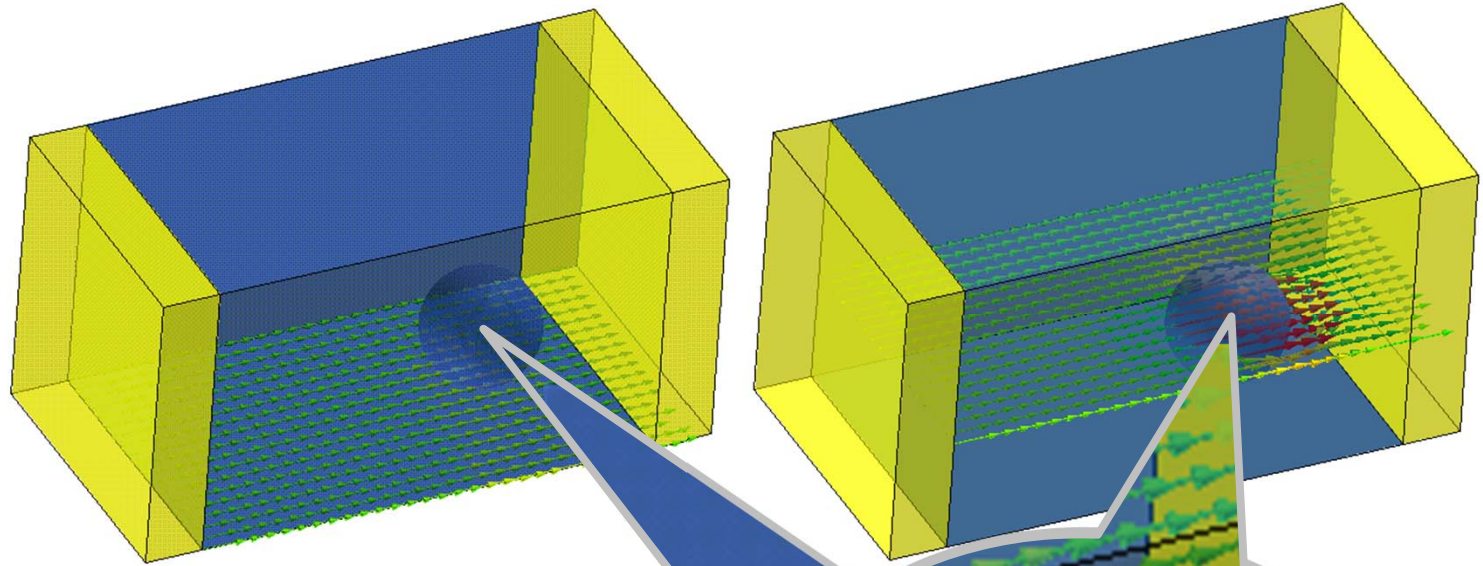
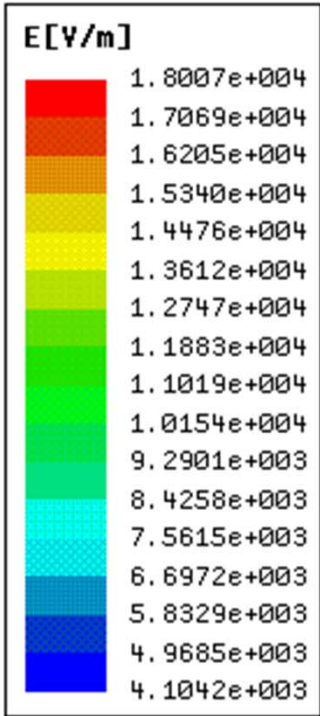
for any dielectric of the same size:

$$V_{(void)} = \epsilon_r * V_{(dielectric)}$$

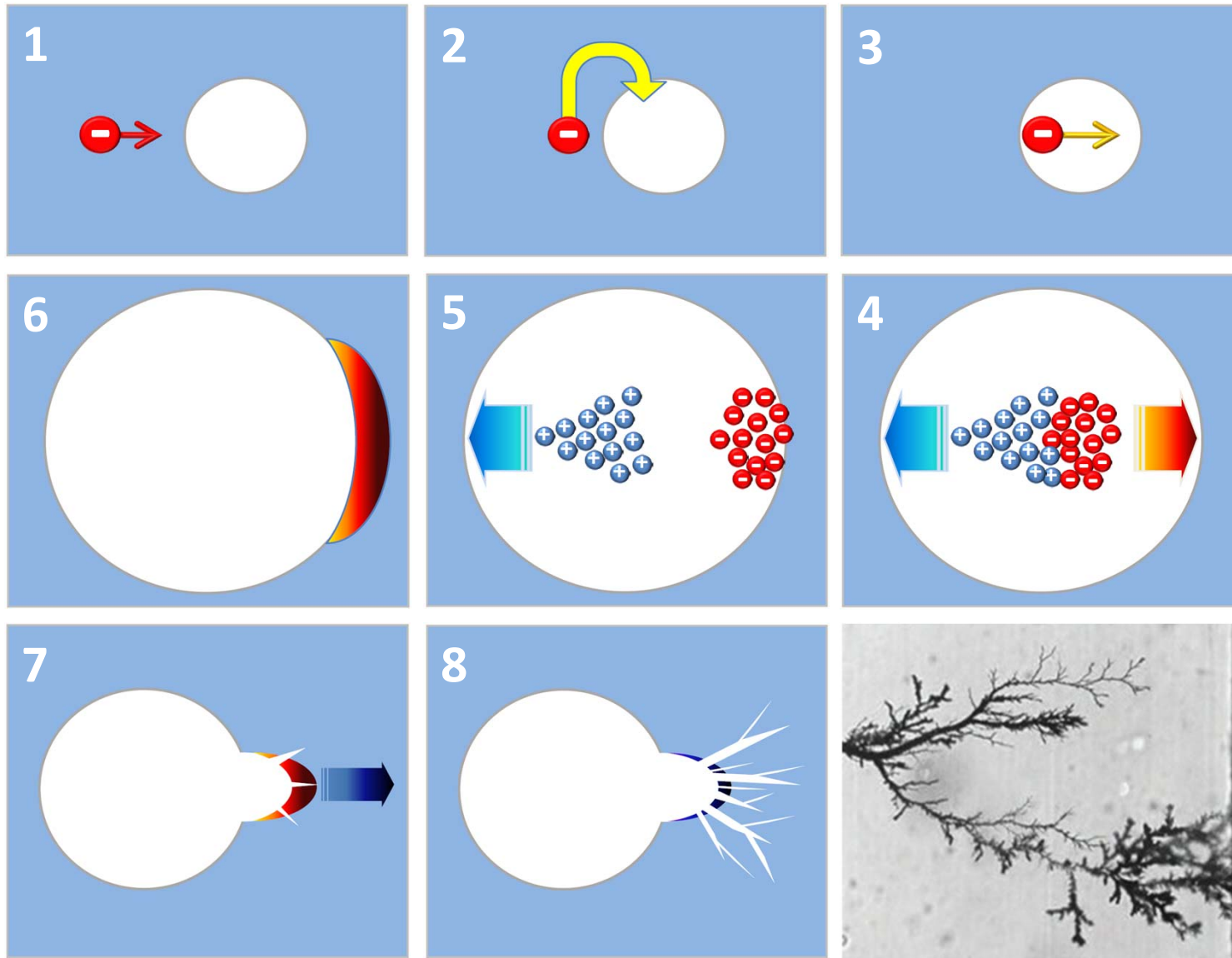
$$V_{(void)} = V \frac{C_{(series)}}{C_{(series)} + C_{(void)}} = V \frac{1}{1 + \frac{1}{\epsilon_r} \left( \frac{d}{t} - 1 \right)}$$



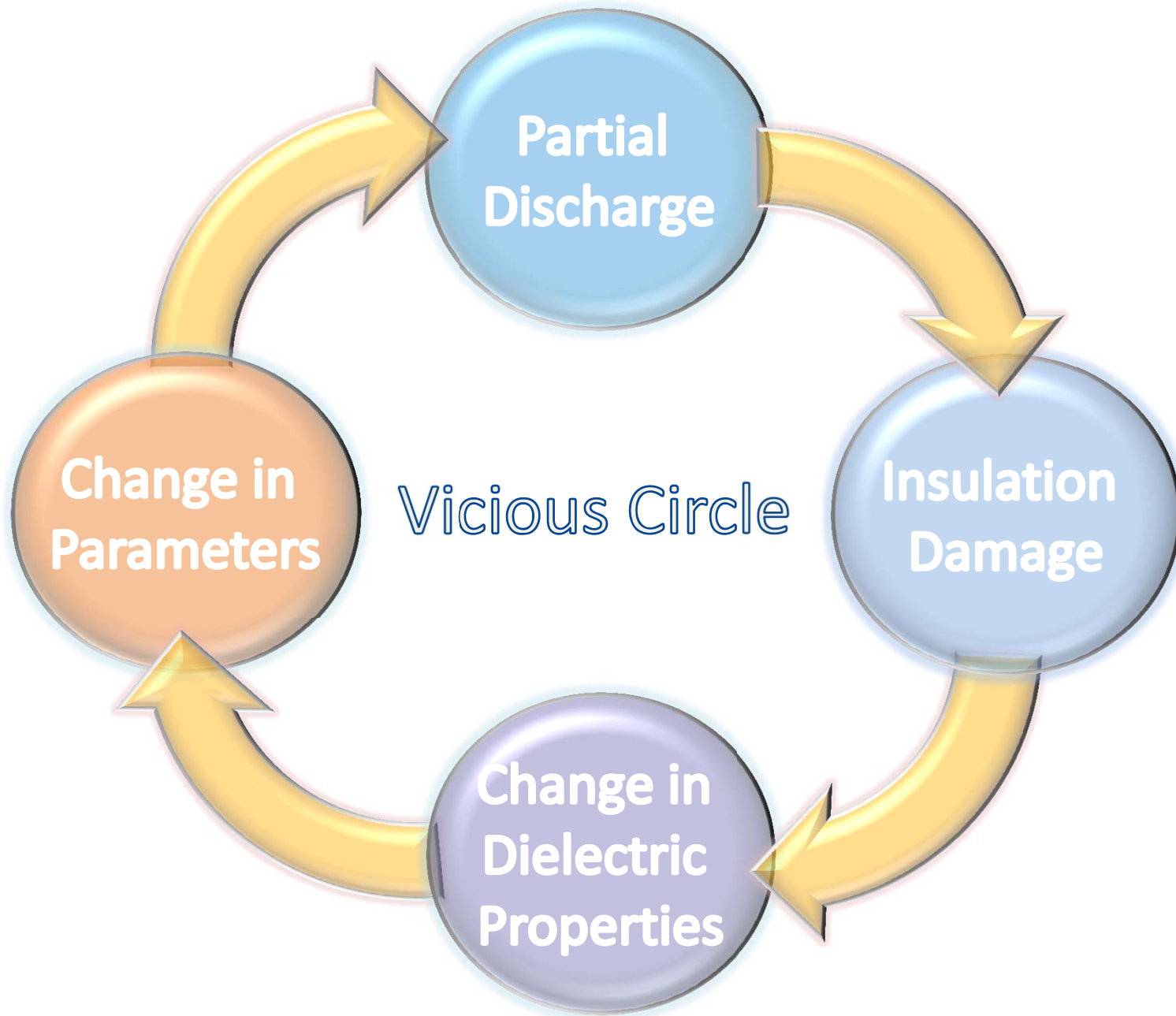




# void-to-tree transition



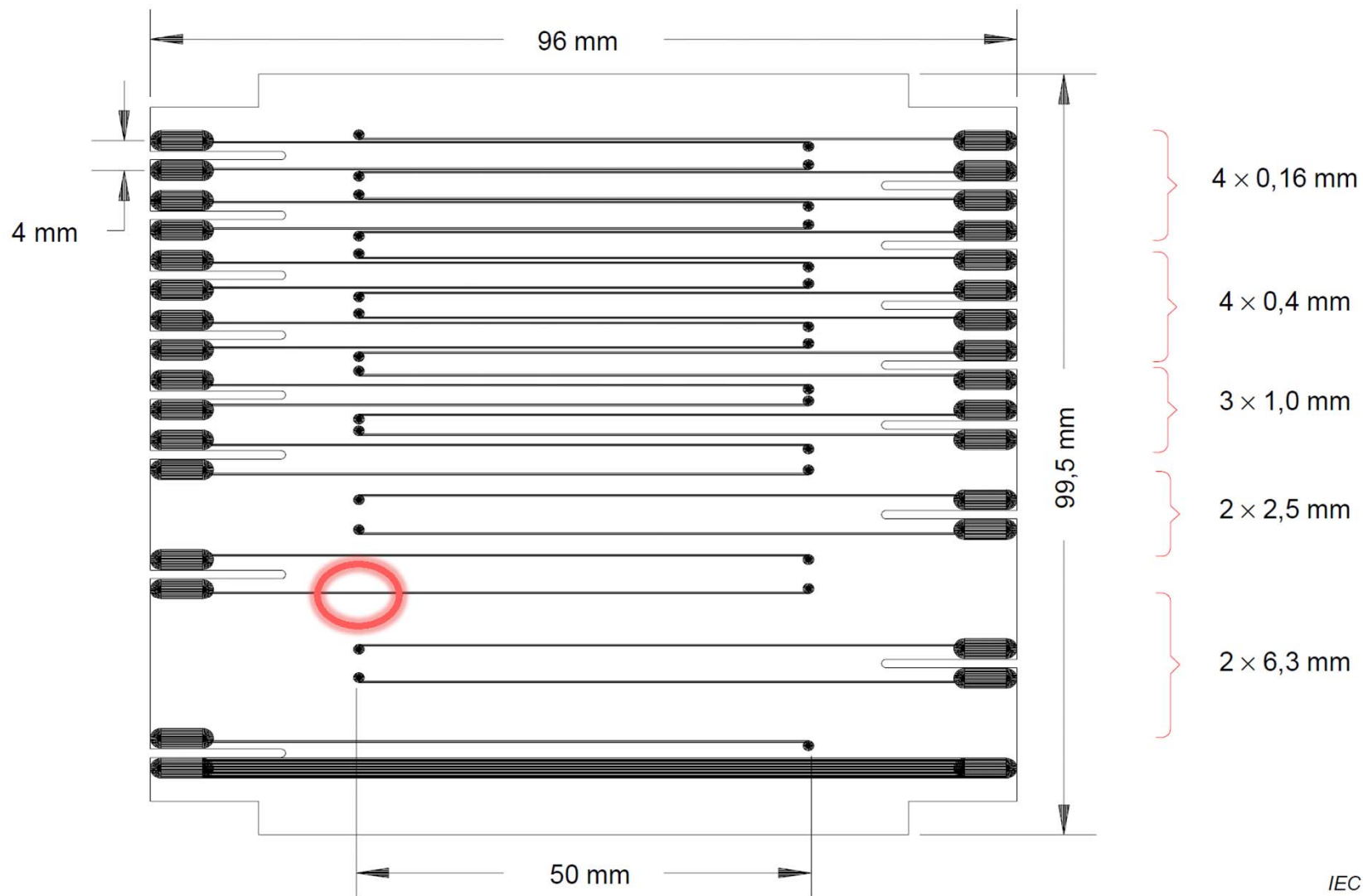




# CREEPAGE DISTANCES



# the experiment



# Figure B.3 — Breakdown Voltage ( $U_b$ )

$U_b$  is less relevant to frequency factor

larger creepage distances do not add to the breakdown voltage,  $U_b$

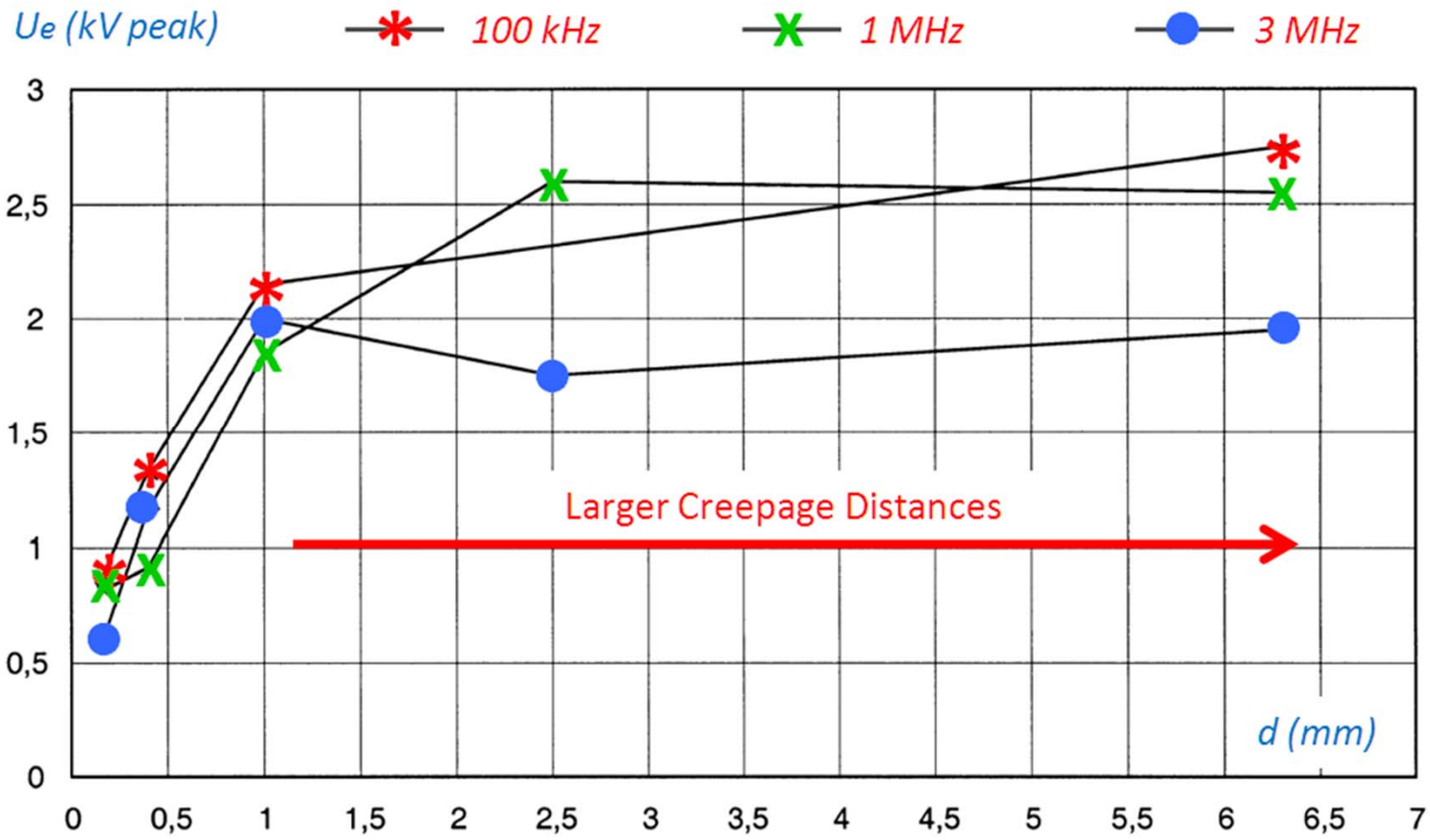
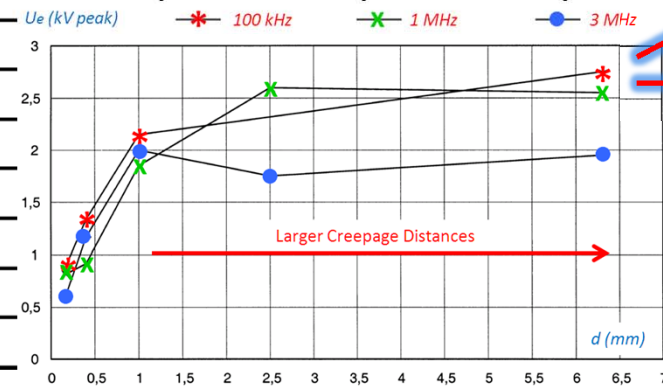
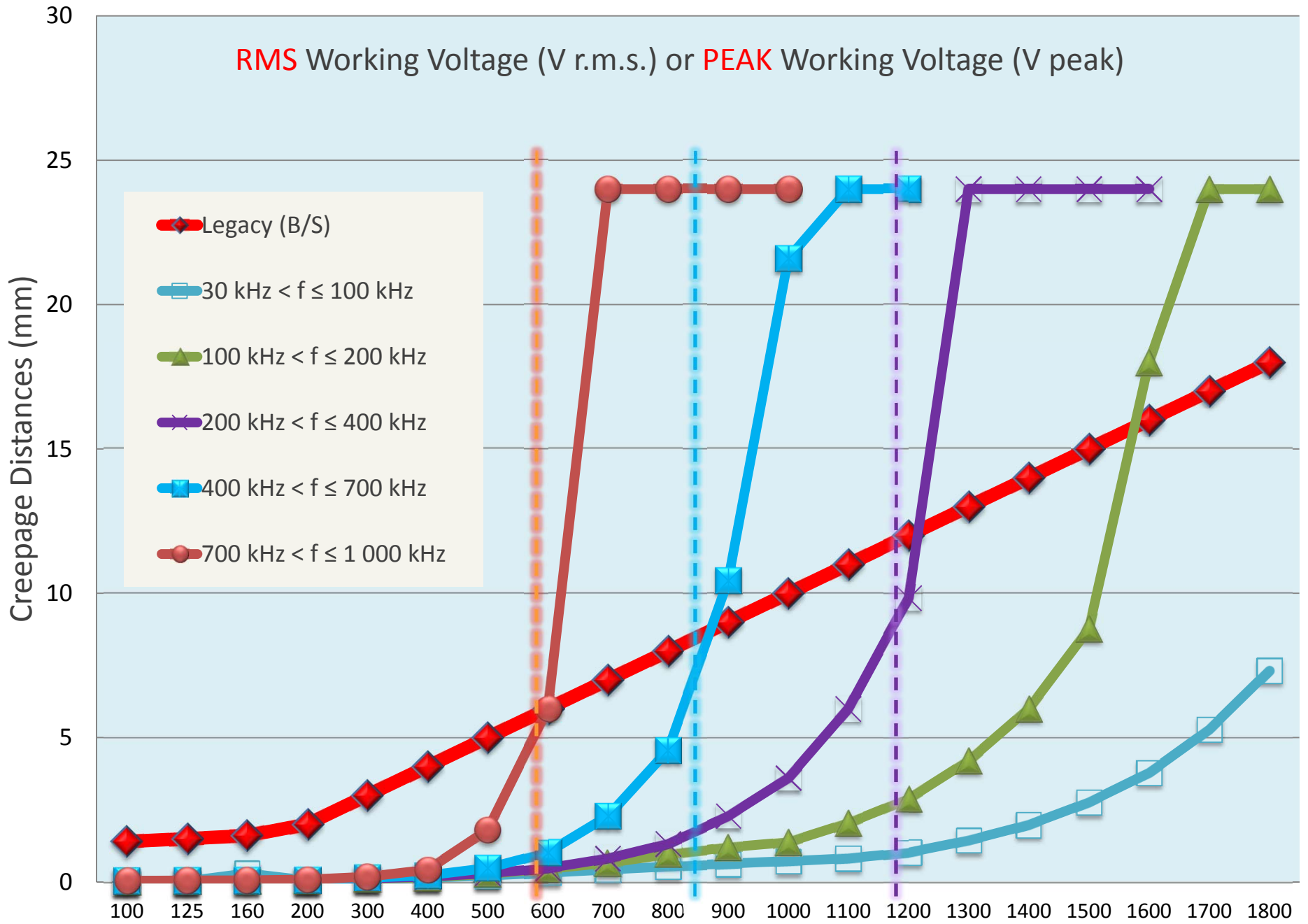


Table 2 – Minimum values of creepage distances for different frequency ranges

Voltage $U_{peak}$ kV	Creepage distance a) mm						
	for $30\text{ kHz} < f \leq 100\text{ kHz}$	for $f \leq 0,2\text{ MHz}^{b)}$	for $f \leq 0,4\text{ MHz}^{b)}$	for $f \leq 0,7\text{ MHz}^{b)}$	for $f \leq 1\text{ MHz}^{b)}$	for $f \leq 2\text{ MHz}^{b)}$	for $f \leq 3\text{ MHz}^{b)}$
0,1	0,0167						0,3
0,2	0,042					0,15	2,8
0,3	0,083	0,09	0,09	0,09	0,09	0,8	20
0,4	0,125	0,13	0,15	0,19	0,35	4,5	
0,5	0,183	0,19	0,25	0,4	1,5	20	
0,6	0,267	0,27	0,4	0,85	5		
0,7	0,358	0,38	0,68	1,9	20		
0,8	0,45	0,55	1,1	3,8			
0,9	0,525	0,82	1,9	8,7			
1	0,6	1,15	3	18			
1,1	0,683	1,7	5				
1,2	0,85	2,4	8,2				
1,3	1,2	3,5					
1,4	1,65	5					
1,5	2,3	7,3					
1,6	3,15						
1,7	4,4						
1,8	6,1						



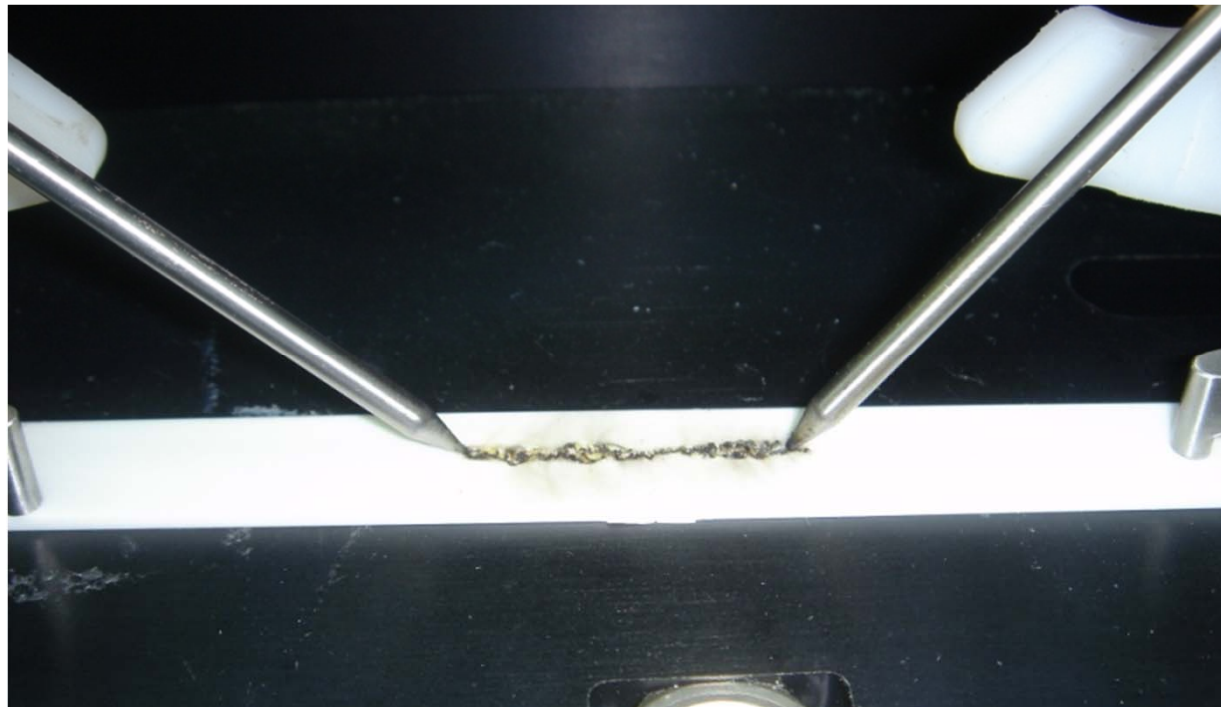




## surface breakdown, i.e., creepage distances

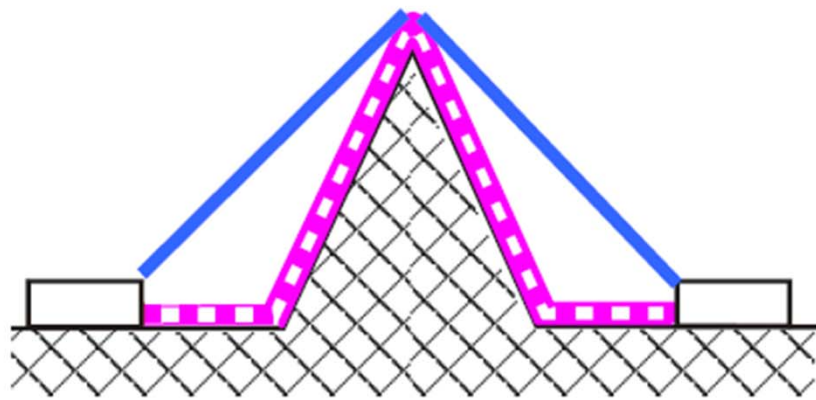
unlike clearances, creepage distances and solid insulation are **NOT** replenishable — permanent damage such as puncture or carbonized tracking, is likely.

- in this sense, clearances are less vulnerable to PD.

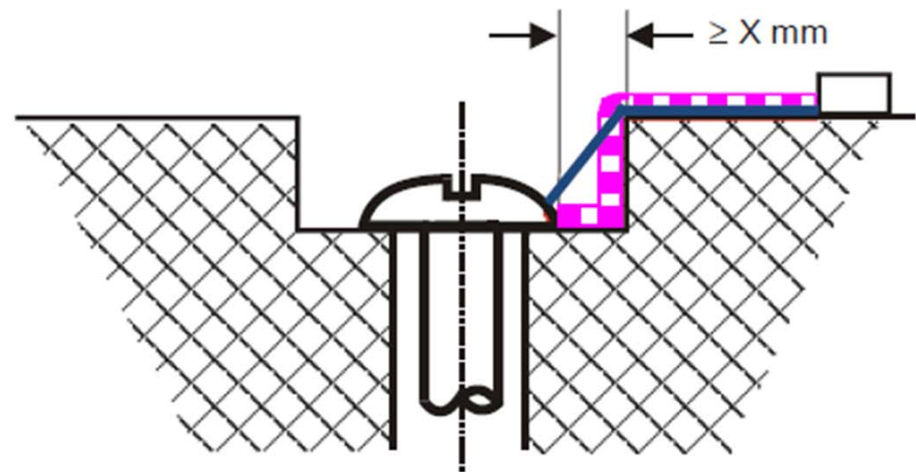


please humor me while I speculate...

what does it mean by saying **“creepage distances must be equal to or greater than clearances?”**



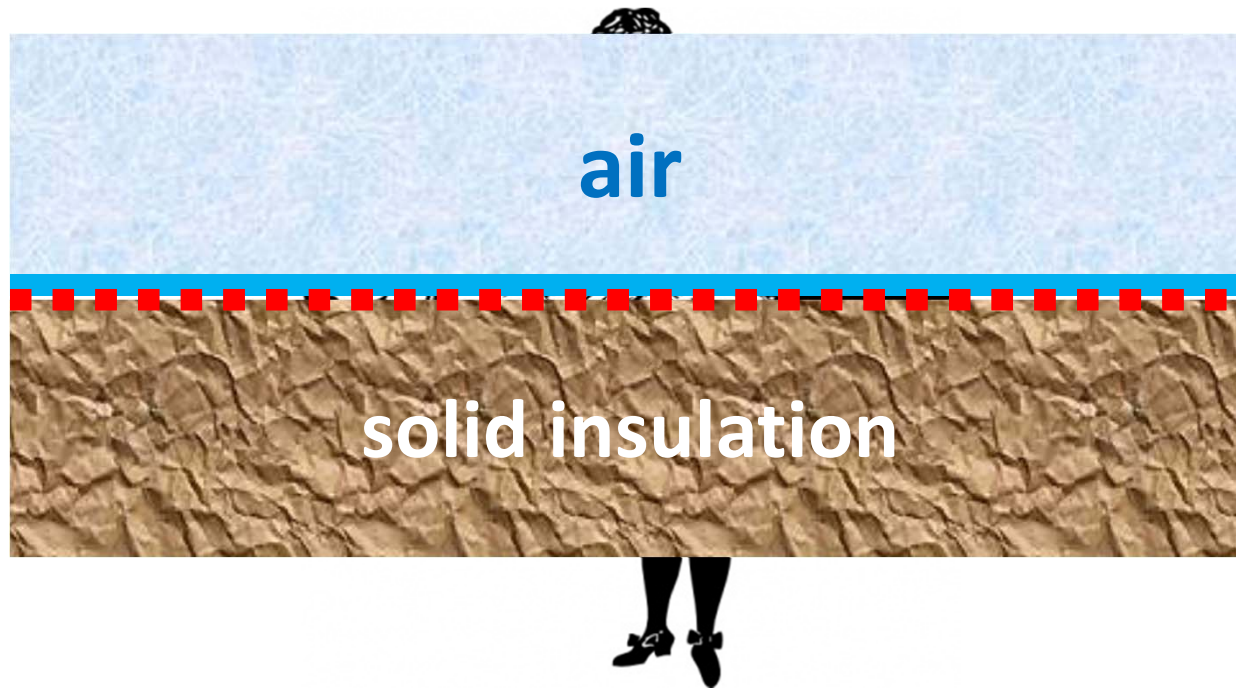
**geometry?**



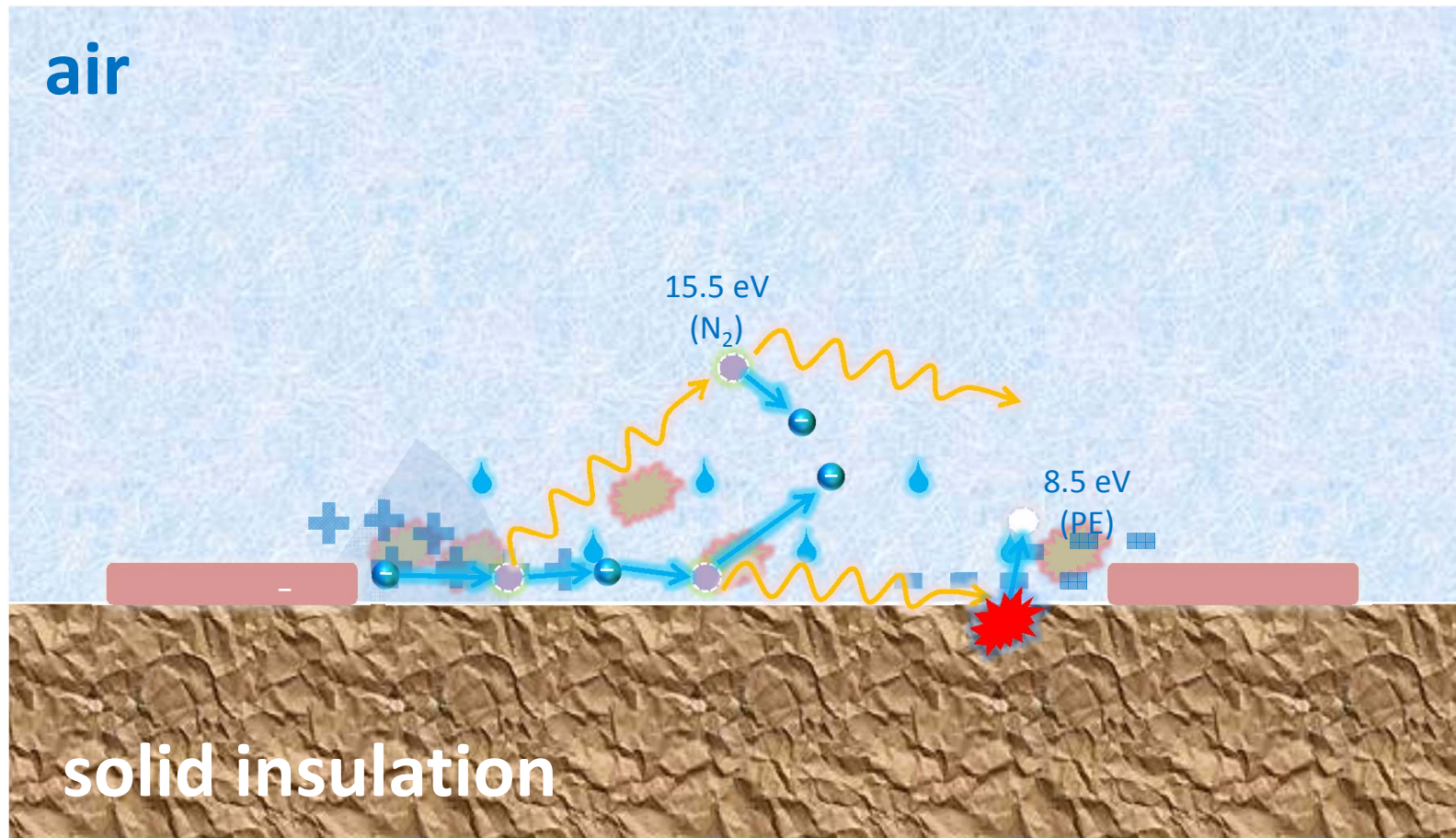
however,  
from this aspect it is difficult to understand  
what is the relationship between CL and CR.



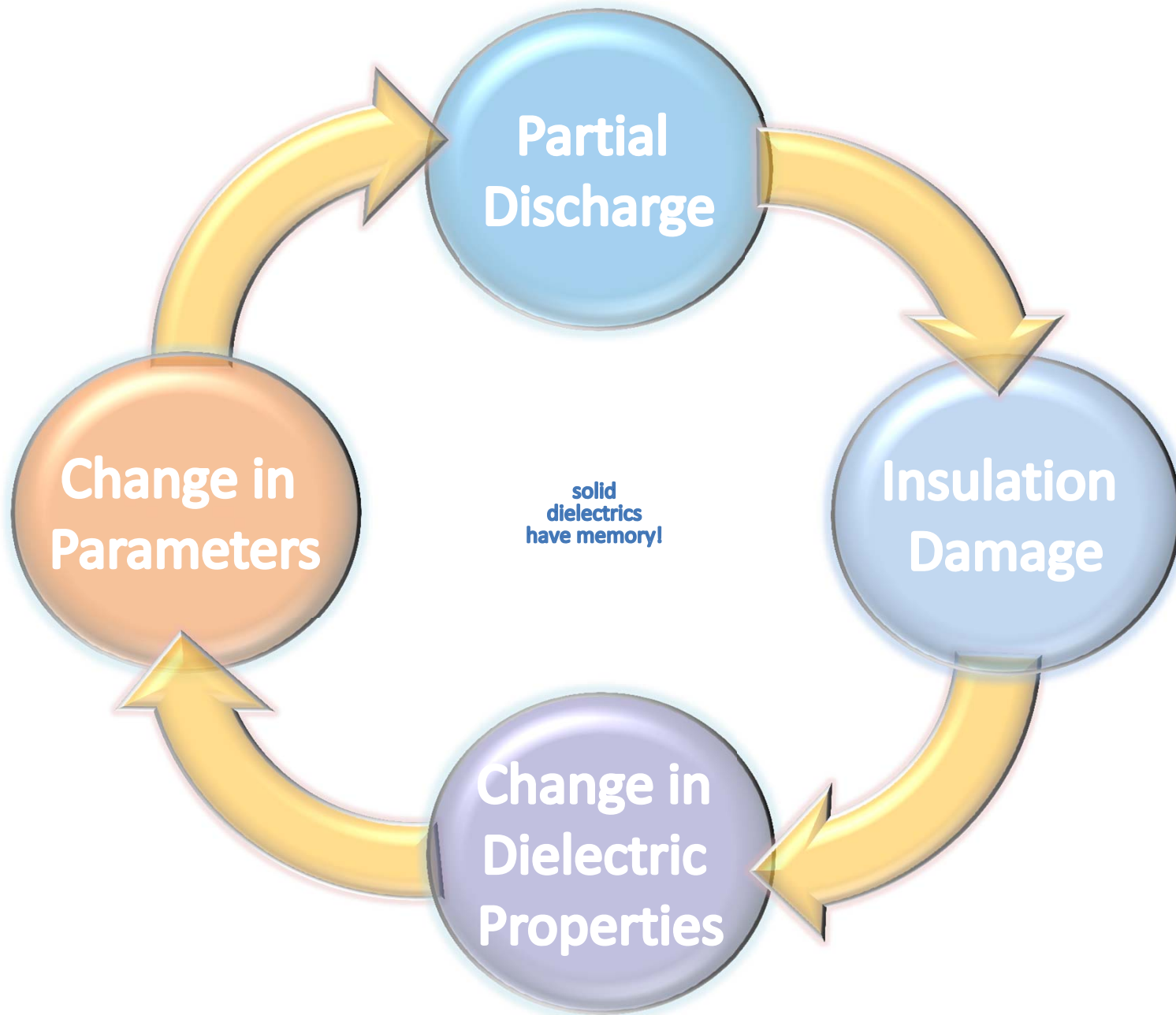
I would say when we're talking about the **creepage distances** we have to keep in mind that we're talking about **clearances** as well.



# how creepage distances and clearances interact with each other?









Product Safety Engineering Society  
**Taipei Chapter**

謝謝大家的時間！

