

NEC Mandated Selective Coordination

Challenges and Solutions

IEEE IAS Meeting May 16, 2011



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Background and Definitions



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Selective Coordination & The National Electrical Code

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|---------|---|-----------|--------|--------|--------|--------|---------------------|
| Article | Title | 1993 | 1996 | 1999 | 2002 | 2005 | 2008 |
| 100 | Definitions | | | | | * | |
| 517 | Healthcare Facilities | | | | | 517.26 | 517.26 |
| 620 | Elevators, Dumbwaiters, Escalators, Moving Walks, Wheel Chair Lifts, and Stairway Chair Lifts | 620.51(a) | 620.62 | 620.62 | 620.62 | 620.62 | 620.62 |
| 700 | Emergency Systems | | | | | 700.27 | 700.27 Exception |
| 701 | Legally Required Standby Systems | | | | | 701.18 | 701.18 Exception |
| 708 | Critical Operations Power Systems (COPS) | | | | | | 708.54 |

No significant changes to Selective Coordination in 2011 National Electrical Code



Selective Coordination -Background

- 2005 National Electric Code (NEC) Article 100 definition "Coordination (Selective)":
 - "Localization of an overcurrent condition to restrict outages to the circuit or equipment affected, accomplished by the choice of overcurrent protective devices and their ratings or settings."

Simply stated: When ONLY the overcurrent device protecting the specific circuit that has an overload or fault opens to clear it.



Selective Coordination - Background

- Required for Elevators since 1993 NEC.
- Added to 2005 NEC for Emergency Systems (Art. 700.27) and Legally Required Standby Systems (Art. 701.18).
- When accepted into 2005 NEC Article 700, by omission it became a requirement for "Essential electrical systems" of Health Care Facilities (Art. 517.26) as well.



Selective Coordination Challenges

- Interpretation
- Design
- Enforcement



Challenge - Interpretation

- Which Devices are Required to be Selectively Coordinated?
 - 700.27 states, "Emergency system(s) overcurrent devices shall be selectively coordinated with all supply side overcurrent protective devices."
 - Similarly, 701.27 states, "Legally required standby system(s) overcurrent devices shall be selectively coordinated with all supply side overcurrent protective devices."



Which devices are required to be Selectively Coordinated?



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Powering Business Worldwide

Which devices are required to be Selectively Coordinated?





Which devices are required to be Selectively Coordinated?

- Answer: It is up to the Authority Having Jurisdiction (AHJ).
 - Jurisdictions with written clarification for Generator Side only: Chicago, Las Vegas, State of Oregon, State of Washington*, State of Wisconsin
 - Jurisdictions rumored to be requiring coordination up to the Normal Source: Charlotte, NC
 - Actual intent of the NEC is somewhat unclear



Challenge - Interpretation

- What level of Selective Coordination is required?
 - Total Selective Coordination
 - 0.01 seconds
 - 0.1 seconds



What Level of Selective Coordination is Required?

- Reasons for Considering 0.1 or 0.01 seconds instead of Total Selective Coordination*
 - Achieving total selective coordination may be nearly impossible for certain systems
 - Achieving total selective coordination may result in undesirable levels of arc flash energy
 - Verification of total selective coordination is difficult.
 - Some jurisdictions have defined a time cut-off for selective coordination

* Choosing a level other than total selective coordination without AHJ approval is risky.



What Level of Selective Coordination is Required?

- Some jurisdictions have defined a level of 0.1 or 0.01 for selective coordination*
 - State of California Healthcare (OSHPD) 0.1
 - State of Florida Healthcare (AHCA) 0.1
 - City of Memphis 0.1
 - Las Vegas 0.01, 0.1 allowable if 0.01 can not be achieved
 - State of Oregon 0.01
 - City of Seattle 0.1
 - NFPA 99 (pending) 0.1
 - But not Georgia...

* This list is subject to change and should always be verified with the AHJ



What Level of Selective Coordination is Required?

- What do these time limits mean in the real world?
 - Design to worst case fault currents bolted fault
 - Most real world faults are lower level arcing faults or ground faults
 - Coordination down to 0.01 seconds allows coordination for all but the highest levels of fault current
 - Coordination down to 0.1 seconds allows coordination for overloads and typical arcing fault levels



What Do These Time Limits Mean in the Real World?



CURRENT IN AMPERES

What Do These Time Limits Mean in the Real World?



CURRENT IN AMPERES



16

Beyond the Curves - Manufacturer's Tables





Challenge - Design

• How Do I Design a System that can be Coordinated?



Selective Coordination

- Design Tips
 - 1. Flatten the system
 - Limit the number of levels of OCPD's
 - Reduces the number of potential coordination problems
 - Limit levels of 480v devices to (3)
 - Depending on fault current, 1st and 2nd levels may need to be Power Circuit Breakers (UL1558 Switchgear)
 - Distribution Panels
 - If possible, avoid 277v lighting
 - Otherwise, don't locate lighting panels in same room as Distribution panels
 - Or, utilize isolation transformers to knock down fault current



Selective Coordination

2. Transformer Breakers

- Do not size primary transformer breakers at 125%
- NEC allows primary up to 250%
 - NOTE: This changes the cable size required
- 480v primary breakers need to be sized around 200%
 - Problem is not with 208v secondary breaker, but with the next level branch breakers (BAB)
- Always size secondary breakers to 125% (and round up)
 - NEC 450-3(B) allows you to round up to the next standard rating
 - Needed to allow coordination between secondary main and feeders



Simplified One-Line



Simplified One-Line – Fault Currents



Simplified One-Line – System Cost – Standard Devices



Simplified One-Line – Device Selection



| × / | Microsoft Excel | - Selectiv | e Coordinatio | n Tables R3 - 4-1-2011.xls | 3 | | | | | | | | | | | | | | d X | |
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| 2 | | | | | Line Side Brea | ker (Standard | d and Curre | nt Limiting | Frames |) | | | | | 1 | | | | | |
| Upstream Breaker | | | | | | | | | | | | | | | | | | | | |
| 4 | | | | Duralise Familie a | EG | F | F | F | F | F | F | J | J | J | К | К | K | K | ŀ | |
| 5 | | | | Breaker Family -> Type Trip Unit -> | T/M | Т /М | T/M | T/M | ETU | ETU | ETU | T/M | T/M | T/M | T/M | T/M | T/M | ETU | El | |
| 6 | | $\langle \rangle$ | | Digitrip RMS Trip Unit -> | | - | - | - | 310+ | 310+ | 310+ | () | - | - | | | _ | 310 | 31 | |
| 7 | | | | Optim Trip Unit -> | _ | - | — | | — | | | - | — | - | 701 0 | = | _ | 550, 1050 |) 550, | |
| 8 | | | <u> </u> | Minimum Trip (Plug/Trip) -> | 125A | 100A | 150A | 225A | 15A | 60A | 100A | 70A | 150A | 250A | 100A | 200A | 400A | 70A | 12 | |
| 9 | Downstream | n | | Maximum Trip (Frame) -> | 125A | 100A | 200A | 225A | 80A | 160A | 225A | 125A | 225A | 250A | 175A | 350A | 400A | 125A | 25 | |
| 10 | Breaker | | \sim | Pow-R-Line : Main - > | 3E | ţ | | 1a,2a,3a,3 | 3E — | | + | - | За | | • | | <u> </u> | ,2a,3a,3E,4 | | |
| 11 | L | | \ | Pow-R-Line : Branch -> | 3E | + | | 3a,4,Swb | <u>d — </u> | | | - | 4,Swbd | \rightarrow | • | | <u> </u> | 4,Swbd | | |
| 12 | | (10 kA at 240v | ac) 1 2 and 3 Pole | PowR-Line : Sub-Feed -> | | - | | 1a,2a,3E | <u> </u> | | | <u> </u> | 38 | | - | | | a,2a,3a,3E | | |
| 13 | DR, DAD, HQF and QC | (10 KA at 240V | Pow-R-Line P | anelboard / Swbd | | | | | | | | | | | | | | | | |
| 15 | | Main | Branch | Sub-Feed | | | | | | | | | | | | | | | | |
| 16 | 15 | | 1a,3a,4, Swbd | | 1.2 | 1.0 | 1.5 | 2.2 | 0.6 | 1.2 | 2.3 | 1.0 | 2.1 | 4.0 | 2.5 | 5.0 | 10 | 8.0 | 6 | |
| 17 | 20 | 8 1 - 14 | 1a,3a,4, Swbd | 3 1 1 7 | 1.2 | 1.0 | 1.5 | 2.2 | 0.6 | 1.2 | 2.3 | 1.0 | 2.1 | 3.4 | 2.0 | 4.0 | 8.0 | 2.5 | 5 | |
| 18 | 30 40 | _ | 18,38,4, SWD0 18,38,4 Swbd | | 1.2 | 1.0 | 1.0 | 22 | 0.0 | 1.2 | 23 | 0.7 | 15 | 34 | 2.0 | 4.0 | 8.0 6.0 | 15 | с И | |
| 20 | 50 | | 1a,3a,4, Swbd | | 0.8 | - | 1.5 | 2.2 | | 1.2 | 2.3 | - | 1.5 | 2.5 | 1.2 | 3.0 | 6.0 | 1.5 | 4 | |
| 21 | 60 | 1a | 1a,3a,4, Swbd | a . 1 7 | 0.8 | 87.57 | 1.5 | 2.2 | | 1.2 | 2.3 | - | 1.5 | 2.5 | 000000 100000 | 3.0 | 6.0 | 1.5 | 4 | |
| 22 | 70 | 1a | 1a,3a,4, Swbd | — | (<u></u> | — | 1.5 | 2.2 | <u></u> 2 | 1.2 | 2.3 | <u></u> | 1.5 | 2.5 | | 2.5 | 5.0 | | 3 | |
| 23 | 80 | 1a 1- | 1a,3a,4, Swbd | | 1 | 37 77 7 | 6- 6 | 2.2 | 10 13 | | 2.3 | 10 -00 | | 2.5 | 10 - 10 F | 2.5 | 5.0 | 0-0 | 3 | |
| 24 | 90 | 18 19 | 1a,3a,4, Swbd | | _ | _ | _ | × 1.2 | | _ | × 2.3 | | _ | 2.3 | _ | 2.5 | 5.0 5.0 | _ | r 3 | |
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| 29 | brail, ai rin, abrin ai | | Pow-R-Line Pa | anelboard / Swbd | | | | | | | | | | | | | | | | |
| 30 | | Main | Branch | Sub-Feed | | | | | | | | | | | | | | | | |
| 31 | 15 | i. Tresh | 1a,3a,4, Swbd | 8 <u></u> 8 | 1.2 | 1.0 | 1.5 | 2.2 | 0.6 | 1.2 | 2.3 | 1.0 | 2.1 | 4.0 | 2.5 | 5.0 | 10 | 3.0 | 6 | |
| 32 | 20 | | 1a,3a,4, Swbd | - | 1.2 | 1.0 | 1.5 | 2.2 | 0.6 | 1.2 | 2.3 | 1.0 | 2.1 | 3.4 | 2.0 | 4.0 | 8.0 | 2.5 | 5 | |
| 33 | 30 | 17-14 | 1a,3a,4, Swbd | 3 | 1.2 | 1.0 | 1.5 | 2.2 | 0.6 | 1.2 | 2.3 | 0.7 | 2.1 | 3.4 | 2.0 | 4.0 | 8.0 | 2.5 | 5 | |
| 34 | 40 | | 1a,3a,4, Swbd | - | 0.8 | 1.0 | 1.5 | 2.2 | U.6 | 1.2 | 2.3 | | 1.5 | 3.4 | 1.2 | 3.0 | 6.0 | 1.5 • • • • | - 4 | |
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Simplified One-Line – LE1 Feeder Breaker Change



Simplified One-Line – Device Selection Continued



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| | $\langle \rangle$ | Breaker | → | | | | | | | | | and the | | | | | 1 | 1 | 福昌者 |
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| 3 | | \langle | | | | | 1 | K-Frame Breaker | | | | L-Frame Breat | kor | | | LG 600 Ampere Breaker | | | LG 600 Ampere |
| 4 | | | | Breaker Family -> | ĸ | ĸ | ĸ | ĸ | ĸ | ĸ | LD | LD | LD | LD | LHH | LHH | LHH | LG | LG |
| 5 | | $\langle \rangle$ | | Type Trip Unit -> | T/M | T/M | T/M | 210 | 210 210 | 210 210 | T/M | T/M | T/M | 210 210 | T/M | T/M | T/M | ETU 310+ | ETU 310+ |
| 0 | | | | Digitrip RMS Trip Unit -> | | | | 010 | 010 | .010 | | | 000 | 510 | 0 | | | 0101 | |
| | | | \backslash | Optim Trip Unit -> | 14 <u>-</u> 74 | (<u>)</u> | | 550, 1050 | 550, 1050 | 550, 1050 | 17 | 17-11 | 17 | 550, 1050 | 10 | | 9 <u>7</u> 72 | | - |
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| 8 | | | $\overline{\}$ | Minimum Trip (Plug/Trip) -> | 100A | 200A | 400A | 70A | 125A | 200A | 300A | 400A | 600A | 300A (Digi) | 125A | 175A | 225A | 100A | 160A |
| 9 | Downstrean | 1 | \sim | Maximum Trip (Frame) -> | 175A | 350A | 400A | 125A | 250A | 400A | 350A | 500A | 600A | 600A | 150A | 200A | 400A | 250A | 400A |
| 10 | Breaker | | $\overline{)}$ | Pow-R-Line : Main -> | - | | 1a | | | - | | | +,5Wbd - | | + | 1a,2a,3a,3⊟,4 | \rightarrow | _ | 2 |
| 12 | ł | | \backslash | PowR-Line : Sub-Feed -> | 4 | | 1; | 4,5%6u - | | | - | | | | - | 4,000u | | - | <u>- 4,5%</u> |
| 84 F | Family (FD, HFD, FD | C, FDB(150A), E | EHD(100A), FDE, HFI | DE, FDCE) | 1 | | | | | | | | | | | | | | |
| 85 | | | Pow-R-Line P | anelboard / Swbd | | | | | | | | | | | | | | | |
| 86 | 15 | Main | Branch | Sub-Feed | 2.0 | 25 | 5.0 | 25 | 4.0 | 5.0 | 10 | 10 | 10 | 10 | 7.5 | 14 | | 4.0 | 10 |
| 87 | 40 | | 3a,4,5wbu 3a,4,Swbd | | 1.6 | 2.5 | 5.0 | 2.5 | 4.0 • 0.2 | × 4.2 | 8.3 | 8.3 | 12 | 12 | 3.2 | 10 | 1 6 | 4.0 3.2 | 8.3 |
| 89 | 100 | 1a,2a,3a,3E | 3a,4,Swbd | 1a,2a,3a,3E | 800 | 2.3 | 3.2 | | 3.2 | 4.0 | 7.0 | 7.0 | 12 | 12 | 8 <u>110</u> 5 | 10 | 14 | 3.2 | 7.0 |
| 90 | 225 | 1a,2a,3a,3E | 3a,4,Swbd | 1a,2a,3a,3E | - | | 3.2 | 1 | | 4.0 | - | 7.0 | 12 | 12 | 10-00 | | 12 | | 7.0 |
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| 108 | 70 | - | 4,Swbd | | (| 2.0 | 3.2 | - | 2.5 | 4.0 | 6.0 | 8.0 | 12 | 12 | 3.2 | 7.6 | 12.7 | 2.8 | 8.0 |
| 109 | 125 | | 4,Swbd | 1- 0- 0- | | - ; | 3.2 | - | 2.5 | 3.7 | 6.0 | 7.0 | 12 | 12 | 5 | 7.6 | 10 | 2.8 | 7.0 |
| 110 | CL 250 Eamily Curren | Za,3a,4 | 4,5W00 | Ta,2a,3a | | | 3.2 | | | a.o | | 7.0 | 10 | 10 | _ | | 10 | | 7.0 |
| 112 | oc zoo r anny oarren | c Ennening | Pow-R-Line P | anelboard / Swbd | | | | | | | | | | | | | | | |
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| 118 | | | Pow-R-Line P | anelboard / Swbd | | | | | | | | | | | | | | | |
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Simplified One-Line – Device Selection Continued



Simplified One-Line – Generator Fault Currents



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| Note Note <th< td=""><td></td><td></td><td>Breaker</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<> | | | Breaker | | | | | | | | | | | | | | | | | | |
| Image: constraining range Provide range | | | | | | | | | | | (illingen) | | | (ataz u | | | | | | | |
| Image: Sub-State Family - by Type Trip Unit | 2 | | \backslash | | | | | 6. | | | 0:0:0 | | | 10:01 | | | · · · · | | A Frame Pres | | |
| Image: constraining function in the constrainin the constraining function in the constraining function in the | 4 | | $\langle \rangle$ | | Broaker Family - > | LD | LD | LD | LD | LHH | LHH | LHH | LG | LG 600 Ampe | LG | LG | NHH | N | N | N | N |
| 1 Digiting Prixes Trig Lunk+> - | 5 | | $\langle \rangle$ | | Type Trip Unit -> | T/M | T/M | T/M | ETU | T/M | T/M | T/M | ETU | ETU | ETU | T/M | ETU | ETU | ETU | ETU | ETI |
| Opwinstream | 6 | | / | | Digitrip RMS Trip Unit -> | 1 | 1 | - | 310 | - | | - | 310+ | 310+ | 310+ | (<u></u>) | 310 | 310 | 310 | 310 | <u>31C</u> |
| Vigue Vigue <th< td=""><td></td><td></td><td></td><td>\backslash</td><td>Ontim Trin Unit - ></td><td></td><td></td><td></td><td>550, 1050</td><td></td><td>17</td><td></td><td>1. <u></u>1.</td><td></td><td></td><td></td><td></td><td>550, 1050</td><td>550, 1050</td><td>550, 1050</td><td>550, 1(</td></th<> | | | | \backslash | Ontim Trin Unit - > | | | | 550, 1050 | | 1 7 | | 1. <u></u> 1. | | | | | 550, 1050 | 550, 1050 | 550, 1050 | 550, 1(|
| Image: Braker Minimum Trip (Pug/Trip) -> 300.4 600.4 600.4 500.4 | 7 | | | | Optim The One -> | | 50 Methode 1946 | TOWN NUMBER | 2004 (Ontim) | 1 | | NONOMINE | (13-32-4-17-45) | narester e co | N3510040 | 10/2419/2023 | Constantino - 10 | 1000 | 1000 | N2 94544 19 M | |
| Bownstream Maximum Trg (rame)-> 300A 300A 300A 300A 400A 400A 500A td>8</td> <td></td> <td></td> <td>$\overline{\}$</td> <td>Minimum Trip (Plug/Trip) -></td> <td>300A</td> <td>400A</td> <td>600A</td> <td>300A (Digi)</td> <td>125A</td> <td>175A</td> <td>225A</td> <td>100A</td> <td>160A</td> <td>250A</td> <td>600A</td> <td>150A</td> <td>400A</td> <td>400A</td> <td>400A</td> <td>600.</td> | 8 | | | $\overline{\}$ | Minimum Trip (Plug/Trip) -> | 300A | 400A | 600A | 300A (Digi) | 125A | 175A | 225A | 100A | 160A | 250A | 600A | 150A | 400A | 400A | 400A | 600. |
| Image: Construction | 9 | Downstrean Breaker | n | \sim | Maximum Trip (Frame) -> | 350A | 500A | 600A 4 Swibd — | 600A | 150A | 200A | 400A | 250A | 400A | 4 Swhd | 600A 4 Swhd | 350A | 400A | 600A | 4 Swhd | |
| Image: Sub-Feed > Im | 11 | | | $\overline{\}$ | Pow-R-Line : Branch -> | • | 4 | Swbd – | | - | 4.Swbd | | • | - 4.Sv | wbd – | +,5₩bu | 4.Swbd | | — 4.S | wbd - | |
| 21 Family (KDB, KD, CRUD, CHKD, | 12 | ↓ ↓ | | | PowR-Line : Sub-Feed -> | | | . <u></u> | | | | | | | | 1 | | - | | | |
| Pow-R-Line Panelboard / Swid Min Branch Sub-Feed 20 | 123 | K Family (KDB, KD, CH | KD, HKD, CHKE | D, KDC) | | | | | | | | | | | | | | | | | |
| Main Branch Sub-Feed 200 - 4,5,4xdd - - 37 10 10 - 5 10 35 42 10 - - 20 20 22 </td <td>124</td> <td></td> <td>1227</td> <td>Pow-R-Line F</td> <td>Panelboard / Swbd</td> <td></td> | 124 | | 1227 | Pow-R-Line F | Panelboard / Swbd | | | | | | | | | | | | | | | | |
| 100 - | 125 | 100 | Main | Branch 4 Swedd | Sub-Feed | 4.2 | 4.2 | 10 | 10 | | , , | 10 | 25 | 4.0 | 10 | | 1 | | | | |
| Image 4001 123,23,23,24 4,5%dd 13,29,39,3E - - 10 - 10 - - 10 - 10 - 10 - 10 - 10 10 - - 10 </td <td>125</td> <td>200</td> <td></td> <td>4,Swbd</td> <td></td> <td>4.2</td> <td>× 3.7</td> <td>10</td> <td>10</td> <td></td> <td></td> <td>10</td> <td></td> <td>3.7</td> <td>10</td> <td>_</td> <td></td> <td>18</td> <td>18</td> <td>18</td> <td>18</td> | 125 | 200 | | 4,Swbd | | 4.2 | × 3.7 | 10 | 10 | | | 10 | | 3.7 | 10 | _ | | 18 | 18 | 18 | 18 |
| Vertice Powr-R-Line Panelboard / Swbd 101 Main Branch Sub-Feed 102 900 3a,4 4,5wdd - - 6.0 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 6.0 - - - 0 18 | 128 | 400 | 1a,2a,3a,3E,4 | 4,Swbd | 1a,2a,3a,3E | - | | 10 | 10 | <u> </u> | _ | <u></u> | _ | | 10 | <u></u> | | - | _ | 18 | <u> </u> |
| Pow-H-Line Panelboard / Swbd Main Branch Sub-Feed 183 400 3a,4 4, Swbd - - 6.0 6.0 - - - 6.0 - - - 18 | 129 | L Family (LDB, LD, CLI | D, HLD, CHLD, | LDC, CLDC) | | | | | | | | | | | | | | | | | |
| Image: Normal bialter John bialter | 130 | | Main | Pow-R-Line I | Panelboard / Swbd | 5 | | | | | | | | | | | | | | | |
| 133 400 3a,4 4,5wbd | 132 | 300 | 3a 4 | 4 Swbd | Sub-reed | | 100 | 60 | 60 | | | <u></u> | | | 6.0 | 022 | | | 18 | 18 | 18 |
| 134 600 3a,4 4,Swbd - - - - - - - - 18 135 LG Family (LGE, LGS, LGH, LGC) - - - - - - - - - - 18 136 Main Branch Sub-Feed - - - - 6.0 - - - 10 18 18 18 136 250 - 4,Swbd - - - 6.0 6.0 - - 10 18 </td <td>133</td> <td>400</td> <td>3a,4</td> <td>4,Swbd</td> <td></td> <td></td> <td></td> <td>6.0</td> <td>6.0</td> <td>-</td> <td></td> <td></td> <td></td> <td>- 1</td> <td>6.0</td> <td>—</td> <td></td> <td></td> <td>_ '</td> <td>18</td> <td>18</td> | 133 | 400 | 3a,4 | 4,Swbd | | | | 6.0 | 6.0 | - | | | | - 1 | 6.0 | — | | | _ ' | 18 | 18 |
| ISS LGF, LGC, LGF, LGC, Main Branch Sub-Feed 138 250 - 4,Swbd - - 6.0 - - 10 18 18 18 139 400 - 4,Swbd - - 6.0 - - - 6.0 - - 10 18 18 18 139 400 - 4,Swbd - - - 6.0 - - - 6.0 - - - 10 18 18 18 18 140 400 - 4,Swbd - - - - - - - 10 18 18 18 18 140 400 - 4,Swbd - - - - - - 10 18 18 18 146 600 4,Swbd - - - - - - 25 25 25 25 25 25 25 25 25 25 </td <td>134</td> <td>600</td> <td>3a,4</td> <td>4,Swbd</td> <td></td> <td></td> <td>-</td> <td></td> <td>-</td> <td></td> <td>-</td> <td></td> <td>-</td> <td>-</td> <td></td> <td>\rightarrow</td> <td>·</td> <td>-</td> <td>-</td> <td>-</td> <td>18</td> | 134 | 600 | 3a,4 | 4,Swbd | | | - | | - | | - | | - | - | | \rightarrow | · | - | - | - | 18 |
| Pow-R-Line Panelboard / Swbd 187 Main Branch Sub-Feed 188 400 - 4,Swbd - - 6.0 6.0 - - 10 18 18 18 189 400 - 4,Swbd - - 6.0 6.0 - - - 10 18 18 18 180 600 4 4,Swbd - - - 6.0 - - - - 10 18 18 18 141 LG Current Limiting Family - - - - - - - - - 18 18 141 LG Current Limiting Family - - - - - - - 25 25 145 400 - - - - - - - - 25 25 25 25 25 25 25 25 25 25 25 25 25 25 25 25 <td< td=""><td>135</td><td>LG Family (LGE, LGS, I</td><td>.GH, LGC)</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<> | 135 | LG Family (LGE, LGS, I | .GH, LGC) | | | | | | | | | | | | | | | | | | |
| 138 250 - 4,Swbd - - - 6.0 6.0 - - - 10 18 18 18 139 200 - 4,Swbd - - - 6.0 - - - 10 18 18 18 139 400 - 4,Swbd - - - 6.0 6.0 - - - 10 18 18 18 140 600 4 4,Swbd - | 136 | | Main | Pow-R-Line I | Panelboard / Swbd | | | | | | | | | | | | | | | | |
| 133 400 - 4.5xbd - - - 6.0 - - - - 6.0 - - - - 2.5 2.5 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 | 138 | 250 | Ivialiti | 4 Swhd | | | | 60 | 60 | | <u></u> | 2 | - | | 6.0 | | | 10 | 18 | 18 | 18 |
| H0 600 4 4,Swbd - - - - - - - 18 H1 LG Current Limiting Family Pow-R-Line Panelboard / Swbd - - - - - - - 18 H2 Pow-R-Line Panelboard / Swbd Main Branch Sub-Feed - 18 H2 Main Branch Sub-Feed - <th< td=""><td>139</td><td>400</td><td>1. <u></u></td><td>4,Swbd</td><td></td><td></td><td>_</td><td>6.0</td><td>6.0</td><td></td><td>1776</td><td></td><td></td><td>_ '</td><td>6.0</td><td></td><td></td><td>1</td><td>_ '</td><td>18</td><td>18</td></th<> | 139 | 400 | 1. <u></u> | 4,Swbd | | | _ | 6.0 | 6.0 | | 1 7 76 | | | _ ' | 6.0 | | | 1 | _ ' | 18 | 18 |
| Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed Initial Concentration of Sub-Feed | 140 | 600 | 4 | 4,Swbd | | | | - | 1000 | - | | | | | - | - | | | | | 1 8 |
| H2 Pow-R-Line Panelboard / Swbd H3 Main Branch Sub-Feed 145 400 - 4, Swbd - - 6 6 - - 6 - - - 25 25 146 400 - 4, Swbd - - 6 6 - - - 25 25 146 4, Swbd - - - - - 6 - - - 25 25 146 4, Swbd - - - - - - 25 25 146 4, Swbd - - - - - - - 25 25 16 4, Swbd - - - - - - 25 25 Ready | 141 | LG Current Limiting Fa | mily | | | | | | | | | | | | | | | | | | |
| Has Diamen Sub-reeq 400 - 4,Swbd - - 6 6 - - 6 - - 25 25 146 400 4,Swbd - - 6 6 - - - 25 25 146 600 4 4,Swbd - - - - - - 25 25 146 600 4 4,Swbd - - - - - - 25 25 146 4 5 0.1 Seconds / - - - - 25 25 Ready | 142 | | M-: | Pow-R-Line P | raneipoard / Swbd | | | | | | | | | | | | | | | | |
| | 14.5 | 400 | Iviain | 4 Swhd | Sub-Feed | | | 6 | 6 | | | | | | 6 | | í | | | 25 | 25 |
| | 146 | 600 | 4 | 4,Swbd | | | | - | _ | | - | <u>9</u> | | | | | <u> </u> | | - | | 25 |
| | K | ↓ ► ► \ 100% Sel | ective / 0.1 | Seconds / | | | | | | | < | | | | | | Juli | | | | > |
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Simplified One-Line – Device Selection Continued



| | Microsoft Excel - | Select | ive Coordina | tion Tables R3 - 4-1-201 | 1.xls | | | | | | | | | | | | | | |
|---|---|---------------------|---|-------------------------------------|----------------|--------|-----------|--|----------------------|--------------------|-------------------|-------------------|----------------------|-------------------|----------------------|-------|----------------|----------|------------|
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| 1 | MCCB Select | ive Co | ordination | Combinations — Tes | | | | | | | | | | | | | | | |
| 2 | / | | | | | | | | | 15 | | | | | | | | | |
| 3 | | Upstream Breaker | | | NFarme Breaker | | N-Frame B | and the second sec | | | | Frame Brake | | | | | | | |
| 4 | | $\langle \rangle$ | | Breaker Family -> | NHH | N | N | N | N | R | R | R | R | R | R | | | | |
| 5 | | \sim | | Type Trip Unit -> | 210 310 | 310 | 310 | 310 | 310 | 310 | ETU 310 | 210 310 | ETU 310 | 310 | 210 310 | | | | |
| | | / | | Digitrip RMS Trip Unit -> | | 550. | 550. | | | 510, 610, | 510, 610, | 510, 610, | 510, 610, | 510, 610, | 510, 610, | | | | |
| 7 | | | \mathbf{X} | Optim Trip Unit -> | (<u>1</u> | 1050 | 1050 | 550, 1050 | 0 550, 1050 | 810, 910, 1050 | 810, 910, 1050 | 810, 910, 1050 | 810, 910, 1050 | 810, 910, 1050 | 810, 910, 1050 | | | | |
| 8 | | | | Minimum Trip (Plug/Trip) -> | 150A | 400A | 400A | 400A | 600A | 800A | 800A | 800A | 800A | 1000A | 1200A | | | | |
| 9 | Downstream | | $\overline{\}$ | Maximum Trip (Frame) -> | 350A | 400A | 600A | 800A | 1200A | 800A | 1000A | 1200A | 1600A | 2000A | 2500A | | | | |
| 10 | Breaker | | / | Pow-R-Line : Main - > | 4 | | | 4,Swbd | 4,Swbd | • | | <u> </u> | vbd —— | | | | | | |
| 11 | Ļ | | \backslash | Pow-R-Line : Branch -> | 4,Swbd | * | 4 | Swbd - | | | | <u> </u> | vbd —— | | • | - | | | |
| 153 | N Family (ND, CND, HND, | CHND, NDC | C. CNDC. NGS. NGH. | NGC) | | | | | | | | | | | | | | | - |
| 154 | | | Pow-R-Line P | anelboard / Swbd | | | | | | | | | | | | 1 | | | |
| 155 | | Main | Branch | Sub-Feed | | | | | - | | <u>.</u> | | <u>.</u> | | <u>.</u> | | | | |
| 156 | 400 | () | 4,Swbd | | 1.000 | 12-24 | | 10 | 12 | 16 | 16 | 16 | 16 | 22 | 25 | | | | |
| 157 | 800 | 4.Swbd | 4,5wbd | | | | _ | 0 | 12 | <u> (* 14</u> | | | 16 | 22 | 25 | | | | |
| 159 | 1200 | 4,Swbd | 4,Swbd | _ | 1,5-1 | | | 12 | | 0 1 - 1 | 1,5 | | | 18 | * 18 | | | | |
| 160 | NHH Family | | | | | | | | | | | | | | | | | | |
| 161 | | Main | Pow-R-Line P Branch | aneiboard / Swbd | | | | | | | | | | | | | | | = |
| 163 | 350 | 4 | 4,Swbd | Cupil Cou | | - | | - | 12 | 16 | 16 | 16 | 16 | 22 | 25 | 1 | | | |
| 164 165 166 167 168 169 170 171 172 173 174 | | | | | | | | | | | | | | | | | | | |
| 175 | | | | | | | | | | | | | | | | | | | * |
| K | ♦ ► ► ► 100% Select | tive / 0.1 | Seconds / | | | | | | | | | | | | | | | | > |
| Rea | dy | × | | | | | h. eu | | | Dimmer L | Dealster | | | | | | | | |
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Simplified One-Line With Total Selective Coordination Up to the Generator



Simplified One-Line – Equipment Costs – Selectively Coordinated System



Simplified One-Line – Flatten the System



Total Selective Coordination Summary

- Flatten the system
- Broaden your ideas on transformer protection
- Check ATS withstand ratings with chosen breakers
- Tables represent a single manufacturer's equipment



Total Selective Coordination Summary

- Fusible Devices
 - Especially with high fault currents
 - New fusible panelboards available
 - Physical sizes for fusible equipment is typically larger than breaker designs





Total Selective Coordination Summary

- Can't I just put in my specs that the switchgear manufacturer must provide a selectively coordinated system?
- Yes, but please don't!
 - Our salesmen won't necessarily know which circuits need to be coordinated
 - Cable sizes may need to be increased, depending on which breakers are required
 - ATS sizes may need to be increased not in our package
 - Generator breaker sizes may need to increase not in our package
 - Distribution equipment size may increase and no longer fit in the room
 - Who pays for all of the above?



Coordination at 0.01 and 0.1 Seconds

- Here's our original equipment (downstream of the ATS) selected without selective coordination in mind
- Do we coordinate at the 0.01 level?
- How about at 0.1 seconds?





Coordination at 0.01 and 0.1 Seconds

 But we have a little bit of work to do upstream of the ATS on the Generator Side.







Coordination at 0.1 Seconds

- We can make one small change and get coordination at 0.1 second – change the ATS feeder to an electronic trip.
- Total adder from our original \$11.5K cost estimate - <\$500, 4% adder.



Emergency Downstream of ATS.tcc Ref. Voltage: 480V Current in Amps x



Coordination at 0.01 Seconds

- To achieve coordination to 0.01 seconds above the ATS on the generator side, we have to:
 - Provide an 800AF/400AT electronic trip breaker to feed the ATS
 - Use a Power Circuit Breaker on the Generator
- Cost adder over base case for our equipment: \$1.5K (not including generator breaker)



CURRENT IN AMPERES



Emergency Downstream of ATS.tcc Ref. Voltage: 480V Current in Amps x

Challenge - Enforcement

- How is Selective Coordination Evaluated?
 - Some jurisdictions are looking at curves
 - Some jurisdictions require a stamped letter from the engineer of record
 - In some jurisdictions, it has yet to be defined



Challenge - Enforcement

- Breaker Curves
 - No standardized method for representing time current curves



CURRENT IN AMPERES





QUICKLAG 3-Pole Circuit Breakers, 15-100 Amperes CURRENT IN PERCENT OF DREAMER TRIP UNIT RA 5 Ē 8 ≂ 88 ₽ Circuit Breaker Time/Current Curves QUICKLAG 3-Pole Circuit Breakers, 15-100 QUICKLAG* 3-Pole Circuit Breakers, 15-100 Amperes For application and coordination purposes only. Based on 40°C ambient, cold start. Connected with four (4) feet of rated wire (80/75°C) per terminal. Tested in open air with current in all poles. 5,000 **BAB Trip Curve** 1.000 Breaker Ratings (UL Listed) Breaker Maximum Continuous Interrupting Capacity RMS Symmetrical Amperes (M) 2,000 Type ≻Fole Volts Ac (60 Hz) Amperes HOP, QC, BAB QCR, QCP QPHW, QBHW, QCHW QHPW, QHCW, HBAW 15-100 15-30 15-100 15-20 240 240 240 240 10 10 22 65 Continuous Amperes Instantaneous Trip Range, Amperes 200-400 300-500 450-550 800-1200 15-20 25-40 45-60 70-100 Single-pole text data at 25°C based on NEMA procedures for verifying performance of molded case circuit breakers. ТП (50-100 Amp) Maximum Single-Pole Trip Times at 25°C () Maximum Minimum +++++++++ 111 1 É LÉTÉ L Ð - 10 пп Maximum Interrupting Time 1 122 12 П пп . . Interrupting Rating (See Tabulation Above) .01 Sec нін 60 .87 - 14 Ш пп П .005 1005 тп Ш 300 002 302 302 000 000 10000 11000 11000 11000 11000 8 8 8 8 8 8 8 2 Â 8 9000 ğ ž CURRENT INFERCENT OF INFEARER TRIP UNIT RATING. .001 B R 9 8 8 8 20,000 10,000 40,000 50,000 50,000 50,000 50,000 50,000 50,000 50,000 CURRENT INPERCENT OF BREAKER TRIP UNIT BATHY.



How is Selective Coordination evaluated?

- The SKM (and all coordination software) plots cut off at 0.01 second
- If coordination to 0.01 seconds is acceptable, be aware that this will be contradicted by our 100% Selective Coordination Tables





Challenge - Design

What about Arc Flash?

- Arc Flash Energy is dependent upon:
 - Actual magnitude of the fault energy
 - *Time that the arc is allowed to propagate*

When we select devices to selectively coordinate, we are purposefully introducing time delays by selecting larger and/or more adjustable devices upstream.



Simplified One-Line – Arc Flash



Challenge – Arc Flash

Techniques for dealing with the Arc Flash Challenge:

- Zone Selective Interlocking
- Arc Flash Reduction Maintenance Switches

Note: 2011 NEC 240.87 mandates one of the above or differential protection when circuit breakers are used without instantaneous protection.



Questions?



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