



**Workshop on Advanced Intelligent
Automation Technology**

Topic 7

**Development of an intellectualized symmetric
high-speed dual-spindle grinding machine and
study on LED probe speedy grinding**

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Outline



1. Introduction – background and objective
2. The proposed approach and procedures
3. Development of the gantry grinding system
4. Development of in-situ dressing
5. The present experimental results
6. Previous results – a commercial case study
7. Conclusions

Background

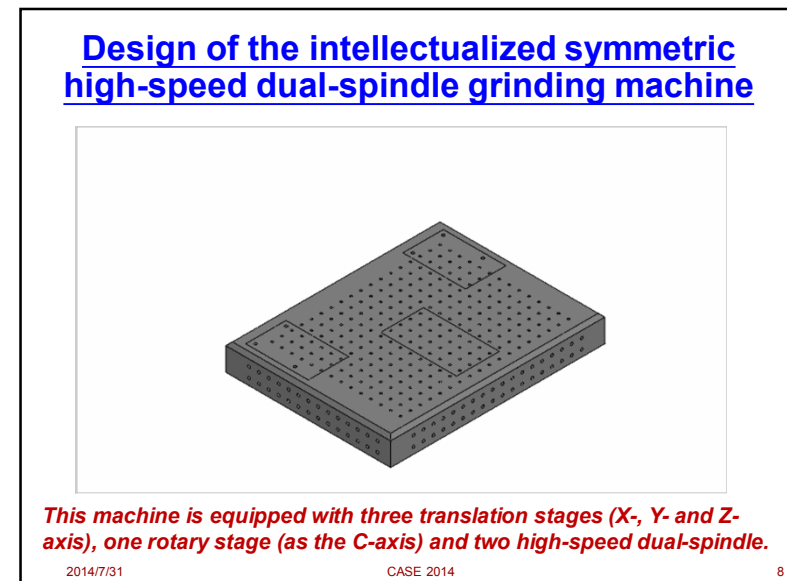
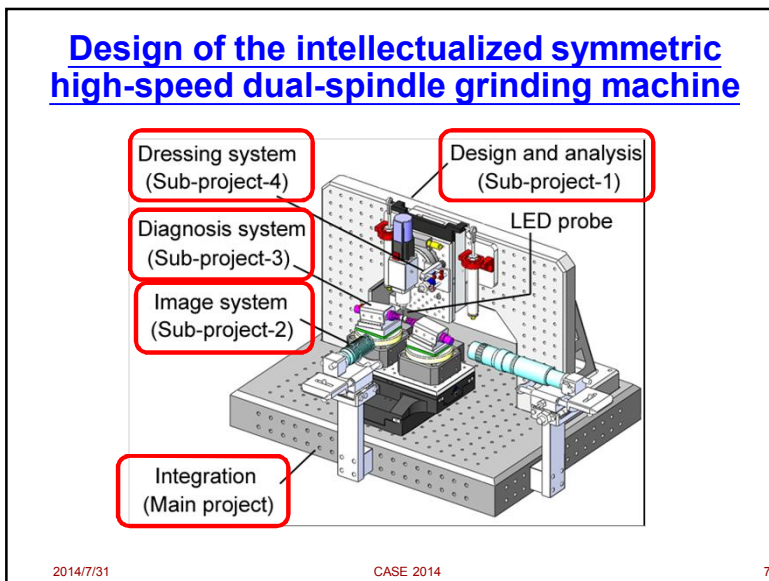
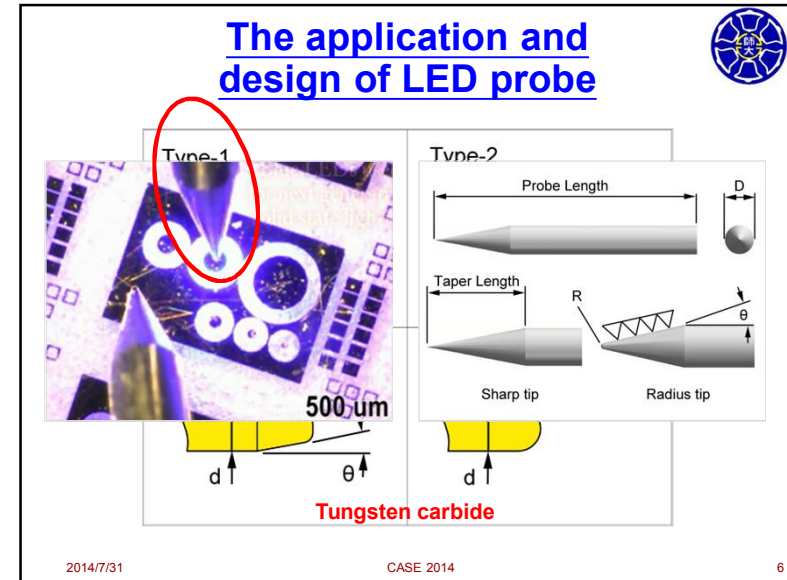
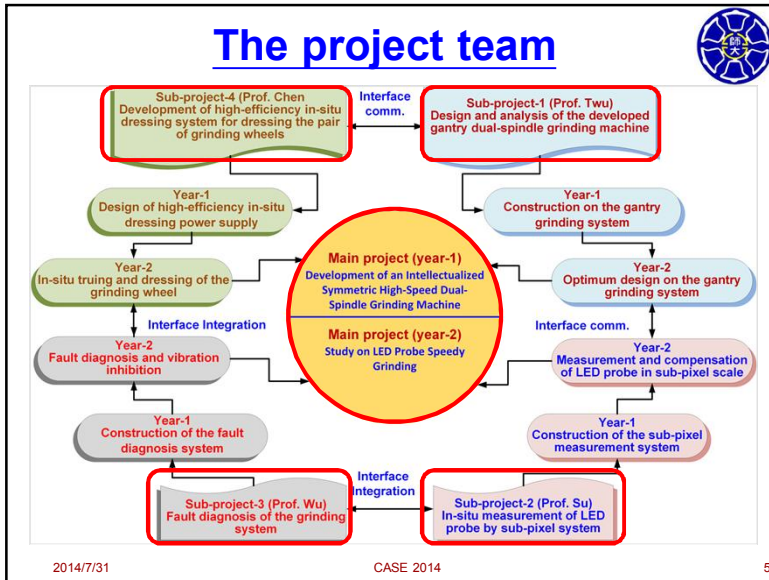


1. Miniaturization of products is a recent trend.
2. LED (Light Emitting Diode) is one of today's most energy-efficient and rapidly-developing lighting technologies.
3. It has the potential to fundamentally change the future of lighting all over the world.
4. Accordingly, a wear-resistant and conductive LED probe is essential for testing LED during process.

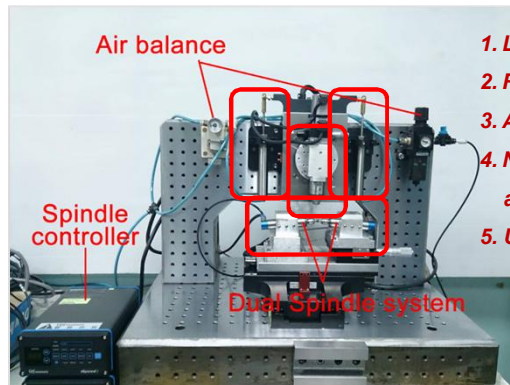
Objective



1. The objective of the research project is to develop an intellectualized symmetric high-speed dual-spindle grinding machine.
2. By applying the developed techniques of the four sub-projects, the LED-probe made of tungsten carbide can be ground efficiently.
3. The current development is focused on the feasibility study of LED-probe fast grinding with less costly way and construction of the autonomous technology.



Finished intellectualized symmetric high-speed dual-spindle grinding machine



1. Linear motor (stage)
2. Resolution: 1nm
3. Accuracy: +/- 300nm
4. No contact, no wear and no backlash
5. USD 300,000 totally

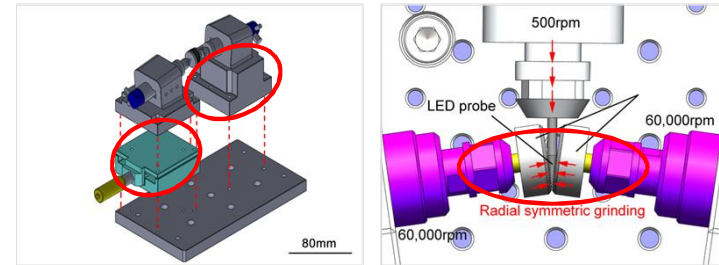
A nanometer scale grinding depth can be provided in the grinding system.

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The proposed approach – double-grinding



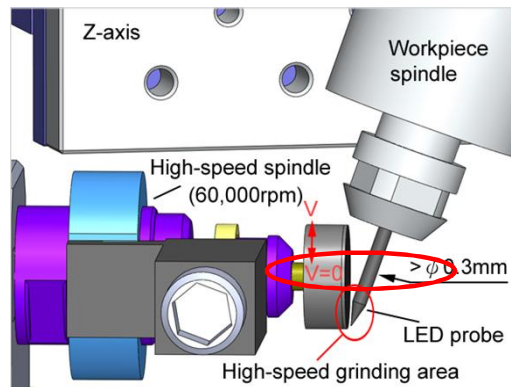
1. To guarantee a high-efficiency and high-precision machining on the LED probe, a double-grinding approach is proposed in this study.
2. This design is helpful in increasing the bilateral symmetry and the grinding efficiency of the LED probe.

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Single-grinding



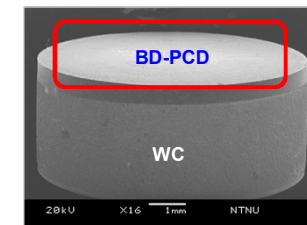
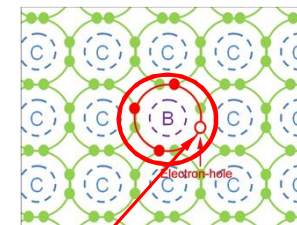
Note, the grinding area is not at the central part of the grinding-wheel since the speed of this area is zero.

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The grinding-wheel used



Boron-doped polycrystalline composite diamond (BD-PCD)

Electron-hole in the diamond lattice, which can contribute to electric conduction.

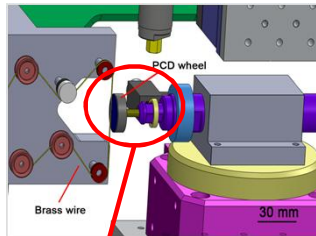
The BD-PCD grinding-wheel can be more easily trued by micro rotary w-EDM.

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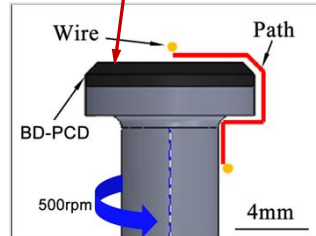
Grinding-wheel truing process



In-situ truing

A high co-axial accuracy is achieved between the grinding-wheel and the high-speed spindle.

Boron-doped polycrystalline composite diamond (BD-PCD)



The BD-PCD grinding-wheel is formed by using micro rotary w-EDM.

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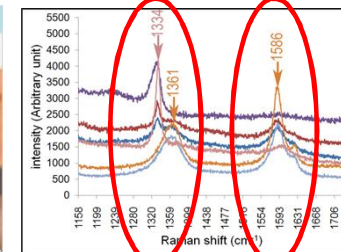
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The trued surface of the BD-PCD grinding-wheel



The trued surface



Raman spectrum

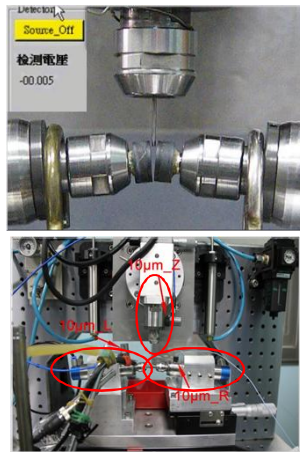
- **During the discharge process, the temperature in the plasma channel may reach 8,000-12,000 °C.**
- **Hence, graphitizing of diamond is inevitable.**

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LED-probe grinding test



Parameter	Condition
Spindle speed	25,000-60,000(rpm)
Workpiece speed	500(rpm)
Workpiece Diameter	Tungsten carbide Φ0.7(mm)
Grinding depth	1(µm/stroke)
Grain size	10, 25, 40(µm)
Feed-rate	0.2(mm/min)
Coolant	DOG 1000(Oil-base)
Grinding time	18(min)

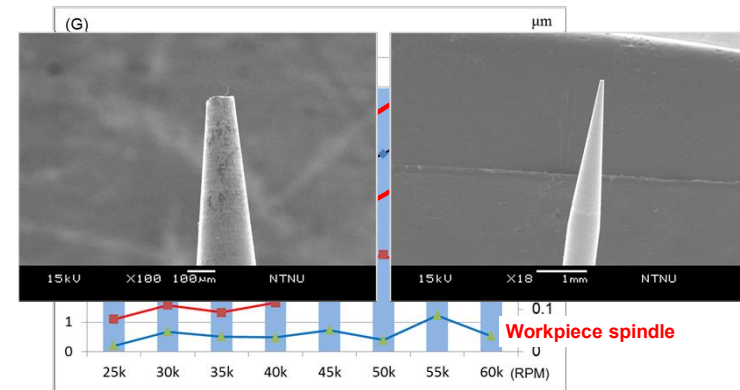
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The amount of the vibration on the corresponding spindle

A grain size of 10 micrometers is used.



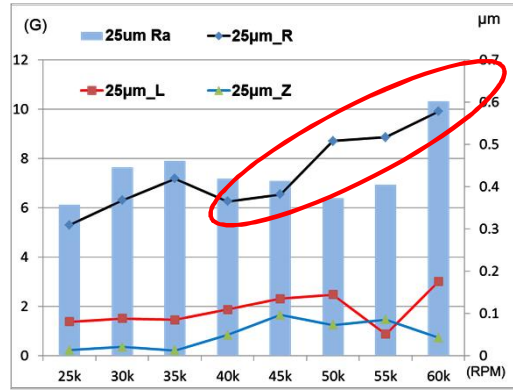
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The amount of the vibration on the corresponding spindle

A grain size of 25 micrometers is used.



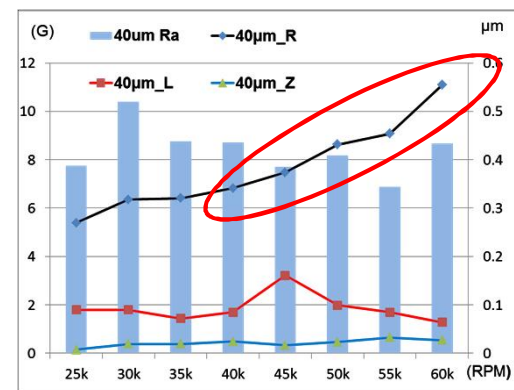
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The amount of the vibration on the corresponding spindle

A grain size of 40 micrometers is used.

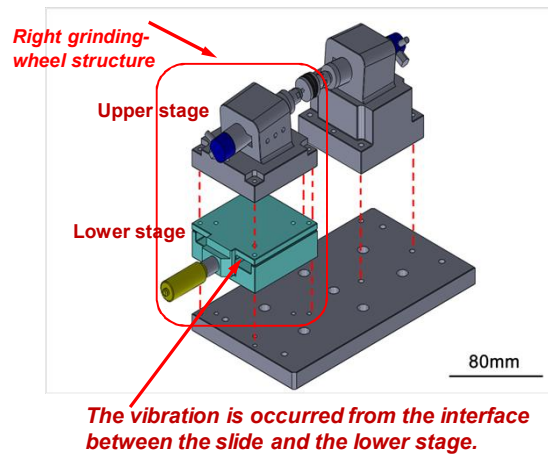


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Vibration source



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A case study in the past

(A commercial case)

Development of a quantitative cell-counting slide made of PMMA

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Characteristics of urine

Composition:

Normally, a human urinary sediments are composed of about 95 percent water and 5 percent solutes.

Normal solutes found in urine include:

- Urea
- Creatinine
- Uric acid
- Ketone bodies
- Potassium
- Sodium
- Chloride



A human urinary sediments

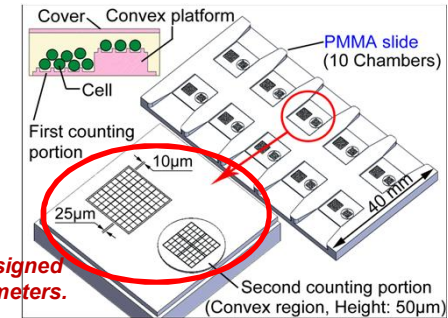
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Design of a quantitative cell-counting slide made of PMMA

(For detection of a human urinary sediments)



The width for each microgroove is designed only at 8-10 micrometers.

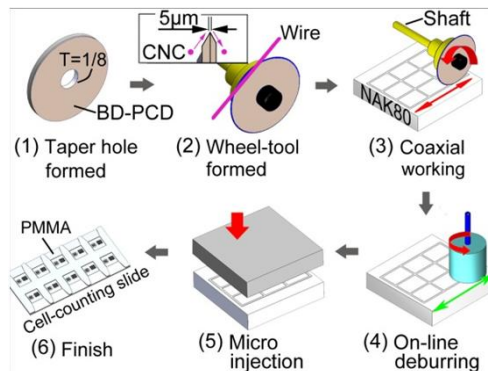
A concave platform cell-counting slide mold

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The proposed in-situ fabrication process



Note, in-situ fabrication enables a microgroove array to precisely generate on a biomedical-mold.

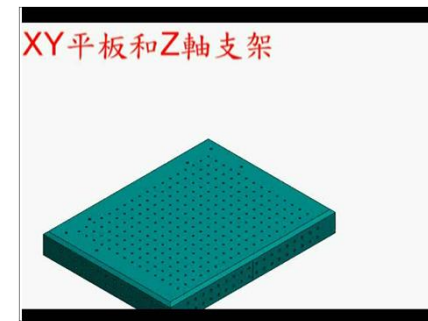
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Design of the high-precision tabletop hybrid CNC machine tool

XY平板和Z轴支架



A tabletop hybrid CNC machine tool

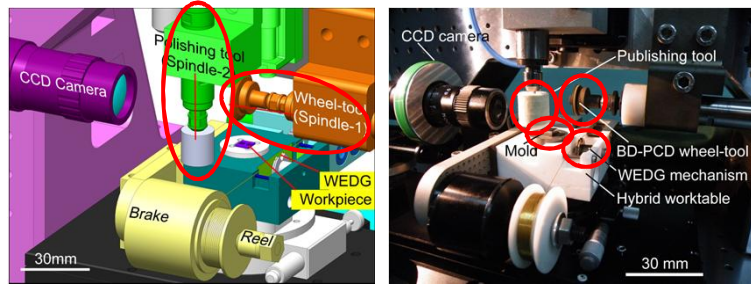
This machine is equipped with three commercial translation stages (X-, Y- and Z- axis) and one rotary stage (as the C-axis).

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Design of the perpendicular dual-spindle



Designed dual-spindle set-up

In-situ machining

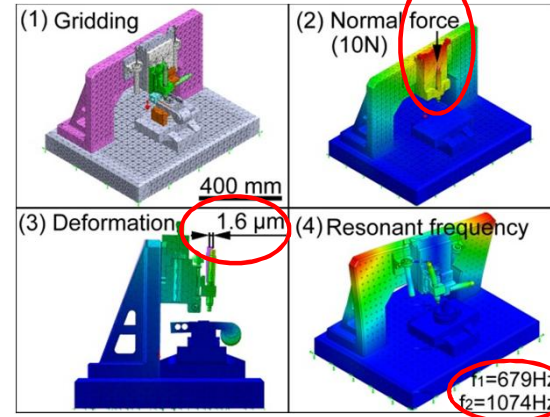
To guarantee machining accuracy and reduce tedious readjustment during process, a set of perpendicular dual-spindle is propose in this study.

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Analyses of deformation and resonance

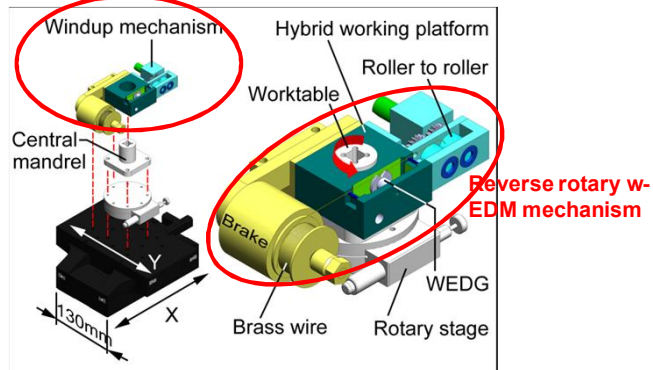


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Design for the hybrid working platform



Reverse rotary w-EDM mechanism

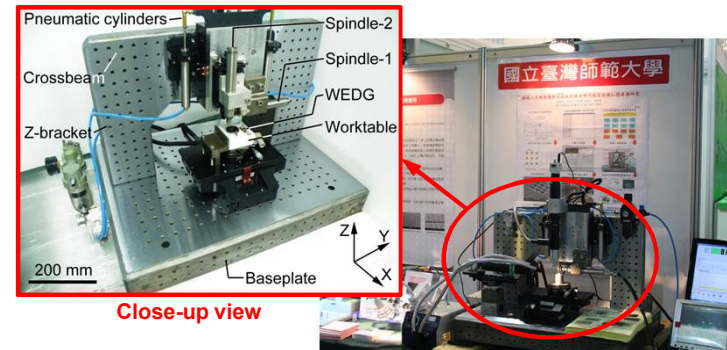
To generate the accuracy of such a fine microgroove array, a hybrid working platform to support the in-situ process is designed.

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Finished tabletop hybrid CNC machine tool



Close-up view

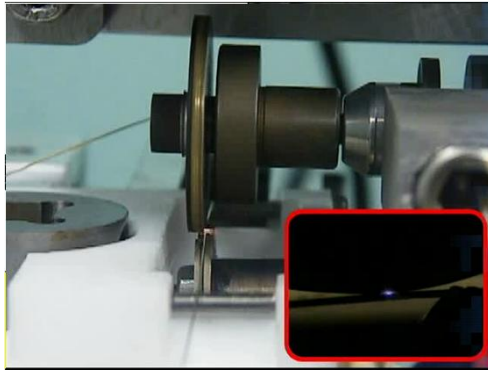
This machine can provide for microgroove grinding by nanometer scale grinding depth.

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Thinning of the BD-PCD wheel-tool



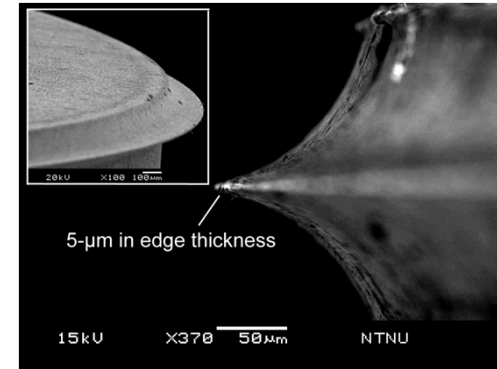
BD-PCD is capable of electrical conductivity, meaning it can be more easily cut by electrical discharge machining on the developed machine tool.

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Thinned grinding-edge



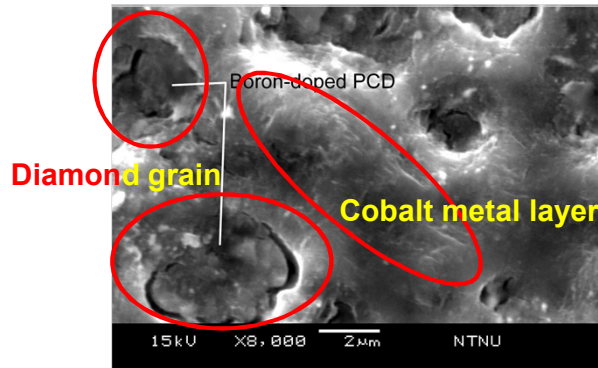
A thinned BD-PCD wheel-tool with an edge-thickness of 5- μ m and a slight draft angle of 5 degree.

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A smoothly cut (broken) in diamond grain



The image demonstrates the BD-PCD can be precisely formed down to an ultrathin level by rotary micro w-EDM.

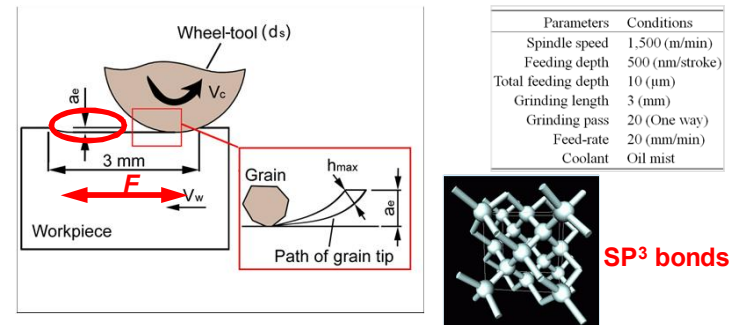
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Microgroove generation by HSFSG

High-Speed & Fast-Shallow Grinding



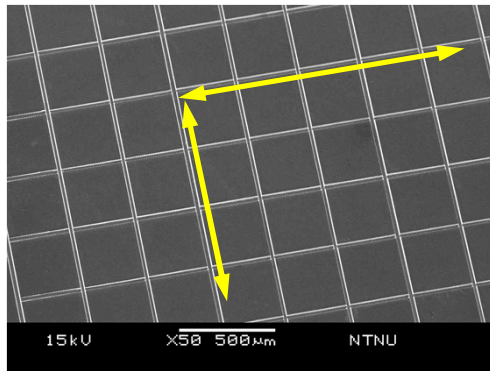
1. By applying a fast grinding feed-rate, we can create considerable metal removals per unit of time.
2. By using a nanometer scale grinding depth, we can keep the diamond lattice in SP³ bond during grinding because of cold machining conditions used.

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Finished crisscross microgroove array



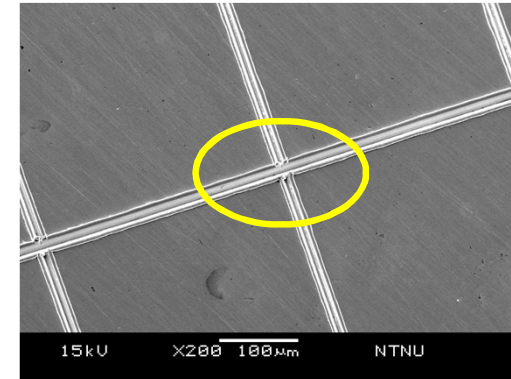
A finished microgroove array with extremely high straightness and high orthogonality.

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Proposed deburring process at the intersections of microgrooves



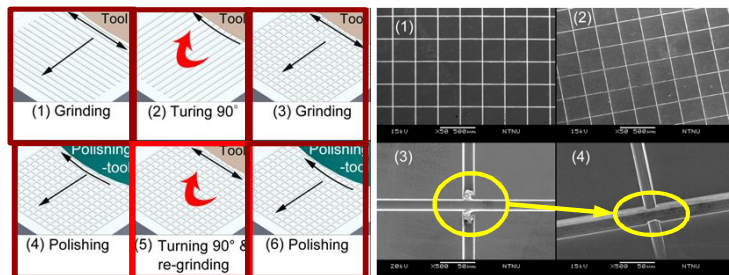
Burrs occur as a result of NAK80 mold steel being ductile, and plowing effect during microgroove grinding.

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Proposed deburring process at the intersections of microgrooves(cont.)



Proposed deburring process

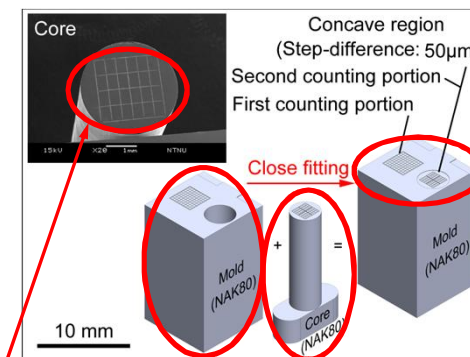
Before and after deburring

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Mold design of a quantitative cell-counting slide



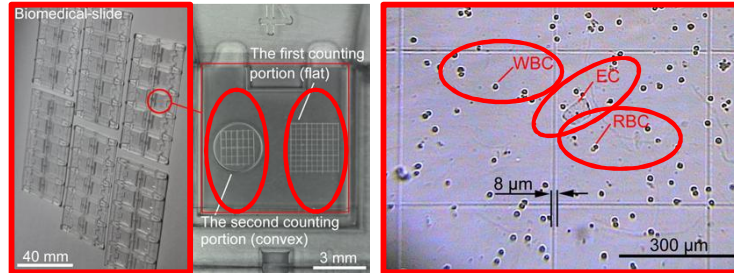
An embedded mold design approach is proposed. The width for each microgroove is only 8-10 micrometers.

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Finished cell-counting slide made of PMMA and an example of cell counting



1. Note, the two distinct cell-counting portions can be clearly revealed in each chamber.
2. It indicates the multiple micro ridge array of the biomedical-slide can be exactly duplicated from the machined biomedical-mold.

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Conclusions

➤ In LED probe grinding case:

1. An intellectualized symmetric high-speed dual-spindle grinding machine for LED probe grinding has been developed and verified successfully.
2. A pair of BD-PCD grinding-wheel is dressed by the rotary w-EDM and a LED probe made of tungsten carbide has been tentatively grinding in first year.

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Conclusions(cont.)

➤ In biomedical-slide mold case:

1. A high-precision tabletop hybrid CNC machine tool for in-situ fabricating a biomedical-slide mold has been developed and verified successfully.
2. The High-Speed & Fast-Shallow Grinding technique is successfully used to grind microgroove array on NAK80 mold steel.
3. By using nanometer scale grinding depth results in a cold machining and preservation for diamond's SP³ bond structure.

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Conclusions(cont.)

4. Due to the design of the in-situ machining function, the machined biomedical-slide mold requires no unloading, reloading and calibration.
5. Experimental results prove the convex platform quantitative cell-counting slide is successfully developed.

Thank you so much
for your attention!

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Topic 7

Development of an intellectualized symmetric high-
speed dual-spindle grinding machine and study on
LED probe speedy grinding

Sub-project I

Design and analysis of the developed gantry
dual-spindle grinding machine

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Outline



1. Introduction and the objectives.
2. The proposed approach and procedures
3. Static and dynamic analysis of initial design
4. Metamodel and structural optimization
5. Summary and conclusion
6. References

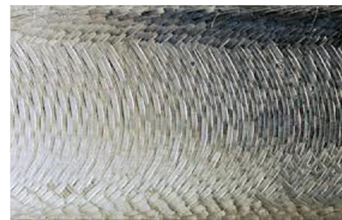
Introduction



One of **key issue** in mechanical manufacturing is **vibration** [1].



texture caused by chatter in turning



texture caused by chatter in milling

Source of figures: <http://74.220.207.117/~horvathl/m-tool-vib.htm>

http://www.hv.se/extra/pod/?action=pod_show&id=753&module_instance=11

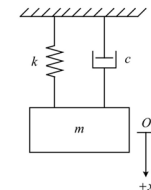
Introduction



Stiffness is a key parameter of vibration problem.
The equation of 1 DOF mass-spring-damper system

$$m\ddot{x} + c\dot{x} + kx = f(t)$$

$$\omega_n = \sqrt{\frac{k}{m}}, \zeta = \frac{c}{2\sqrt{km}}, \omega_d = \omega_n \sqrt{1 - \zeta^2}, \zeta < 1$$



The stiffness of system is determined by mass
distribution of structure.

Structural design is the foundation for the
development of high-precision manufacturing system.
Analyzing stiffness is an important issue in machine tool
design [2].

Objectives of sub-project I



1. To optimize the structural design for the proposed intellectualized symmetric high-speed dual-spindles grinding machine.
2. To propose a dynamic model of grinding chatter for the designed system.
3. To develop the strategy of chatter suppression for the designed system.

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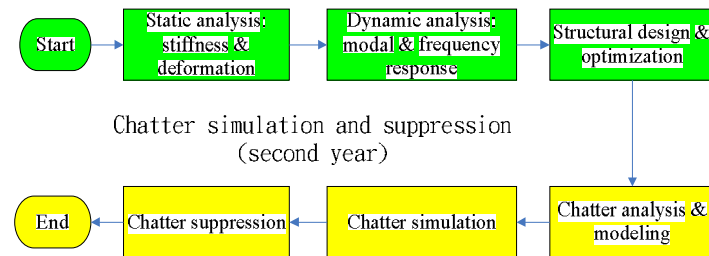
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Procedure of research



Structural design and analysis
(first year)

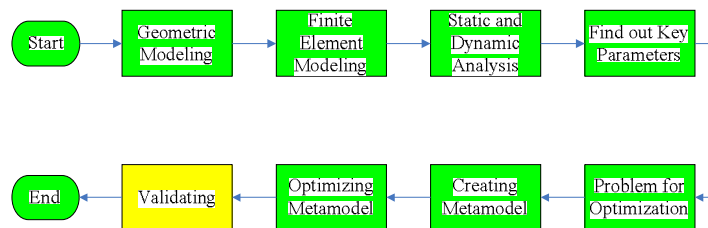


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Procedure of the first year research

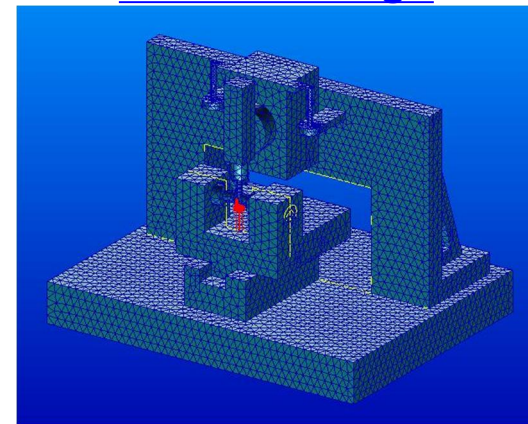


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Finite element model of initial design

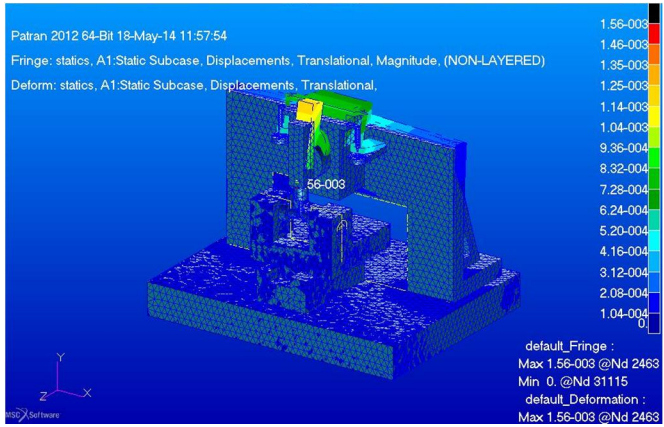


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Static analysis results of initial design - displacement

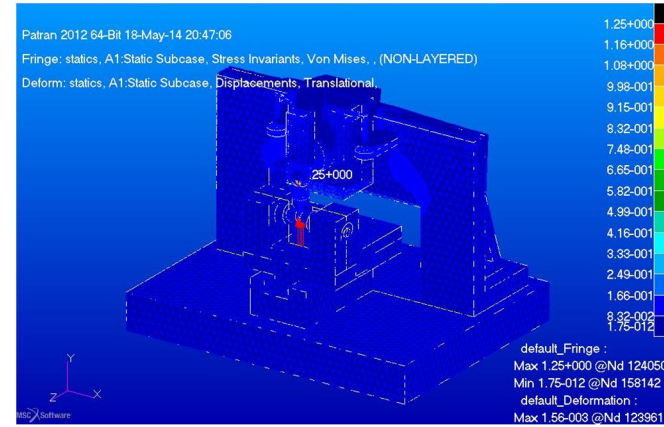


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Static analysis results of initial design - stress

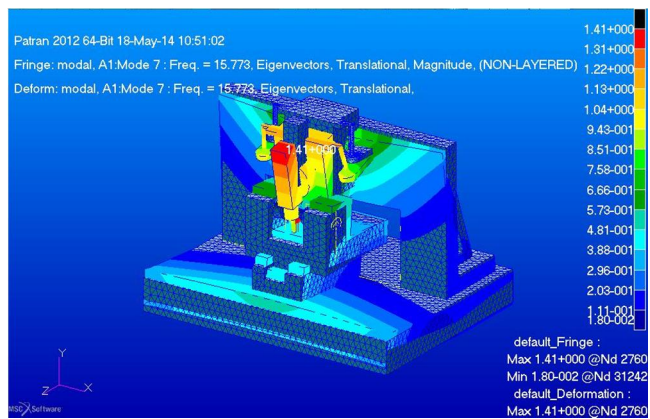


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Dynamic analysis results of initial design - 1st mode

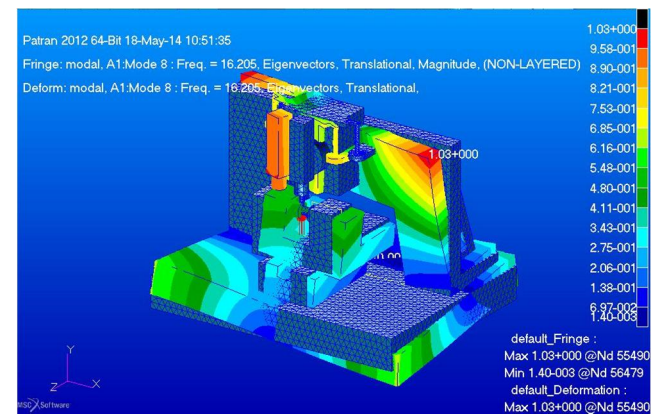


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Dynamic analysis results of initial design - 2nd mode



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Results of analysis



Deformation at tip < 1 μm

Max. stress < 2 N/mm^2

Natural frequency = 11.5, 16.2, 20, 25.1, 26.4, 38.9, 43.1, 46.7, 49.3, 50.7...

The lowest frequency > 10 Hz > the frequency of the low speed spindle (500 rpm)

The high speed spindle (60000 rpm) is far beyond the 100th natural frequency of the system.

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The key part and key point of structural design



From the results of finite element analysis, the first modal shape and deformation, we know that **headstock and supporting pneumatic cylinder** play main role in static and dynamic responses.

Two key factors decide the static and dynamic behavior of the designed structure:

The **stiffness of contact interface** between headstock and column

The **coefficients of structural damping**

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Optimization problem



Objective: minimize the weight (or volume)

Design variables: length (xL), height (yH), width (zW)

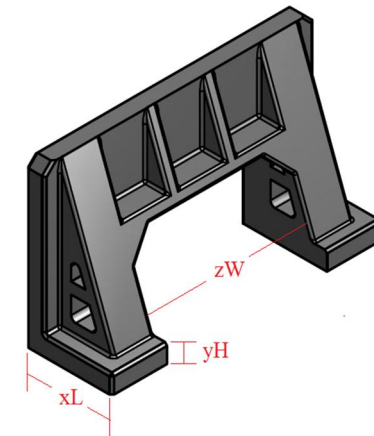
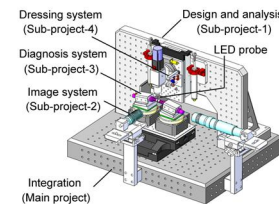
Constrains: deformation at tip of probe < 2 μm
stress < yielding stress
2nd natural frequency > 10
(since the 2nd natural frequency is the most sensitive one)

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Design Variables



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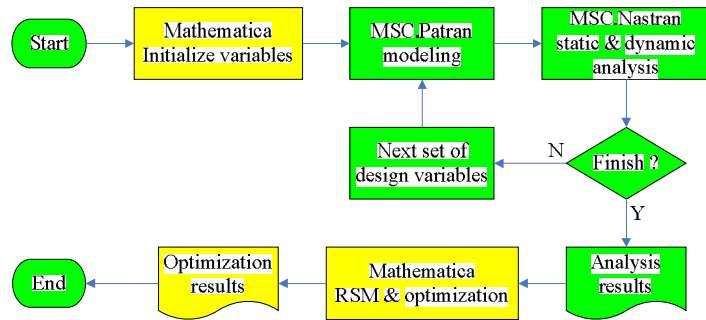
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Flowchart of optimization

Mathematica: the mathematic software to do the RSM and optimization.

MSC.Patran/Nastran: the software to do the finite element analysis.



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Metamodel Response Surface Method

Metamodel

also known as **surrogate model**, is an approximate representation [3].

an alternative to costly analysis or experiment [4].

e.g. Genetic algorithms, artificial neural networks,...

Response surface methodology (RSM)

mathematical and statistical techniques to develop functional relationship between input and response [5].

Design optimization is a computation intensive process.

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Response surface

The **response surface** is represented by the polynomial function **F(x,y,z)**.

Quadratic polynomial items for response surface

$$\{1, x, y, z, xy, xz, yz, x^2, y^2, z^2\}$$

Cubic polynomial item for response surface

$$\{1, x, y, z, xy, xz, yz, x^2, y^2, z^2, xyz, xy^2, xz^2, x^2y, x^2z, y^2z\}$$

The process of RSM is to find the **coefficients** of these polynomial items.

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Creation of response surface

Three factors, xL, yH, and zW, are used for RSM.

Three levels for each of these factors.

Totally there are **3³ designs**.

Two kinds of **finite element analysis**, static and dynamic analysis, are run for each design, which means **54 runs of analysis**.

Two results of finite element analysis, **displacement** and **2nd frequency** are used to create the response surface, along with volume of structure.

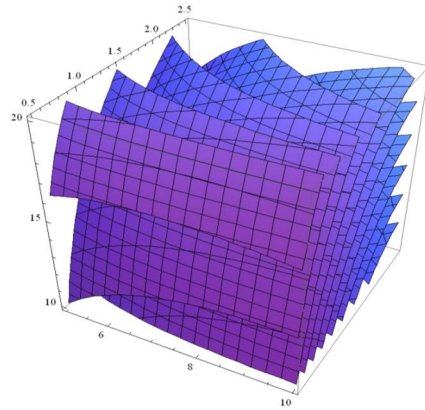
The **stress result is not considered** since it is far below the yielding stress.

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Response surface of volume

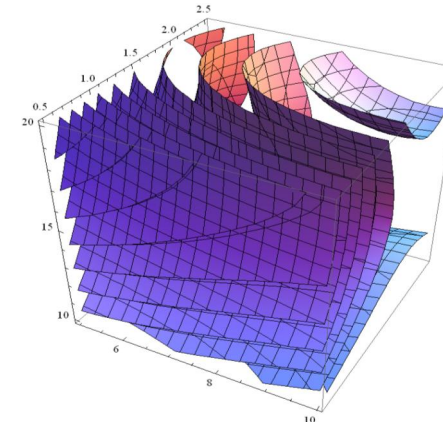


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Response surface of displacement

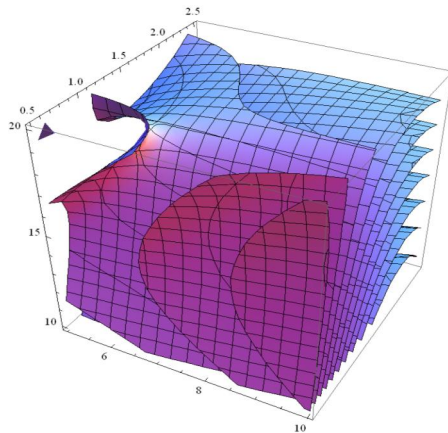


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Response surface of 2nd frequency



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Optimization results



Mathematica is used to find the optimal point on the response surface. Quadratic and cubic polynomials are used for design I and II respectively.

	(xL, yH, zW) (mm)	Change of Volume %	Change of Displacement %	Change of Frequency %
Original Design	(200,40,355)	0	0	0
Optimal Design I	(175,51,389)	-11.34	-0.3	-0.818
Optimal Design II	(184,47,389)	-11.62	-0.32	-0.823

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Summary and conclusion



The **finite element analysis of initial design** is used to decide the key points for subsequent analysis and design.

The **optimization** for the weight of structure of initial design is completed.

Metamodel with response surface method is used for optimization.

Stiffness of contact interface and structural damping coefficient of the headstock are the **key parameters** of analysis.

Further experiments to identify system parameters are needed for validation of the design model.

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References



[1] G. P. Zhang, Y.M. Huang, W.H. Shi, W.P. Fu, Predicting dynamic behaviours of a whole machine tool structure based on computer-aided engineering, International Journal of Machine Tools & Manufacture 43, p. 699-706, 2003.

[2] D. T. Huang, J.-J. Lee, On obtaining machine tool stiffness by CAE techniques, Intl' J. of Machine Tools & Manufacture 41, p. 1149-1163, 2001.

[3] M. Ramu, V. P. Raja, P. R. Thyla, M. Gunaseelan, Design optimization of complex structures using metamodels, Jordan Journal of Mechanical and Industrial Engineering, v.4 no. 5, p. 653-664, 2010.

[4] D. J. Lizotte, R. Greiner, D. Schuurmans, An experimental methodology for response surface optimization methods, Journal of Global Optimization, 53(4), p. 699-736, 2011.

[5] S. Chakraborty, A. Sen, Adaptive response surface based efficient finite element model updating, Finite Elements in Analysis and Design, 80, p. 33-40, 2014.

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Thanks for listening



2014/7/31

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Sub-pixel Edge Detection of LED Probes Based on Partial Area Effect and Iterative Curve Fitting

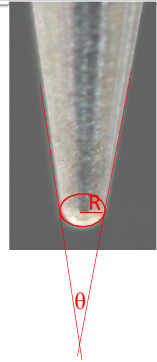
Advisor : Chung-Yen Su

Students : Nai-Kuei Chen, Chen-Chun Wang, Li-An Yu

1

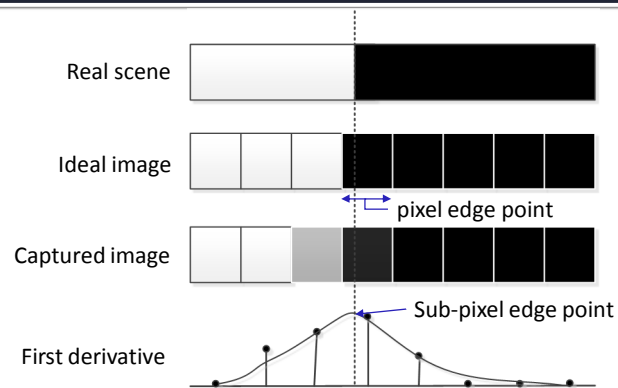
Introduction (1/2)

- This subproject is focused on measure the angle and radius of a LED probe by computer vision.
- To do that, we need to find edge points.
- Some of the common pixel-level edge detection methods are
 - Sobel, Canny, Laplacian of Gaussian (LOG), Scharr
- Sub-pixel edge detection is used to increase the precision of edge detection.
- The common sub-pixel edge detections include
 - Curve-fitting method
 - Moment-based method
 - Reconstructive method
 - Partial area effect method



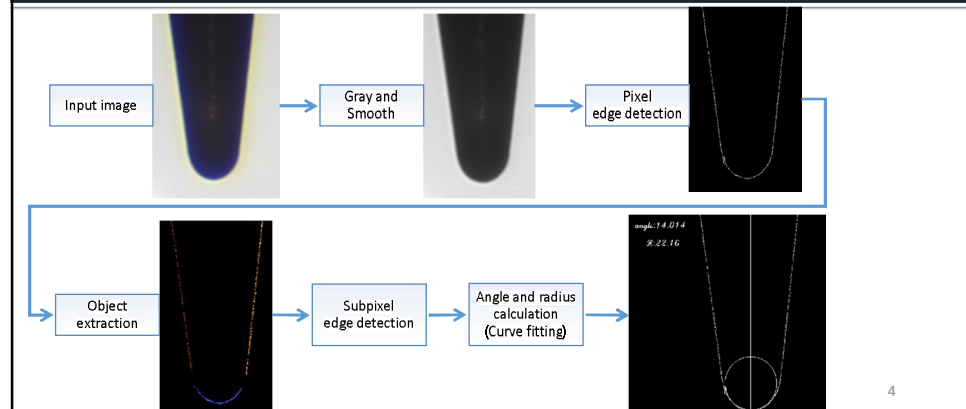
2

Introduction (2/2)



3

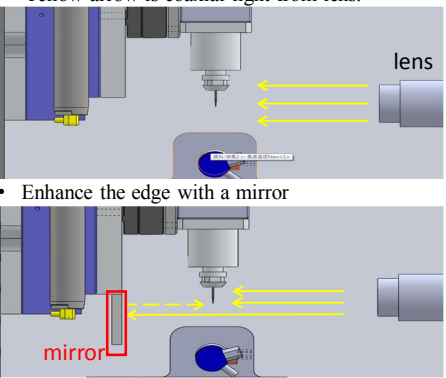
Flow Chart



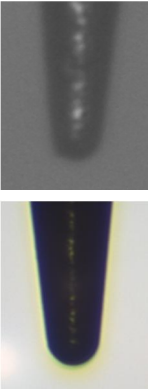
4

Getting the Input Image

- Yellow arrow is coaxial light from lens.



- Enhance the edge with a mirror



5

Converting and Smoothing

- Convert a RGB image to a gray image
 - Gray = 0.299R + 0.587G + 0.114B
- Use a Gaussian filter to smooth the resulting gray image


1	4	6	4	1
4	16	24	16	4
6	24	36	24	6
4	16	24	16	4
1	4	6	4	1

$\frac{1}{256} \times$

6

Automatic Threshold (1/2)

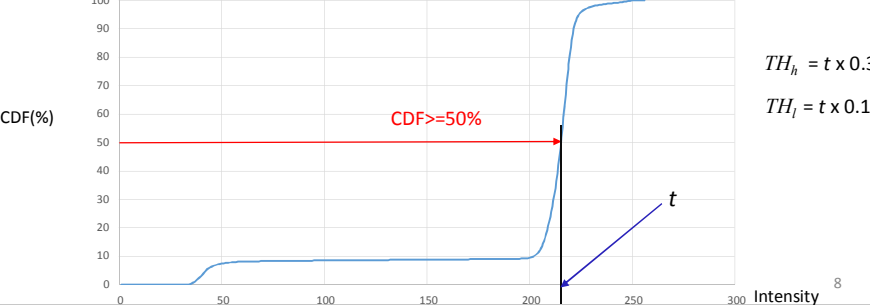
- For Sobel
 - Use Sobel operator to measure the magnitudes of gradient($|dx|+|dy|$) over the image and make CDF



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Automatic Threshold (2/2)

- For Canny
 - Multiply the median of gray image by 0.3 as high threshold and 0.1 as low threshold.



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$TH_h = t \times 0.3$
 $TH_l = t \times 0.1$

Object Extraction

Classify edge points into three groups

1. Distinguish between left and right side:

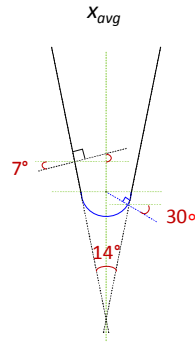
$$x_{avg} = \frac{\sum_{i=0}^{edge\ point\ counts} x_i}{edge\ point\ counts}$$

2. Get gradient direction: $\theta = \tan^{-1} \frac{dy}{dx}$

$$dx = \begin{matrix} & -1 & 0 & 1 \\ \begin{matrix} -1 \\ -2 \\ -1 \end{matrix} & * & \begin{matrix} 0 \\ 0 \\ 0 \end{matrix} & \begin{matrix} 1 \\ 2 \\ 1 \end{matrix} \\ & -1 & 0 & 1 \end{matrix} \quad dy = \begin{matrix} & -1 & -2 & -1 \\ \begin{matrix} 0 \\ 0 \\ 0 \end{matrix} & * & \begin{matrix} 0 \\ 0 \\ 0 \end{matrix} & \begin{matrix} 1 \\ 2 \\ 1 \end{matrix} \\ & 1 & 2 & 1 \end{matrix}$$

3. Differentiate edge points between line and circle:

- 1) Line: $|\theta| < 7^\circ$, Circle: $|\theta| > 30^\circ$.
- 2) Discard: $7^\circ \leq |\theta| \leq 30^\circ$



Sub-pixel Edge Detection

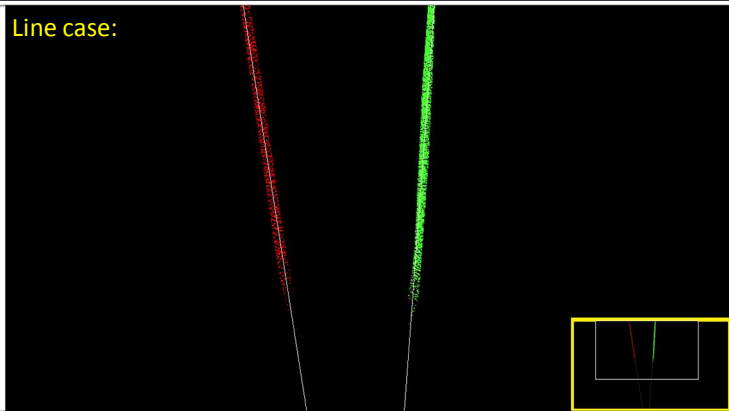
After object extraction, we compute Sub-pixel edge detection for every groups respectively. And the Sub-pixel edge detection methods we use are:

- 1. Curve-fitting method
- 2. Moment-based method [1]
 - > Invariant rotation and orthogonal
- 3. Reconstructive method [2]
 - > Create a quadratic model with adjacent gray-scale values to the selected points
- 4. Partial area effect method [3]
 - > Create a new mask from camera acquired images

Iterative Curve Fitting (1/5)

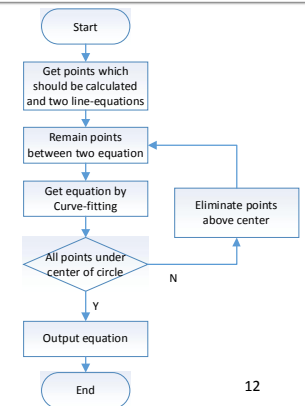
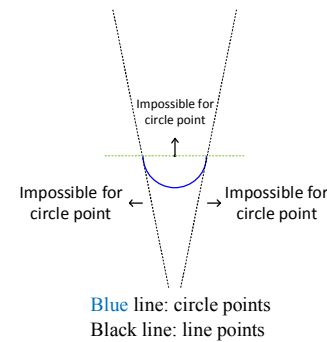
Line case:

iterative times : 0
iterative times : 1
iterative times : 5



Iterative Curve Fitting (2/5)

Circle case:



Iterative Curve Fitting (3/5)

iterative
times : 0
iterative
times : 1
iterative
times : 5

Circle case:



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Iterative Curve-Fitting (4/5)

Curve-fitting

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Iterative Curve Fitting (5/5)

iterative
curve-fitting

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Calculate Angle and Radius

- Angle: Use the cosine theorem

$$\theta = \cos^{-1}\left(\left|\frac{\text{slope}_1 \times \text{slope}_2 + 1}{\sqrt{\text{slope}_1^2 + 1} \times \sqrt{\text{slope}_2^2 + 1}}\right|\right)$$

- Radius: According to parameters of circle equation

Circular equation:

$$x^2 + y^2 + dx + ey + f = 0$$

Radius :

$$R = \frac{1}{2}\sqrt{d^2 + e^2 - 4f}$$

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Result

- M1: Sobel + curve-fitting
- M2: Sobel-Zernike moments [1] + curve-fitting
- M3: Canny + curve-fitting
- M4: Canny + partial area effect [3] + curve-fitting
- M5: Canny + reconstructive [2] + curve-fitting
- M1': Sobel + iterative curve-fitting
- M2': Sobel-Zernike moments [1] + iterative curve-fitting
- M3': Canny + iterative curve-fitting
- M4': Canny + partial area effect [3] + iterative curve-fitting
- M5': Canny + reconstructive [2] + iterative curve-fitting

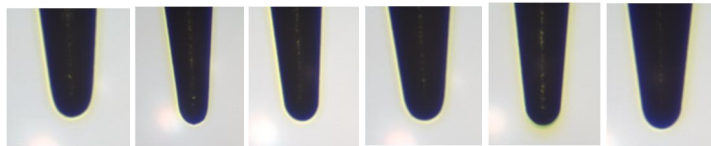


Fig. 1 Fig. 2 Fig. 3 Fig. 4 Fig. 5 Fig. 6

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Angle Result (1/2)

Angle Image	Referred values	M1		M2		M3		M4		M5	
	Angle (degree)	Angle (degree)	Error(%)	Angle (degree)	Error(%)	Angle (degree)	Error(%)	Angle (degree)	Error(%)	Angle (degree)	Error(%)
Fig. 1	11	18.579	68.9	18.748	70.436	11.111	1.009	11.089	0.809	11.027	0.245
Fig. 2	11.2	11.401	1.795	11.427	2.0267	10.847	3.152	10.824	3.357	10.768	3.857
Fig. 3	9.9	13.696	38.343	13.787	39.263	10.063	1.646	10.045	1.464	10.007	1.08
Fig. 4	13.1	18.865	44.007	18.963	44.756	13.247	1.122	13.24	1.068	13.251	1.153
Fig. 5	10.8	11.411	5.657	11.433	5.861	10.824	0.222	10.816	0.148	10.803	0.027
Fig. 6	13.8	14.545	5.399	14.566	5.551	14.011	1.529	13.992	1.391	14.017	1.572
Average error		27.350%		27.982%		1.447%		1.373%		1.322%	

Angle Result (2/2)

Angle Image	Referred values	M1'		M2'		M3'		M4'		M5'	
	Angle (degree)	Angle (degree)	Error(%)	Angle (degree)	Error(%)	Angle (degree)	Error(%)	Angle (degree)	Error(%)	Angle (degree)	Error(%)
Fig. 1	11	13.045	18.591	13.124	19.309	11.054	0.491	11.019	0.172	10.859	1.282
Fig. 2	11.2	11.457	2.295	11.486	2.554	10.826	3.339	10.801	3.563	10.749	4.027
Fig. 3	9.9	11.363	14.777	11.409	15.242	10.063	1.646	10.045	1.465	9.993	0.939
Fig. 4	13.1	14.520	10.832	14.567	11.198	13.232	1.008	13.222	0.931	13.218	0.901
Fig. 5	10.8	11.386	5.426	11.388	5.444	10.824	0.222	10.816	0.148	10.803	0.028
Fig. 6	13.8	14.545	5.399	14.566	5.551	14.011	1.529	13.992	1.391	13.982	1.319
Average error		9.553%		9.883%		1.372%		1.278%		1.416%	

Radius Result (1/2)

Radius Image	Referred values	M1		M2		M3		M4		M5	
	Radius (um)	Radius (um)	Error(%)	Radius (um)	Error(%)	Radius (um)	Error(%)	Radius (um)	Error(%)	Radius (um)	Error(%)
Fig. 1	19.75	128.232	549.276	128.232	549.276	21.132	6.997	21.168	7.179	21.808	10.42
Fig. 2	20.25	70.994	250.588	70.995	250.592	20.512	1.294	20.529	1.378	21.472	6.035
Fig. 3	21.75	90.304	315.190	90.304	315.190	22.320	2.621	22.352	2.768	22.943	5.485
Fig. 4	22.25	134.073	502.575	134.073	502.575	23.165	4.112	23.213	4.328	22.899	2.917
Fig. 5	24.25	102.606	323.117	102.606	323.117	22.417	7.559	22.447	7.435	22.834	5.839
Fig. 6	22.75	194.681	755.741	194.681	755.741	21.976	3.402	22.014	3.235	22.385	1.604
Average error		449.415%		449.416%		4.331%		4.387%		5.383%	

Radius Result (2/2)

Radius Image	Referred values	M1'		M2'		M3'		M4'		M5'	
	Radius (um)	Radius (um)	Error(%)	Radius (um)	Error(%)	Radius (um)	Error(%)	Radius (um)	Error(%)	Radius (um)	Error(%)
Fig. 1	19.75	20.038	1.458	20.064	1.590	21.132	6.997	21.135	7.013	21.346	8.081
Fig. 2	20.25	19.621	3.106	19.624	3.091	20.512	1.294	20.496	1.215	20.496	1.215
Fig. 3	21.75	21.330	1.931	21.318	1.986	22.320	2.621	22.335	2.689	22.574	3.788
Fig. 4	22.25	21.821	1.928	21.824	1.914	23.165	4.112	23.141	4.004	23.167	4.121
Fig. 5	24.25	21.605	10.907	21.610	10.886	22.417	7.559	22.439	7.468	22.704	6.375
Fig. 6	22.75	21.149	7.037	21.137	7.090	21.976	3.402	22.007	3.266	21.925	3.626
Average error		4.395%		4.426%		4.331%		4.276%		4.534%	

Conclusion

- According to the experiment, iterative curve-fitting normally has better results than that without iteration.
- We compare M3' with M4' because they have better results than the others:

	M3'	M4'
Run time (ms)	1473.4	1669.5
Average angle error	1.372%	1.278%
Average radius error	4.331%	4.276%

Platform: Win7 64bit,
Intel Xeon E3-1230V2,
8G RAM

- M3': Canny + iterative curve-fitting
- M4': Canny + partial area effect [3] + iterative curve-fitting
- We use M4' as the algorithm of detecting led probes so far.

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Reference

- [1] Y. D. Qu, C. S. Cui, S. B. Chen, J. Q. Li, "A fast subpixel edge detection method using Sobel-Zernike moments operator," *Image and Vision Computing*, 23 (1), pp. 11-17, 2005.
- [2] Fabijańska, A., Sankowski, D. "Edge detection with sub-pixel accuracy in images of molten metals", *IEEE International Conference on Imaging Systems and Techniques*, Thessaloniki, Greece, pp. 186-191, 2010.
- [3] A. Trujillo-Pino, K. Krissian, M. Alemán-Flores, D. Santana-Cedrés, "Accurate subpixel edge location based on partial area effect", *Image and Vision Computing*, 31, pp. 72-90, 2013.
- [4] N. Q. Chen, J. J. Wang, L. A. Yu, and C. Y. Su, "Sub-pixel Edge Detection of LED Probes Based on Canny Edge Detection and Iterative Curve Fitting", in the *Proc. of IEEE International Symposium on Computer, Consumer and Control*, pp. 131-134, 2014.

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2014 IEEE International Conference
on Automation Science and Engineering

Prognostics for Rolling Bearing Based on
Multiscale Entropy, Permutation Entropy and
Support Vector Data Description

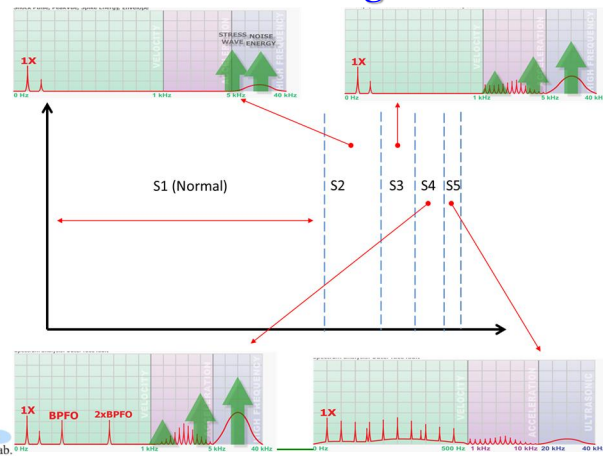


Dr. Shuen-De Wu
August 15, 2014

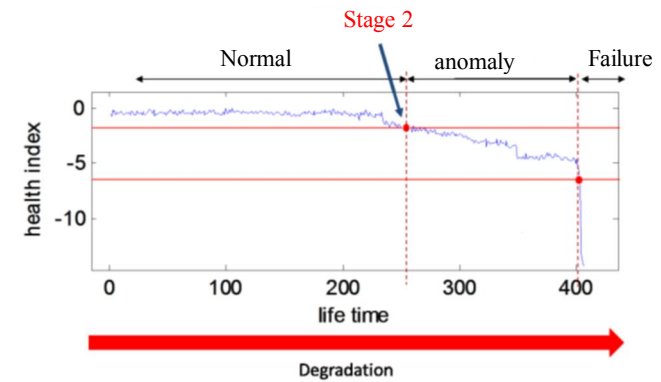
Introduction

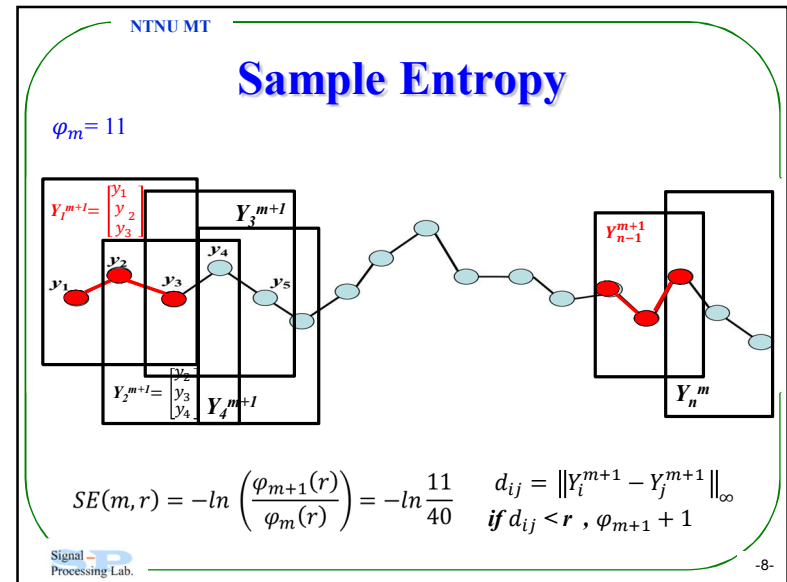
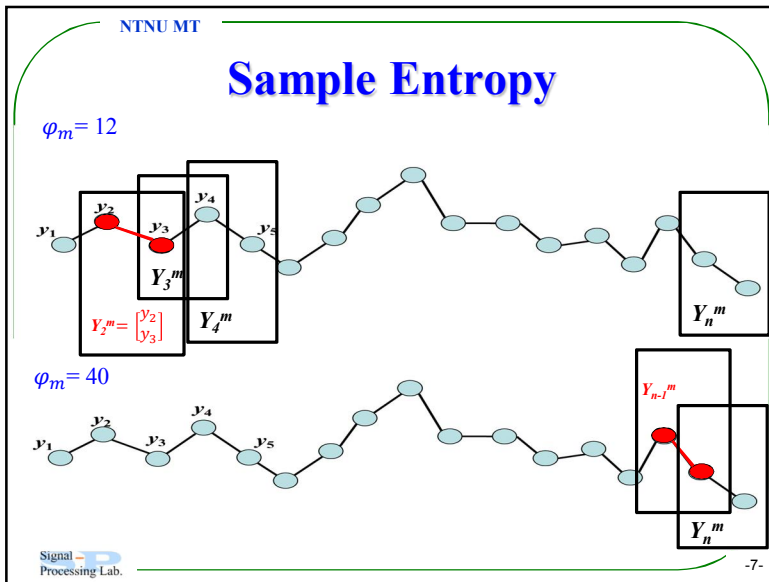
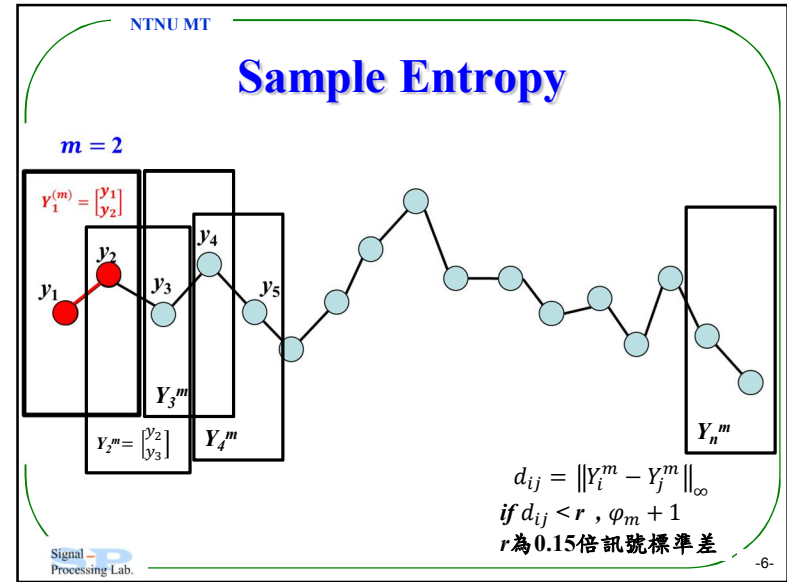
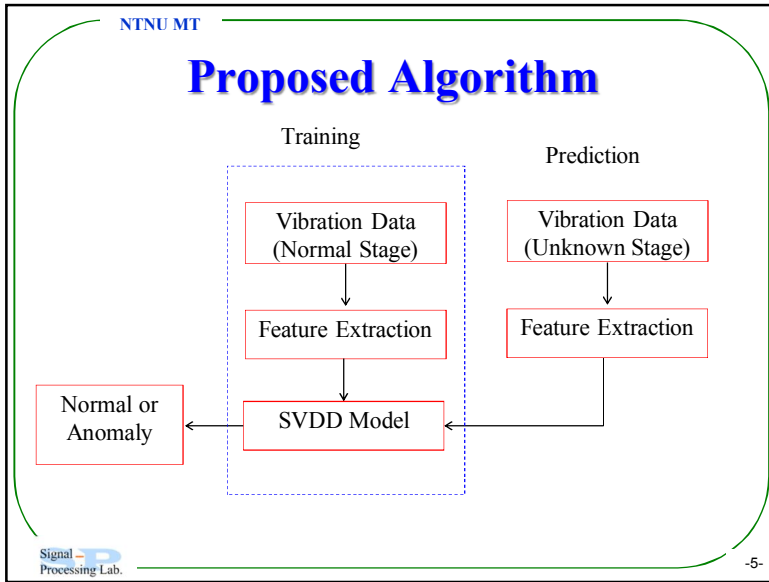
- Rolling bearing failure represents a high percentage of the breakdowns in rotating machinery and may result in catastrophic failures.
- Failure prognosis in long-term predictions are important topics when trying to ensure safety of the operation of machine tool.
- The main issue in prognosis is the ability to detect anomaly of bearing as early as possible.
- In this study, we propose a prognosis algorithm for rolling bearings based on multiscale entropy, permutation entropy and support vector data description.

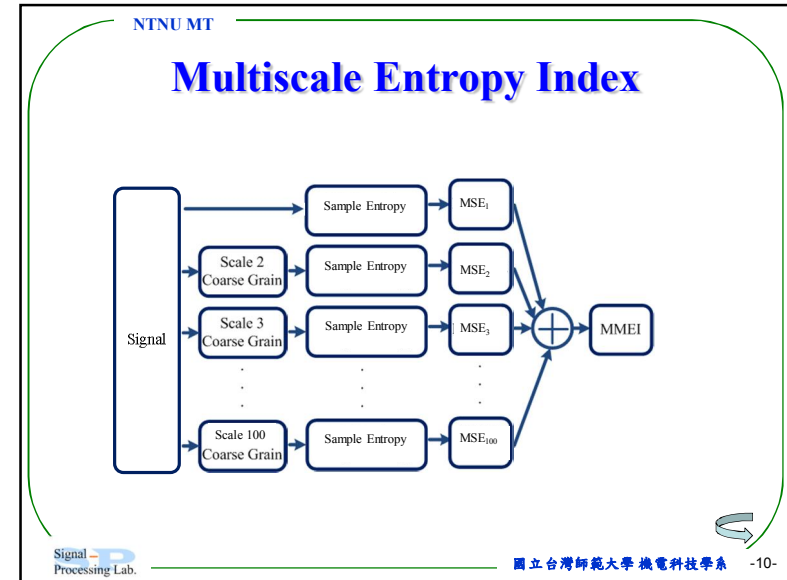
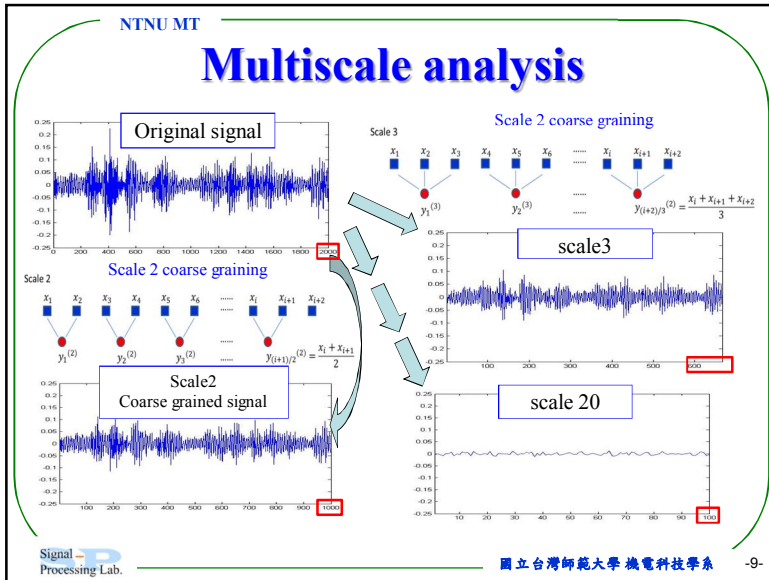
Frequency Response of Bearing at
Different Stages



Anomaly Detection







NTNU MT

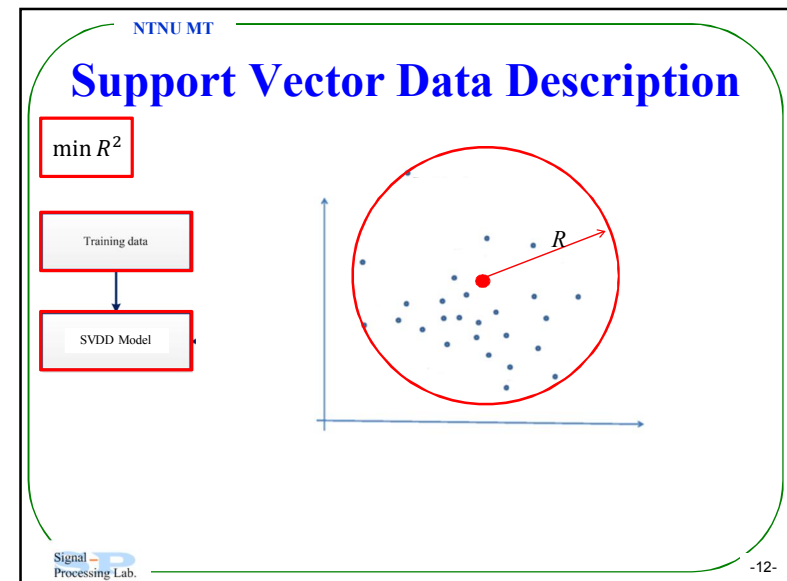
Permutation entropy

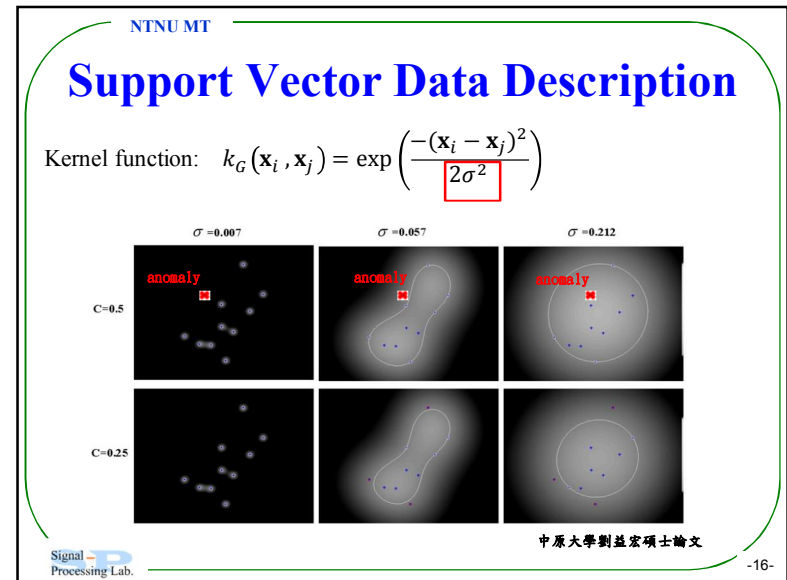
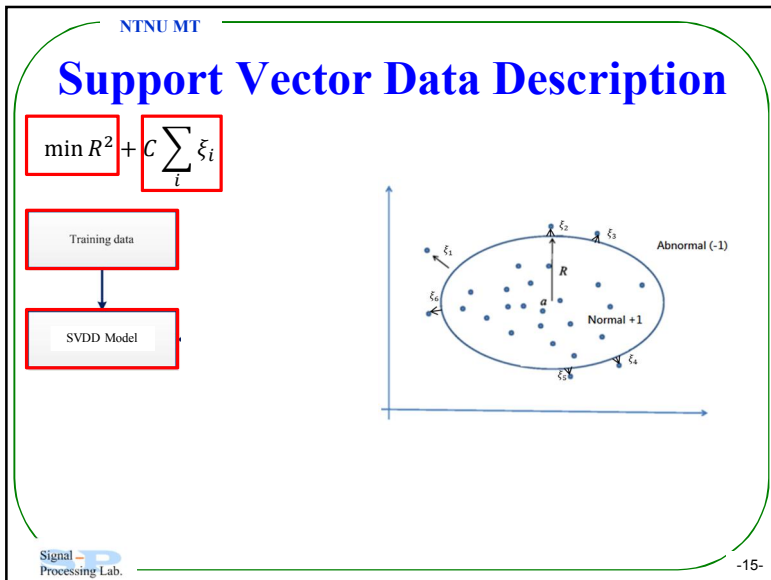
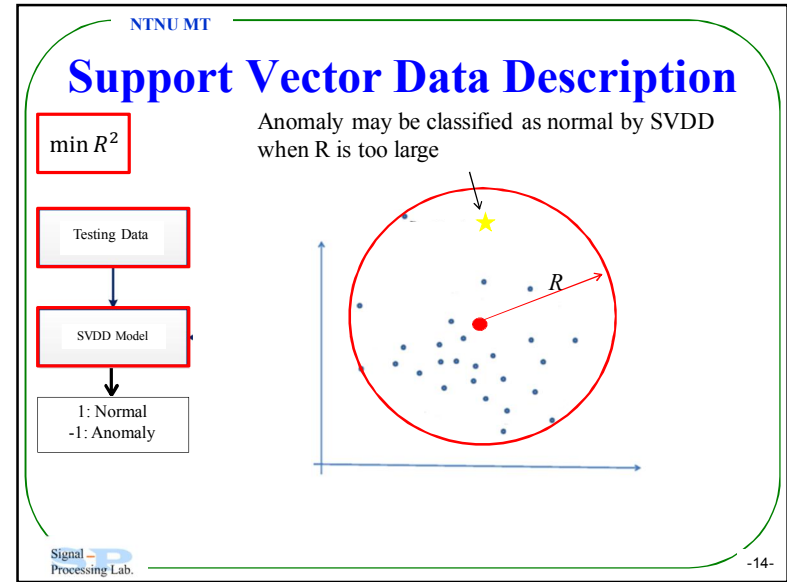
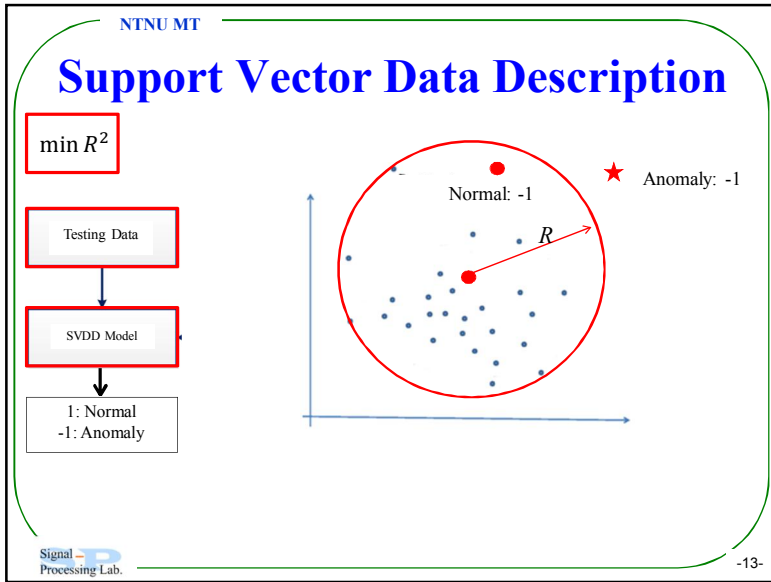
- $x = (4, 7, 9, 10, 6, 11, 3)$ $m = 3$

	0	1	2	
x_1^3	4	7	9	$\leftarrow \pi_{012}$
x_2^3	7	9	10	$\leftarrow \pi_{012}$
x_3^3	9	10	6	$\leftarrow \pi_{201}$
x_4^3	10	6	11	$\leftarrow \pi_{102}$
x_5^3	6	11	3	$\leftarrow \pi_{201}$

- $p(\pi_{012}) = 2/5, p(\pi_{102}) = 1/5, p(\pi_{201}) = 2/5$
- $PE_n(x, 3) = -2/5 \ln(2/5) - 1/5 \ln(1/5) - 2/5 \ln(2/5) = 1.522$
- Normalize: $nPE_n(x, 3) = \frac{1.522}{\ln(3!)} = 0.8494$

Signal Processing Lab. -11-

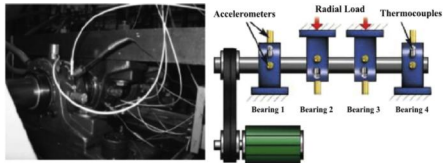




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Experimental Data

- IMS bearing Data
 - Motor speed : 2000 rpm
 - Load : 6000lb
 - Record : 1 sec / 10 min
 - Sampling rate : 20k Hz
 - Time : 164 hr
 - bearing 1 was damaged

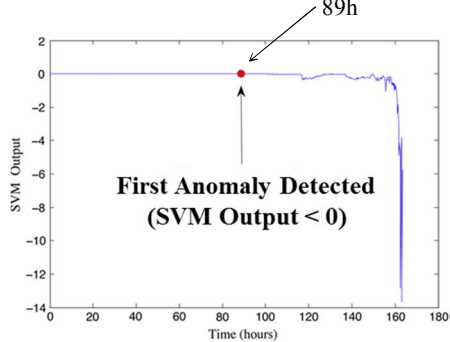


Signal Processing Lab. -17-

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Past Approach

D. Fernandez-Francos, D. Martinez-Rego, O. Fontenla-Romero, and A. Alonso-Betanzos, "Automatic bearing fault diagnosis based on one-class v-SVM," Computers & Industrial Engineering, vol. 64, pp. 357-365, Jan 2013.



89h

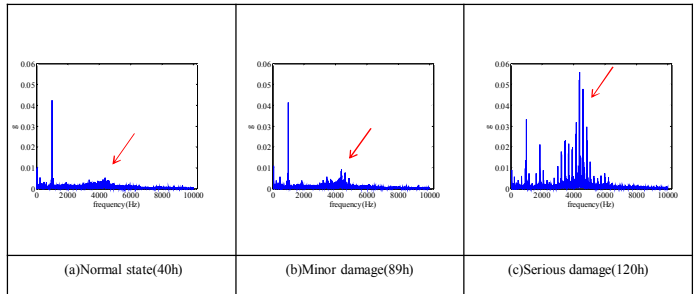
First Anomaly Detected (SVM Output < 0)

Signal Processing Lab. -18-

NTNU MT

Past Approach

- Spectrum analysis of vibration data



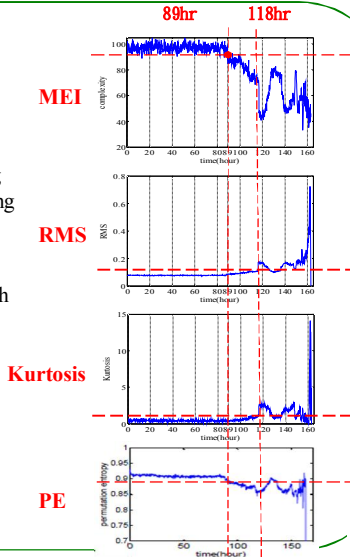
(a) Normal state(40h) (b) Minor damage(89h) (c) Serious damage(120h)

Signal Processing Lab. -19-

NTNU MT

Algorithm 1

- Results
 - Anomaly can be detected by using MEI, PE at 89h after the beginning of experiments
- Difficulty
 - What is the threshold to distinguish anomaly state from normal state?



89hr 118hr

MEI

RMS

Kurtosis

PE

Signal Processing Lab. -20-

