

Interconnection of electrical energy storage systems for power quality improvement

M. Brenna, G.C. Lazaroiu, R. Rotaru, E. Tironi

Abstract--Energy storage is playing an increasingly important role in the electrical power system thanks to the development and advance in various energy storage and power electronics technologies in recent years. The paper inquires into energy storage examining electrical energy storage devices, especially supercapacitors. Relative on these energy storage concerns, different dc/dc converters were analyzed using the EMTP/ATPDraw program to observe their behavior on different parameters such as: duty cycle, switching frequency or capacitance. Moreover the effects of the switching frequency variation have been analyzed.

Index Terms— boost converter, buck converter, DC/DC converters, supercapacitors, THD

I. INTRODUCTION

THE energy storage is playing an increasingly important role in the electrical power system thanks to the development and advance in various energy storage and power electronics technologies in recent years. On the other hand, the increase in electrical load, the tendency to operate the power system closer to its limit, and the associated reliability issues are driving the development of the energy storage technologies and their applications [1].

The dc/dc converters have attracted special interest in various fields related to the alternative and renewable energy generation and power supplies of small-scale distributed type photovoltaic generation system (PVGS), fuel cell generation system (FCGS), battery and supercapacitor energy storage systems [2].

Relative on these energy storage concerns it were simulated different dc/dc converters, using the ATP Program to observe their behavior on different parameters variations, such as: duty cycle, switching frequency, and capacitance. The simulation are realized in particular on buck and boost chopper, two different converters that will form the device used in energy storage buck-boost.

M. Brenna is with the Department of Energy of the Politecnico di Milano, Milan, Italy (e-mail: morris.brenna@polimi.it).

G. C. Lazaroiu is with the Department of Electrical Engineering, University Politehnica of Bucharest, Splaiul Independentei 313, Bucharest, Romania (e-mail: clazaroiu@yahoo.com).

R. Rotaru is with S.C. Metroul S.A., Gutenberg Street 3, 050027 Bucharest, Romania (e-mail: rodica.rotaru@metroul.ro)

E. Tironi is with the Department of Electrical Engineering of the Politecnico di Milano, piazza Leonardo da Vinci 32, Milano 20133, Italy (e-mail: enrico.tironi@polimi.it)

II. ELECTRICAL ENERGY STORAGE

Supercapacitors are electrochemical capacitors that have an unusual high energy density when compared to common capacitors, typically on the order of thousands of times greater than a high-capacity electrolytic capacitor.

The electrical double layer is a structure that describes the variation of electric potential near a surface, and has a large bearing on the behavior of colloids and other surfaces in contact with solutions and solid state fast ion conductors.

The analogue in plasma is the double layer. An electrolytic capacitor is a type of capacitor typically with a larger capacitance per unit volume than other types, making them valuable in relatively high-current and low-frequency electrical circuits.

This is especially the case in power-supply filters, where they store charge needed to moderate output voltage and current fluctuations, in rectifier output, and especially in the absence of rechargeable batteries that can provide similar low-frequency current capacity [3, 4].

Supercapacitors can be viewed as two non-reactive porous plates suspended within an electrolyte, with a voltage applied across the plates. The applied potential on the positive plate attracts the negative ions in the electrolyte, while the potential on the negative plates attracts the positive ions.

This effectively creates those two layers of capacity storage, one where the charges are separated at the positive plate, and another at the negative plate.

Supercapacitors are normally designed and optimized in dedicated applications. The charging and discharging times are decided accordingly.

Commercial capacitors are designed for specific purpose such as switchgear, power quality, high speed photography and repetitive applications as shown in Table I.

TABLE I APPLICATION ORIENTED CHARGE AND DISCHARGE TIMES OF SUPERCAPACITORS

Applications	Charging time	Discharging time
Switchgears	60 - 120 s	20 - 50 s
Power Quality	50 - 100 s	10 ms-10 s
Flash lamps	10 - 20 s	1 -100 ms
Pulsed	<1.0ms	> 1.0 ms

Supercapacitors have relatively longer charge and discharge times; at least > 1.0 ms so they are not good for storing microsecond lightning pulses. However, normal capacitors may be considered as an alternative. The dc

batteries, whatsoever, are absolutely unable to store lightning surges [5]. Supercapacitors are much more suitable for leveling voltage/current sags created by short circuit faults on power system. Thus the primary applications of supercapacitors are more attractive for, vehicles and power quality area.

III. DC/DC CONVERTERS

In recent years, the higher efficiency and the more advanced power conversion, the energy utilization equipment, the variety of circuit topologies of the soft switching dc/dc power converter are spread used. A dc/dc converter is a device that accepts a dc input voltage and produces a dc output voltage [6, 7]. Typically the output produced is at a different voltage level than the input.

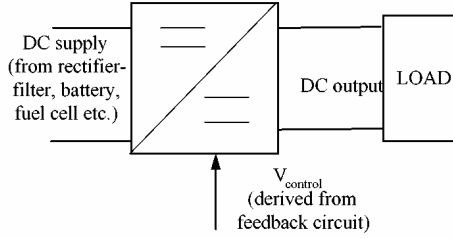


Fig. 1. General block diagram of a DC-DC converter.

A. Buck (step-down) converter

The model implemented in ATP Program is shown in Fig. 2.

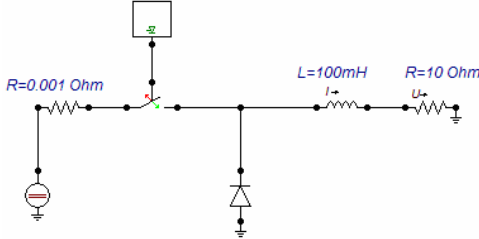


Fig. 2. Model of the buck chopper implemented in ATPDraw.

To evaluate the quality of the converter output waveform can be expressed by using the Fourier analysis data to calculate the total harmonic distortion (THD) in relative values for voltage using (1).

$$THD_V = \frac{\sqrt{V_1^2 + V_2^2 + V_3^2 + \dots + V_n^2}}{V_0} \quad (1)$$

Firstly, the influence of the duty cycle variation on the total harmonic distortion of the output voltage is investigated. The duty cycle δ is varied between 0.1 and 0.9, and the switching frequency is set $f_{sw} = 1000$ Hz. The inductance is set to 100mH. The total harmonic distortion in relative values is reported in Table II [8].

TABLE II. VARIATION OF (THD_V) WITH THE DUTY CYCLE IN RELATIVE VALUES

δ	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
THD_V	3.67	3.26	2.85	2.44	2.04	1.63	1.22	0.81	0.41

The variation of THD values with the duty cycle δ is shown in Fig. 3. According to Fig. 3, the dependence between THD and duty cycle is a linear one because the continue component on which we divided the square root is a bigger one.

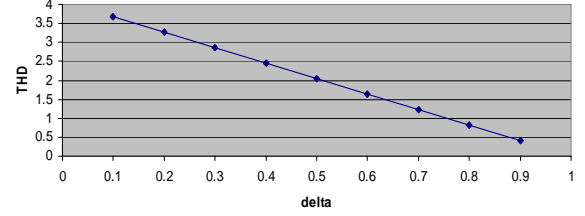


Fig. 3. Variation of the THD_V with the duty cycle δ .

The simplest way to reduce a DC voltage is to use a voltage divider circuit, but voltage dividers waste energy, since operated by bleeding off excess voltage as heat; also, output voltage isn't regulated (varies with input voltage). Admittedly that buck chopper is a step-down converter, on the other hand, can be remarkably efficient (easily up to 95% for integrated circuits) and self-regulating, making it useful for tasks.

Therefore, can be observe that the output voltage is lower on $\delta=0.1$ that means a directly proportionality between output voltage waveform and duty cycle δ , Fig. 4.

The quality of the output waveform of the buck chopper is tending to be a very good one when the constant δ is approaching to value $\delta=1$, also the ripple is becoming smaller but on the same time the output voltage is increased. Fig. 5 shows the variation of the output voltage and input current for the duty cycle $\delta=0.9$, $f_{sw}=1000$ Hz, $L=100$ mH.

Increasing the duty cycle δ will slow down the stability, the time to get to stability point will be bigger such as: for $\delta=0.1$ the output voltage waveform is stabilized after 0.03s (Fig. 4), and for $\delta=0.9$ after 0.04s (Fig. 5).

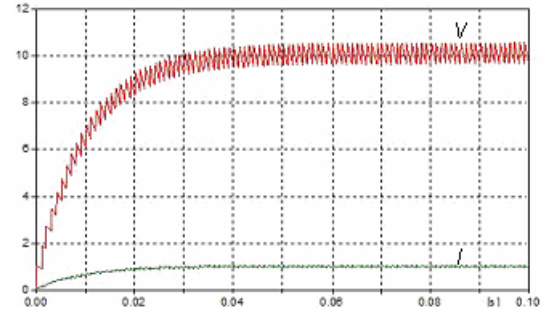


Fig. 4. Variation of the voltage and current for $\delta=0.1$, $f_{sw}=1000$ Hz, $L=100$ mH

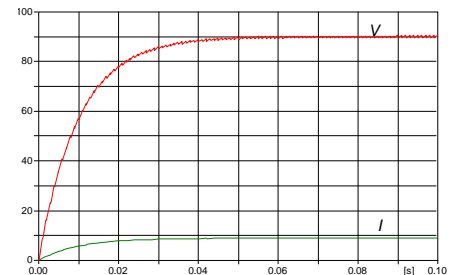


Fig. 5. Variation of the voltage and current for $\delta=0.9$, $f_{sw}=1000$ Hz, $L=100$ mH

Secondly, the influence of the switching frequency variation on the total harmonic distortion of the output voltage is investigated. The switching frequency is varied between 1kHz and 10kHz, while the duty cycle is set $\delta=0.5$. The variation of THD_V with the switching frequency is shown in Fig. 6.

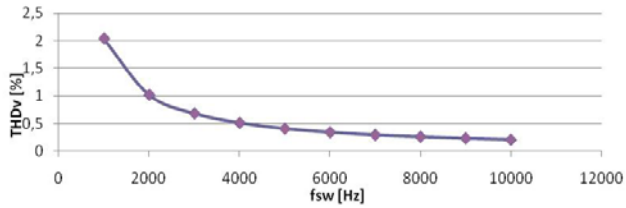


Fig. 6. Variation of the THD_V with the switching frequency f_{sw} .

Fig. 6 shows that increasing of the switching frequency, the THD_V becomes lower, which means a higher quality of output waveform.

Based on the harmonic distributions, on lower switching frequency $f_{sw}=1000\text{Hz}$, the fundamental harmonic is almost 50V, while on $f_{sw}=5000\text{Hz}$ it is becoming 250V, at $f_{sw}=10000\text{Hz}$ is 500V, which means it is a directly proportionality between switching frequency and fundamental harmonic.

Fig. 7 shows the variation of the output voltage and input current for the duty cycle $\delta=0.5$, $L=100\text{mH}$ and $f_{sw}=1000\text{Hz}$, while Fig. 8 shows the variation of the output voltage and input current for the duty cycle $\delta=0.5$, $L=100\text{mH}$ and $f_{sw}=10000\text{Hz}$.

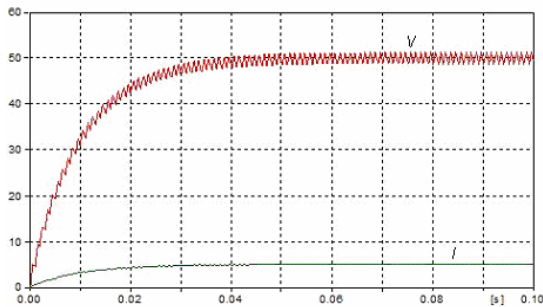


Fig. 7. Variation of the voltage and current for $\delta=0.5$, $L=100\text{mH}$, $f_{sw}=1000\text{Hz}$

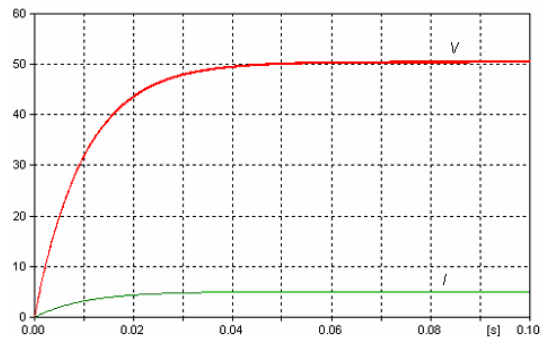


Fig. 8. Variation of the voltage and current for $\delta=0.5$, $L=100\text{mH}$, $f_{sw}=10000\text{Hz}$

B. Boost (step-up) converter

The boost converter (step-up converter) is a power converter with an output dc voltage greater than its input dc voltage. The model implemented in ATP Program is shown in Fig. 9.

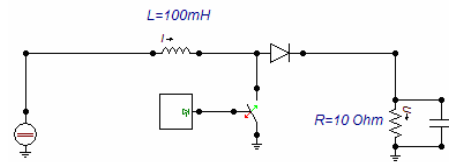


Fig. 9. Model of the buck chopper implemented in ATPDraw.

As for the buck converter, the investigation of the duty cycle and switching frequency influence on the THD_V are considered. In addition, the variation of the THD with the capacitance C of the capacitor is considered.

The total harmonic distortion (THD) in relative values is reported in Table III.

TABLE III. VARIATION OF (THD_V) WITH THE DUTY CYCLE IN RELATIVE VALUES

δ	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
THD_V	0.41	0.82	1.22	1.63	2.04	2.45	2.86	3.31	3.80

The variation of THD values with the duty cycle δ is shown in Fig. 10. The variation of THD values with the duty cycle δ is a linear one, as for the case of the buck converter. The quality of the output waveform of the buck chopper is tending to be a very good one when the constant δ is approaching to value $\delta=0.1$, also the ripple is becoming smaller but on the same time the output voltage is increased.

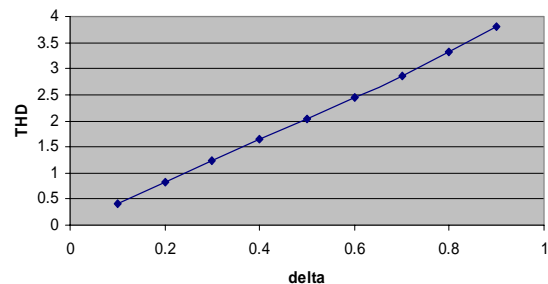


Fig. 10. Variation of the THD_V with the duty cycle δ .

Increasing the duty cycle δ will slow down the stability, the time to get to stability point will be bigger such as: for $\delta=0.5$ the output voltage waveform is stabilized after 0.1s (Fig. 11), and for $\delta=0.8$ after 0.6s (Fig. 12).

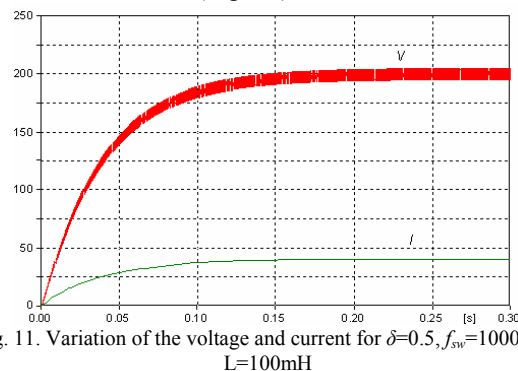


Fig. 11. Variation of the voltage and current for $\delta=0.5$, $f_{sw}=10000\text{Hz}$, $L=100\text{mH}$

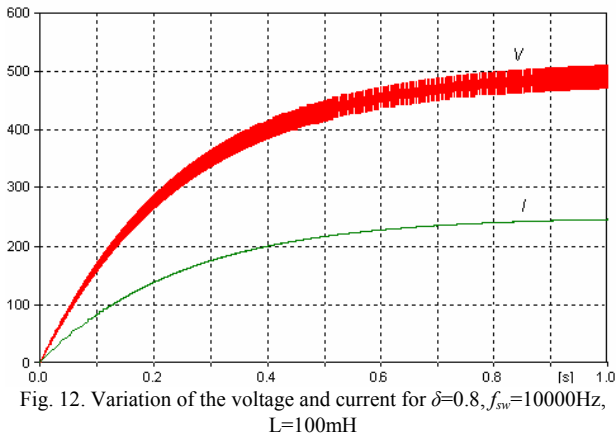


Fig. 12. Variation of the voltage and current for $\delta=0.8, f_{sw}=10000\text{Hz}, L=100\text{mH}$

Secondly, the influence of the switching frequency variation on the total harmonic distortion of the output voltage is investigated. The switching frequency is varied between 1kHz and 10kHz, while the duty cycle δ is set $\delta=0.5$. The variation of THD_v with the switching frequency is shown in Fig. 13. It can be observed that after a frequency of $f_{sw}=4000\text{Hz}$, the dependence between THD and switching frequency is not changing very much.

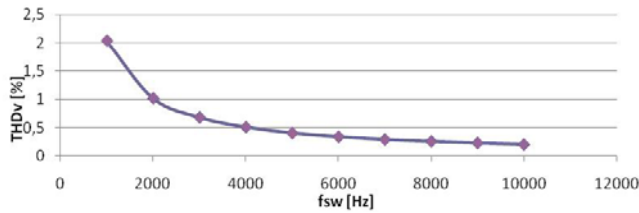


Fig. 13. Variation of the THD_v with the switching frequency f_{sw} .

Fig. 14 shows the variation of the output voltage and input current for the duty cycle $\delta=0.5, L=100\text{mH}$ and $f_{sw}=1000\text{Hz}$, while Fig. 15 shows the variation of the output voltage and input current for the duty cycle $\delta=0.5, L=100\text{mH}$ and $f_{sw}=10000\text{Hz}$.

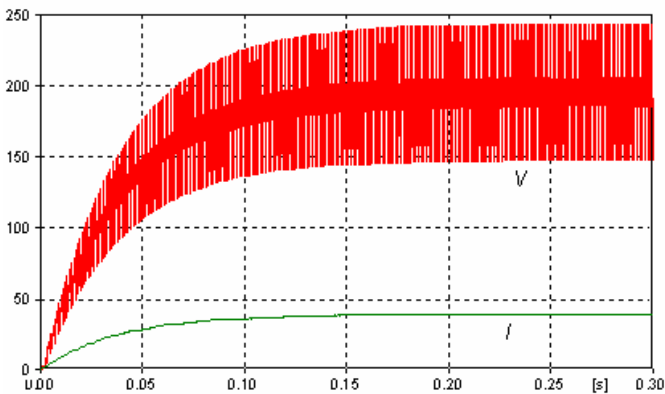


Fig. 14. Variation of the voltage and current for $\delta=0.5, L=100\text{mH}, f_{sw}=1000\text{Hz}$

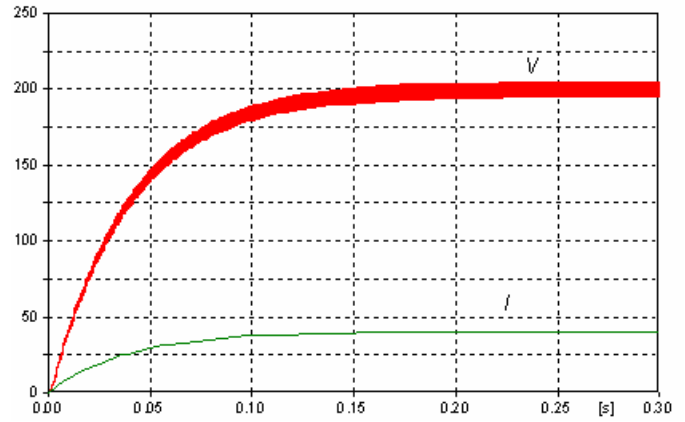


Fig. 15. Variation of the voltage and current for $\delta=0.5, L=100\text{mH}, f_{sw}=10000\text{Hz}$

The time to get to stability is almost the same and is not changing with the increase of the switching frequency. It can be observed that the ripple factor, also the amplitude, decrease by increasing the switching frequency.

When the duty cycle is kept constant $\delta=0.5$ and the switching frequency is set $f_{sw}=1000\text{Hz}$, the capacitance is varied between $100\mu\text{F}$ and $3000\mu\text{F}$, with a step of $300\mu\text{F}$. The variation of THD values with the capacitance C is shown in Fig. 16.

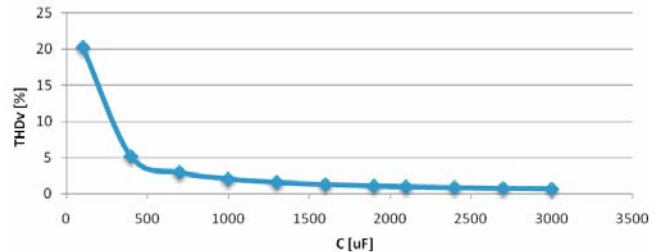


Fig. 16. Variation of the THD_v with the capacitance C .

It can be observed that for a capacitance greater as $700\mu\text{F}$, the dependence between THD and the capacitance is not so important. The explanation is the fact that the efficiency is not a linear one. The ripple factor decreases with the increase of the capacitance.

For $\delta=0.5$ and for a switching frequency of 1000Hz , the variation of the voltage and current with respect to the capacitance C are illustrated in Fig. 17 and Fig. 18.

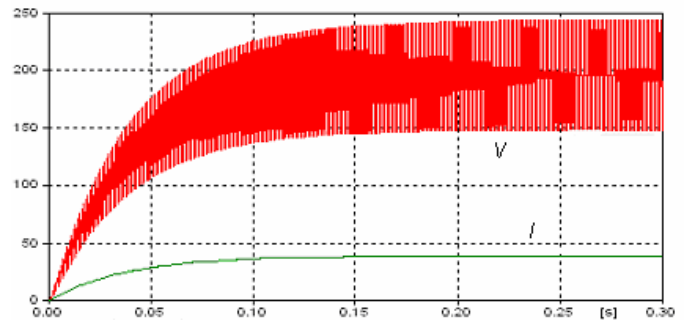


Fig. 17. Variation of the voltage and current for $\delta=0.5, L=100\text{mH}, f_{sw}=1000\text{Hz}$ and $C=100\mu\text{F}$.

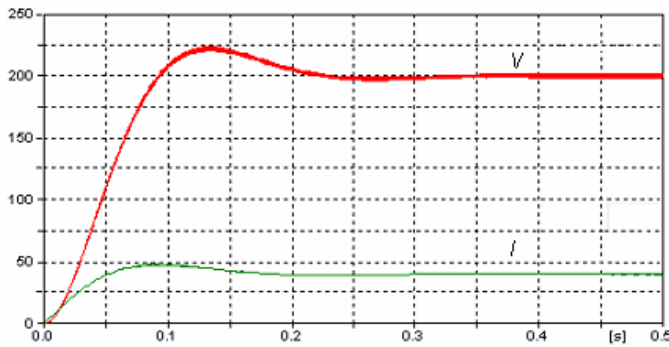


Fig. 18. Variation of the voltage and current for $\delta=0.5$, $L=100\text{mH}$, $f_{\text{sw}}=1000\text{Hz}$ and $C=3000\ \mu\text{F}$.

IV. CONCLUSIONS

The energy storage is playing an increasingly important role in the electrical power system thanks to the development and advance in various energy storage and power electronics technologies in recent years. On the other hand, the increase in electrical load, the tendency to operate the power system closer to its limit, and the associated reliability issues are driving the development of the energy storage technologies and their applications.

The simulations realized using the ATP Program on the dc converters for different duty cycle, switching frequency, and capacitance show how the characteristics of these two choppers can be varied. For the buck converter, variation of the duty cycle decreases the ripple. For the boost it has a different variation because the ripple is also influenced by capacitance value giving the boost operation. If a decrease of ripple, maintaining the switching frequency constant, is desired the buck will need a higher duty cycle; the boost will need a lower duty cycle without varying the capacitance, or 0.5 value if the capacitance is increased.

Referring to the operation of these converters during the switching frequency keeping on the duty cycle at the medium value it can be observed that the ripple factor decreased if the switching frequency it is augmented. Therefore, in the future and also today they are used converters on high switching frequency even to improve power quality on energy storage.

V. REFERENCES

- [1] R. Rotaru, "Interconnection of electrical energy storage systems for power quality improvement" graduation project, Department of. Power Systems, University POLITEHNICA of Bucharest, 2008.
- [2] M. Brenna, G. C. Lazaroiu, E. Tironi, "High Power Quality and DG Integrated Low Voltage dc Distribution System", in *Proc. IEEE Power Engineering Society General Meeting 2006*, June 18-22, Montreal, Canada, pp. 6
- [3] Francis P. Malaspina and Fort Pierce, Fla. *Supercapacitor Electrode and Method of Fabrication Theory*, 1990
- [4] Marie-Francoise, J.-N. Gualous, H. Berthon, A., Supercapacitor thermal- and electrical-behaviour modelling using ANN, *IEE Proceedings on Electric Power Applications*, vol. 153, no. 2, pag. 252-263
- [5] *IEEE Standard for interconnecting distributed resources with electric power systems*, IEEE Standard 1547, 2003.

- [6] N. Mohan, T. Undeland, W. Robbins, *Power Electronics*, John Wiley & Sons, 2003.
- [7] A. Kislovski, R. Redl, and N. Sokal, *Dynamic Analysis of Switching-Mode DC/DC Converters*, New York: Van Nostrand Reinhold, 1994.
- [8] *IEEE recommended practice for monitoring electric power quality*, IEEE Standard 1159, 1995

VI. BIOGRAPHIES

Morris Brenna received the M.S. degree in Electrical Engineering from the Politecnico di Milano, Italy, in 1999 and the Ph.D. degree in 2003, where he is assistant professor in the Department of Energy. His current research interests include power electronics, distributed generation, traction systems and electromagnetic compatibility. He is a member of Italian Electrical Association (AEI) and Italian Railways Engineering Association (CIFI).

R. Rotaru received the B.Sc from the Department of Electrical Engineering, University POLITEHNICA of Bucharest in 2008. She is currently studying Electrical Advanced Power Networks on Master program on University POLITEHNICA of Bucharest. She is currently Design Electrical Engineer on Metroul S.A.

George Cristian Lazaroiu received the B.Sc and M.Sc. from the Department of Electrical Engineering, University POLITEHNICA of Bucharest, in 2002 and 2003 respectively, where he is assistant professor. He received the Ph.D. degree in Electrical Engineering, from Politecnico di Milano in 2006. His areas of research include distributed generation, power electronics and power quality.

Enrico Tironi received the M.S. degree in Electrical Engineering from the Politecnico di Milano, Italy, in 1972. In 1972 he joined the Department of Electrical Engineering of the Politecnico di Milano where he is Full Professor and Head of Department at present. His areas of research include power electronics, power quality and distributed generation. He is a member of Italian Standard Authority (C.E.I.), Italian Electrical Association (A.E.I.) and Italian National Research Council (C.N.R.) group of Electrical Power System.