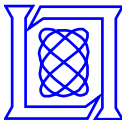


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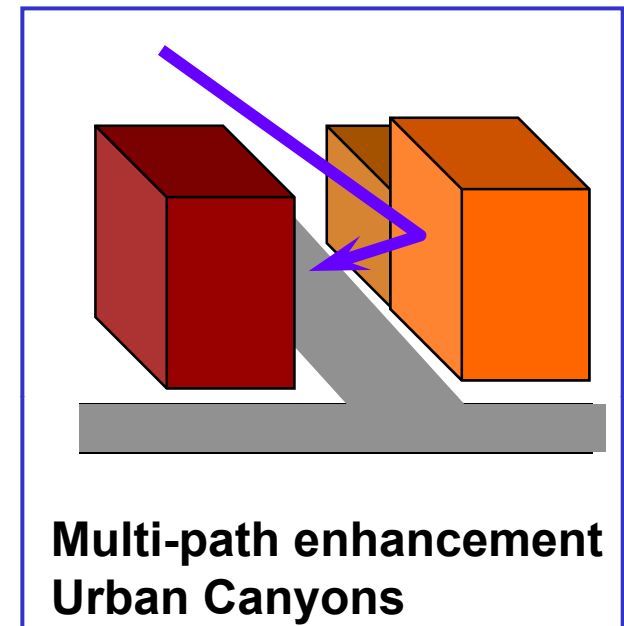
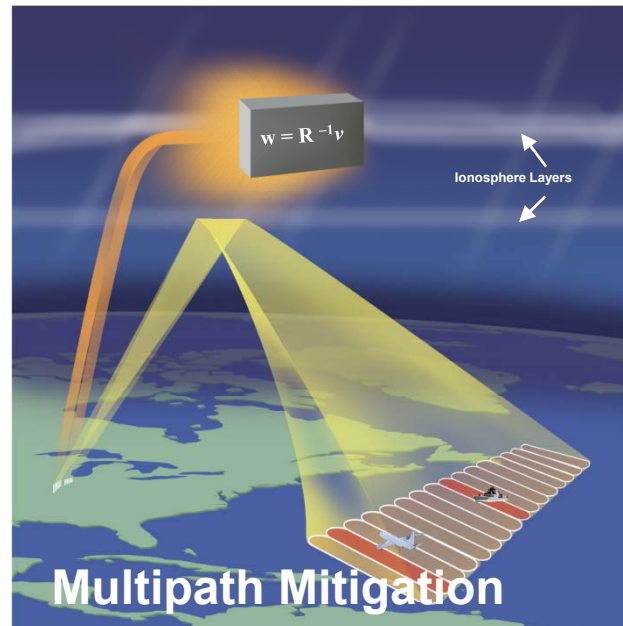
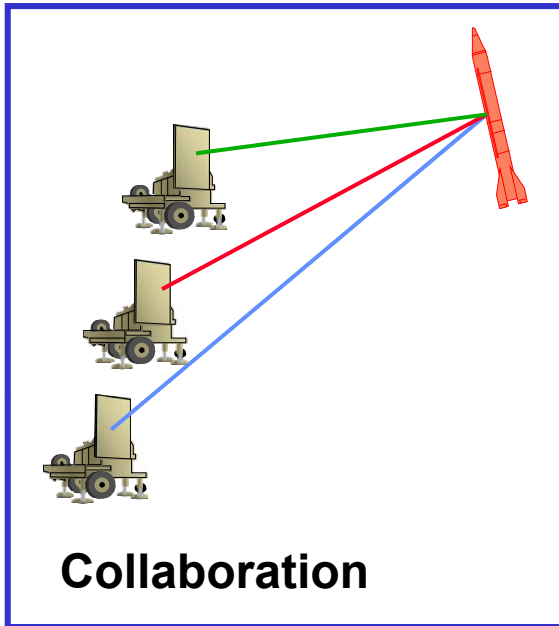
# **MIMO Radar SIMO Equivalence And the Resulting Waveform Constraints**

**By Dr. Frank Robey  
Presentation for  
IEEE AESS Dayton Section  
Previously presented at:  
Defense Applications of Signal Processing  
5/27/2010**

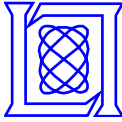
This research effort was supported by the Department of the Air Force under Contract FA8721-05-C-0002. Opinions, interpretations, conclusions and recommendations are those of the author and are not necessarily endorsed by the United States Government.



# Coherent MIMO Application



- **Coherent MIMO utilizes control system *observability***
  - Understand and observe propagation of signals in environment
- **Application of multi-variate control to radar**



# Outline

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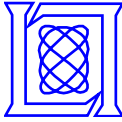
- Introduction
- • **Coherent MIMO Surveillance Radar Range Equation**
- Comparison and Assumptions
- Conclusion



# Briefing Purpose

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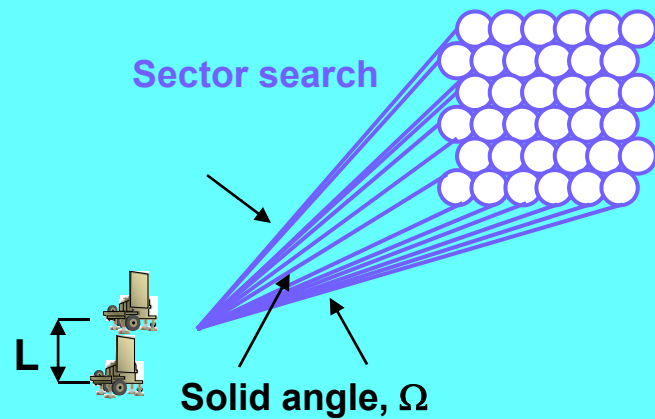
- **MIMO has observability advantages over SIMO radar**
  - Ability to understand signal propagation in environment
  - Observability is key to controlling environment impact on radar
- **What is impact on surveillance SNR?**
- **What assumptions are made?**
  - How can this SNR be realized?



# Pseudo-Monostatic MIMO Radar

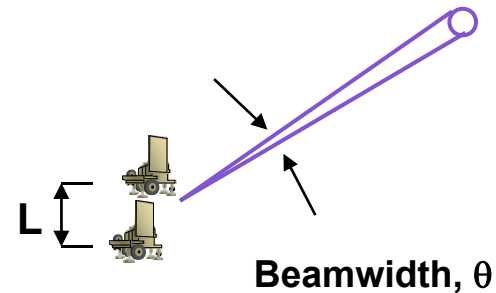
## Search Radar

Determine target presence over region in space



## Track Radar

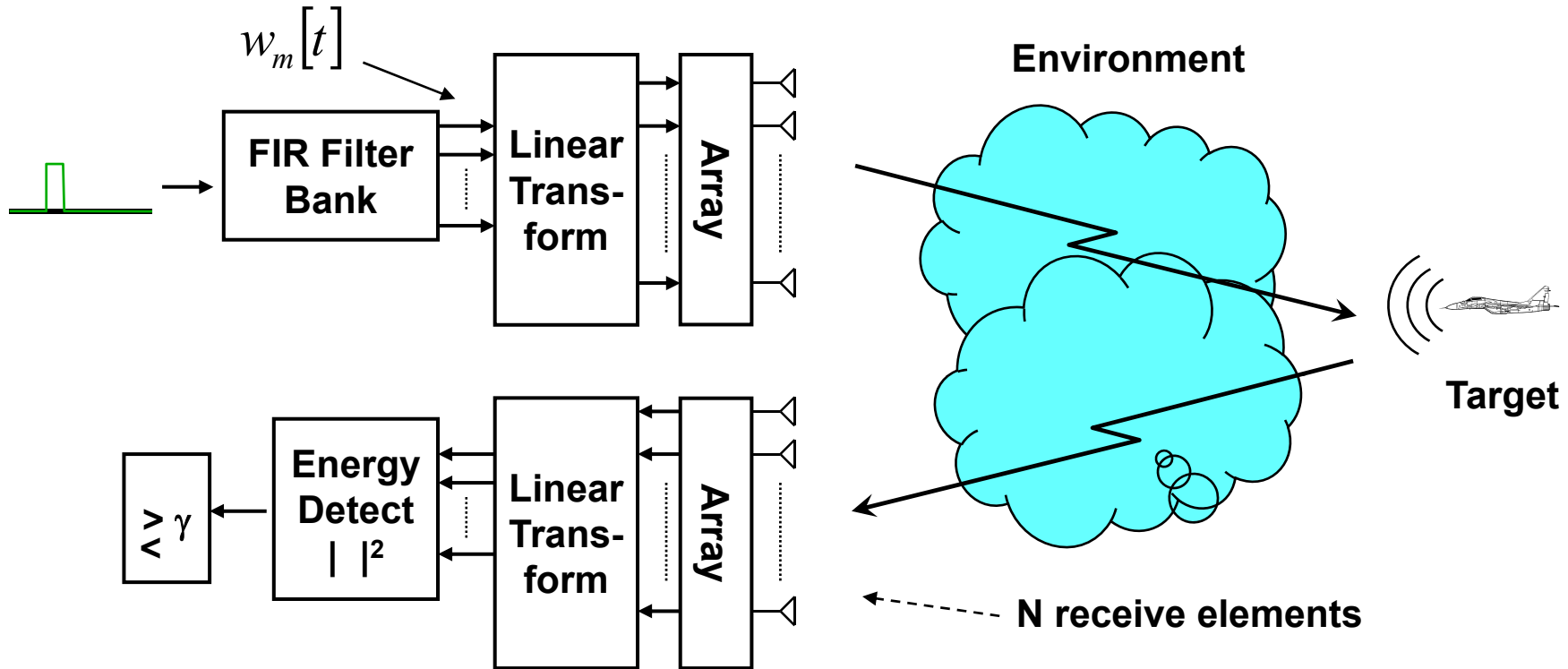
Parameter estimation at known location



- Detect and locate targets in desired surveillance sector  $\Omega$
- Sensor spacing and range are such that angle differences from each aperture are negligible



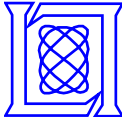
# Coherent MIMO Radar



- Single impulse synchronizes system
- $M$  linearly-independent/orthogonal waveforms

$$\sum_{i=1}^L w_m[i] w_n^*[i+j] = |a_m|^2 \delta[m-n] \delta[j]$$

- FIR filter bank model represents the three methods of achieving orthogonality: code division, frequency division, time division



# Outline

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- **Introduction**
- **Coherent MIMO Surveillance Radar Range Equation**
- **Comparison and Assumptions**
- **Conclusion**



# MIMO Radar Range Equation (1)

Energy density from radar transmitting spherical wave into solid angle  $\Omega$

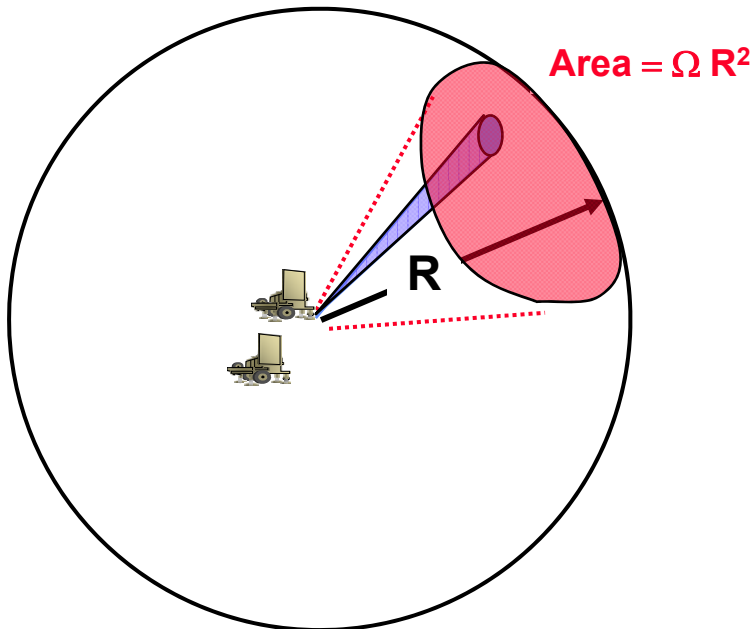
$$\frac{P T}{\Omega R^2}$$

$P$  = average transmitter power

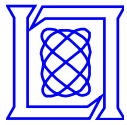
$$\sum_{m=1}^M |a_m|^2 = P T$$

$T$  = time to search solid angle  $\Omega$

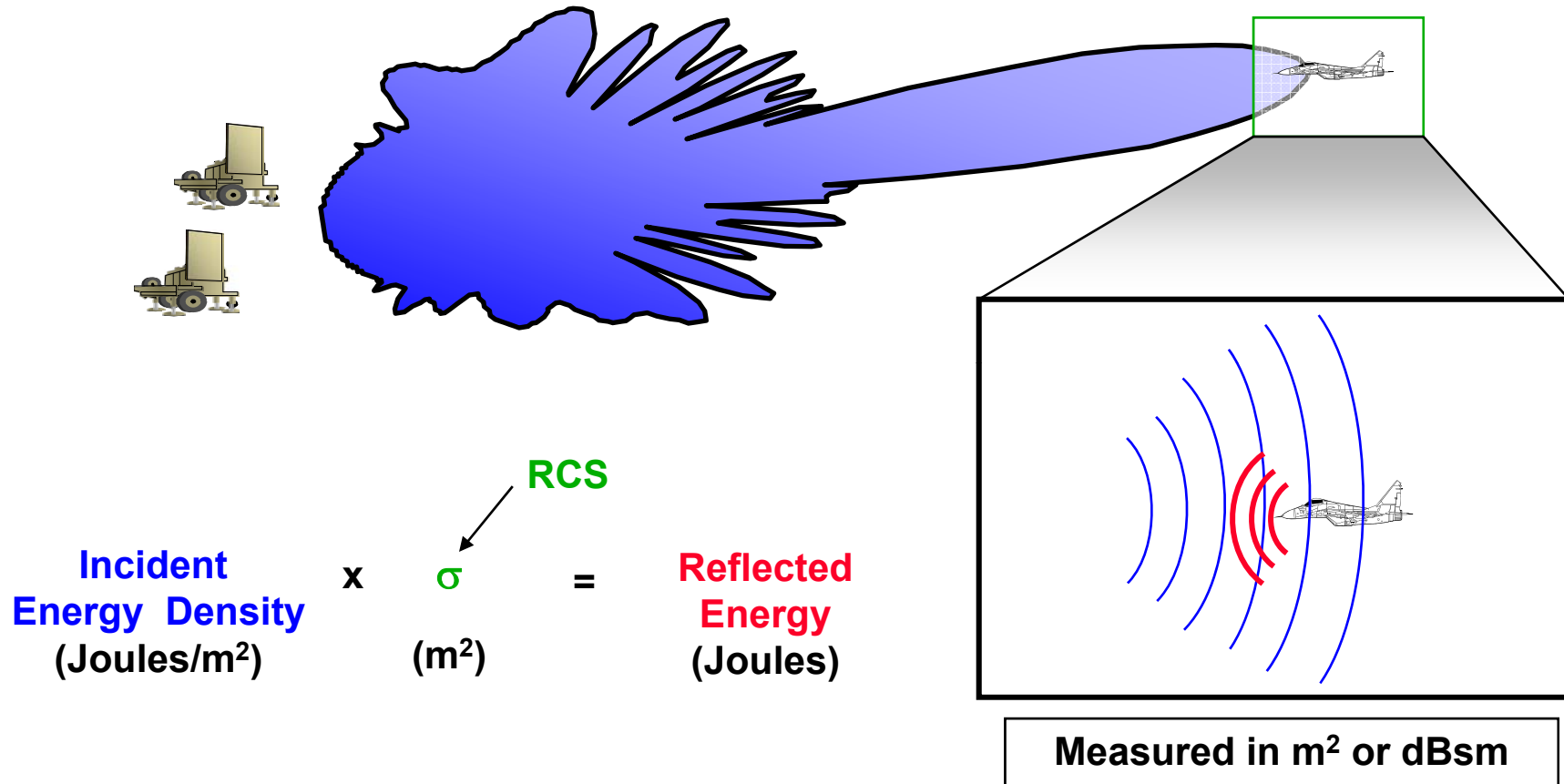
$R$  = distance from radar



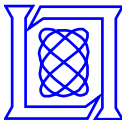




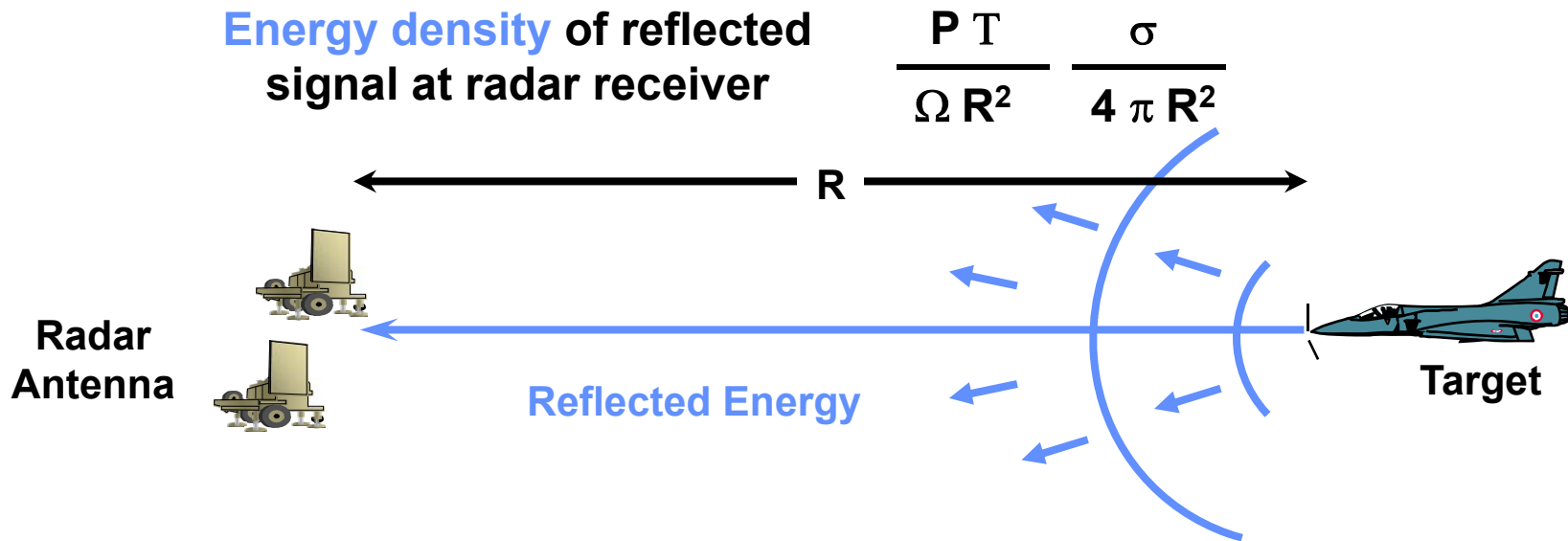
# Pseudo-Monostatic Radar Cross Section (RCS)



- Radar Cross Section (RCS, or  $\sigma$ ) magnitude is identical for all apertures (the effective cross-sectional area of the target as seen by the radar)



# Search Radar Range Equation (2)



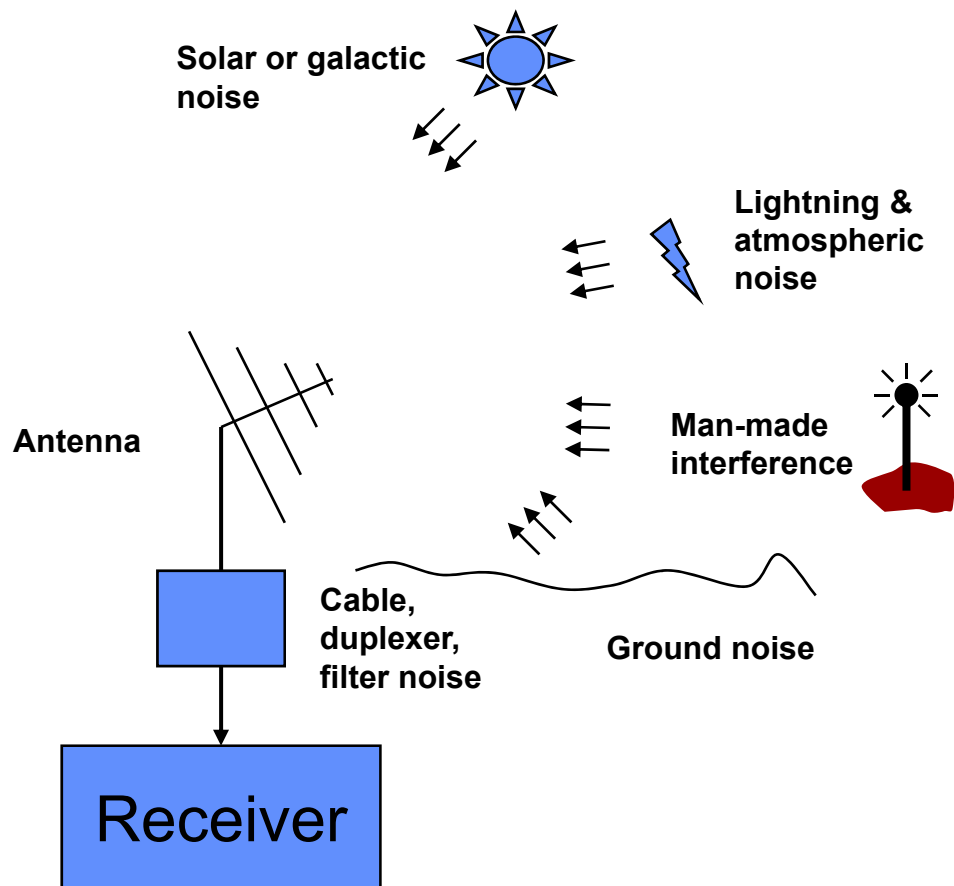
**Energy of reflected signal from target and received by radar**

$$E_r = \frac{P_T}{\Omega R^2} \frac{\sigma A_e N}{4\pi R^2}$$

- $E_r$  = Energy received
- $A_e$  = Effective area of each receiving antenna
- $N$  = Number of receive aperture



# Received Noise



Total effect represented by a single noise source at the antenna output terminal.

The noise energy at the receiver is given by:

$$N_r = k T_s$$

$k$  = Boltzmann's constant  
=  $1.38 \times 10^{-23}$  joules/Kelvin  
 $T_s$  = System Noise Temperature



## Search Radar Range Equation (3)

---

Signal Energy reflected  
from target and  
received by radar

$$E_r = \frac{P T}{\Omega R^2} \frac{\sigma A_e N}{4 \pi R^2}$$

Average Noise Energy

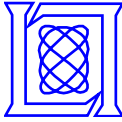
$$N_r = k T_s$$

Signal to Noise Ratio

$$\text{SNR} = E_r / N_r L$$

L = Loss Factor

$$\text{SNR} = \frac{P T A_e N \sigma}{4 \pi \Omega R^4 k T_s L}$$



# Receive Signal Processing

- Matrix of receive data (N by P)

$$\mathbf{Y} = \mathbf{d}(\varphi_r) \mathbf{s}^H(\varphi_t) + \mathbf{N}$$

Each element of  $\mathbf{N}$ ,  $\mathcal{N}(0, \sigma^2)$ ,  
total noise energy  $N_r$

- Define orthonormal transformations

$$\mathbf{A} = [\mathbf{d}(\varphi_r) : \mathbf{D}_\perp]$$

$$\mathbf{B} = [\tilde{\mathbf{s}}(\varphi_t) : \mathbf{S}_\perp]$$

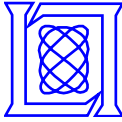
- After transformation,

$$\tilde{\mathbf{Y}} = \begin{bmatrix} \hat{a} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{bmatrix} + \tilde{\mathbf{N}}$$

Each element of  $\tilde{\mathbf{N}}$ ,  $\mathcal{N}(0, \sigma^2)$

- Signal appears in upper left corner with total signal energy  $E_r$

**No different for SIMO or MIMO:  
SNR is equal**



# Outline

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- Introduction
- Coherent MIMO Surveillance Radar Range Equation
- ➔ • Comparison and Assumptions
- Conclusion



# Target and Environment Assumptions

---

- **Target and environment must be constant for significantly longer time period**

$$\left| E[\sigma(t)\sigma^*(t+\tau)] \right| = \sigma^2 \forall t, t+\tau \in (0, T)$$

- **Single beam dwell area**

$$\text{Antenna Gain} = 4 \pi A_{t\lambda} \quad A_{t\lambda}: \text{area in wavelengths}$$

- **Dwell time increased by the number of beam positions to scan region:**

$$k = \text{Number of beams} = \Omega / 4 \pi A_{t\lambda}$$

- **It is difficult to meet coherence assumption in many applications**
  - **Alternative processing approaches likely can mitigate this**
- **Dwell time is often determined by required Doppler resolution rather than SNR**



# Waveform Assumptions

---

- **Compact Uniform Spatial Spectrum**

- Energy in region of interest is

$$\max_{\Omega} \int |S(k)|^2 dk$$

- Or conversely,

$$\min_{k \notin \Omega} \int |S(k)|^2 dk$$

- **Uniformity of illumination criteria is:**

$$\min \max_{\Omega} (\text{ave}(|S(k)|^2) - |S(k)|^2)$$

- **SIMO radar precisely generates and scans a single beam**
- **MIMO attempts to “uniformly” illuminate a larger area**

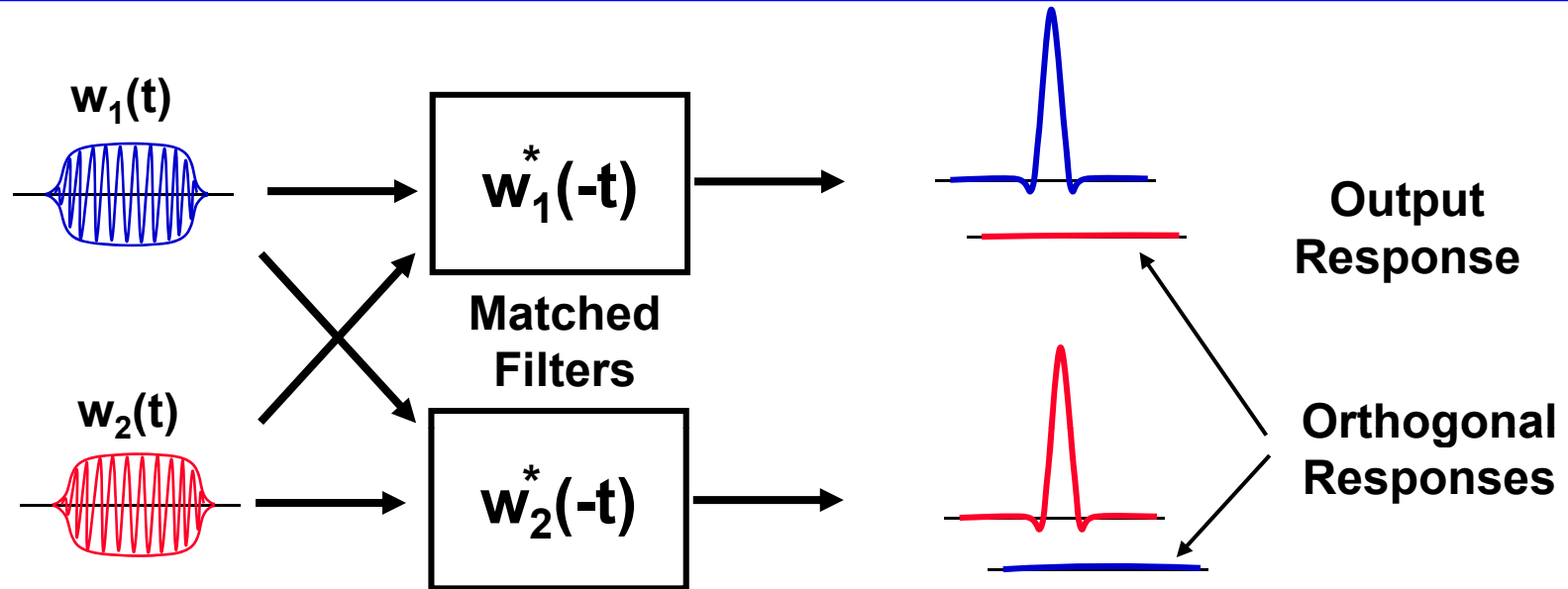
- **Waveform Spectral Response**

- **Waveforms are not disjoint frequency for coherent operation**
- **MIMO observability lost if disjoint**
- **SIMO has no such restriction**





# Orthogonal Waveforms



- **Orthogonal waveforms are the key enabler to MIMO**
  - Limit mutual interference
  - Enable cooperative operation
  - Provide visibility into paths between transmitter and receivers
- **Three methods of achieving orthogonality**
  - Time division, frequency division, code division
  - Orthogonality achievable determined by time-bandwidth product



# Waveform Assumptions (2)

## Correlation Properties

---

- **Autocorrelation function**
  - Autocorrelation function critical for both MIMO and SIMO

$$\begin{aligned}\chi(\tau, f) &= \int_{-\infty}^{\infty} w_m(t) w_m^*(t - \tau) e^{-j2\pi ft} dt \\ &= \delta(\tau) \cdot \delta(f)\end{aligned}$$

- **Cross correlation**

$$\int_{-\infty}^{\infty} w_A(t) w_B^*(t + \tau) d\tau = 0 \quad \forall t, A \neq B$$

- **Waveform packing of Abramovich and Fraser**
  - Constraint on clear area of waveform ambiguity function
  - MIMO more difficult by factor of M for the same time-bandwidth
  - But time-bandwidth is likely higher by factor of M



# Additional Waveform Assumptions

- **Constant amplitude at array face**

$$|s(t)| = c \quad \forall t$$

- Required for efficient power amplifier performance
- Not met with linear transformation in generic MIMO model
- Can be met in straightforward manner with SIMO

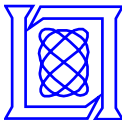
- **Frequency spectrum to meet NTIA requirements**

- Maximize in-band energy

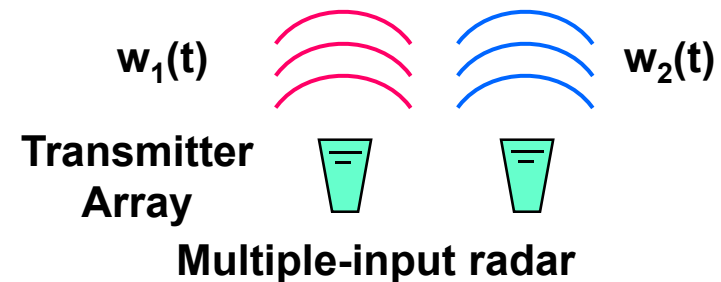
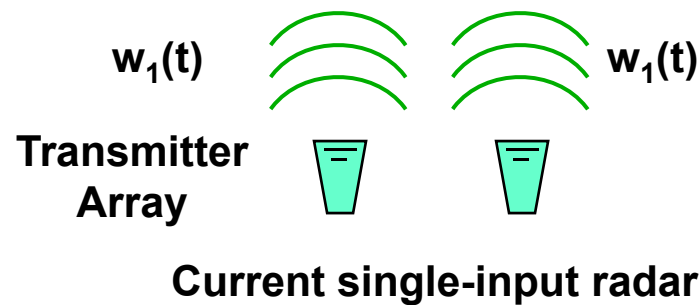
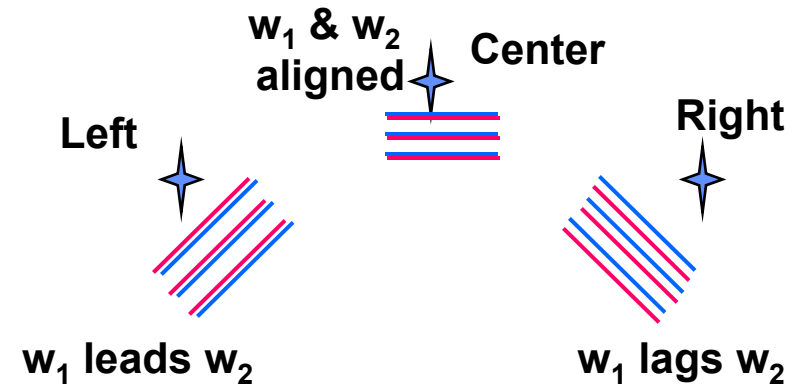
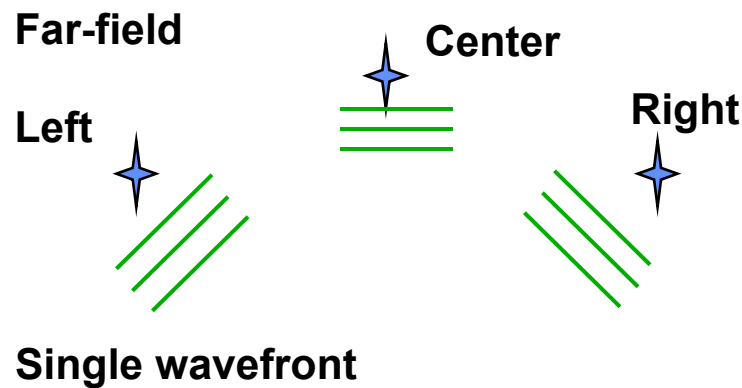
$$\max_{f_L} \frac{\int_{f_L}^{f_H} |S(\omega)|^2 d\omega}{\int_0^{\infty} |S(\omega)|^2 d\omega}$$

- And minimize the maximum out-of-band spectral sidelobes

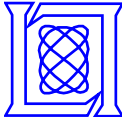
$$\min \max_{\omega < f_L, \omega > f_H} (|S(\omega)|^2)$$



# MIMO Radar Observability



- Rank of illumination waveform must be  $>1$  for observability
  - Does not have to be element-space waveforms
- Observability determined by transmit array/waveform manifold curvature



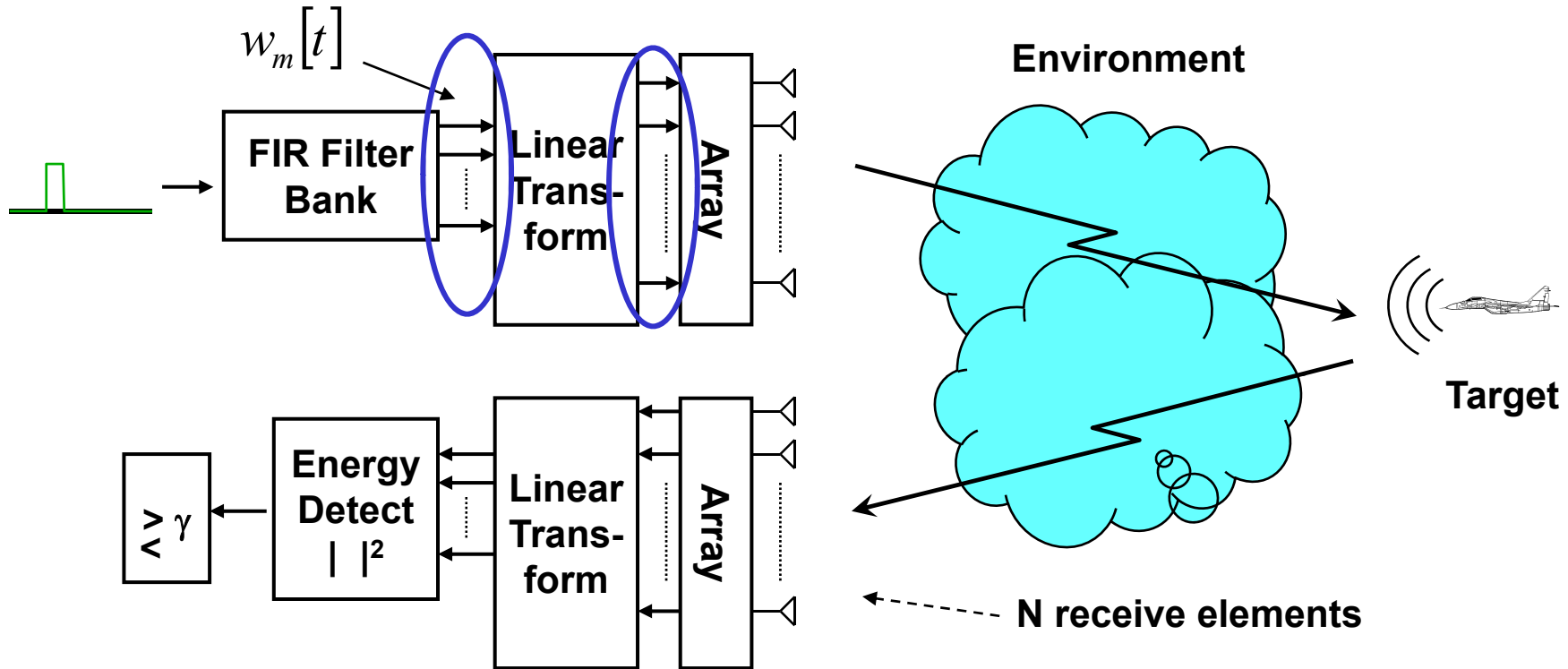
# Maximizing MIMO Radar Observability

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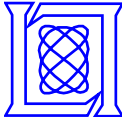
- **Small waveform rank is required to meet correlation limits**
- **Array/waveforms will interact to determine needed rank**
- **Array manifold arc-length and curvature will determine resolution and observability**
- **Equations need to be developed**
- **This is a work in progress**
  - **Cramer-Rao bounds for receive-only arrays apply directly for the virtual array or sum co-array**
  - **This should not be the same as maximizing observability**
  - **This should not be the same as maximizing ultimate SNR**



# Waveform Assumptions



- **Waveform assumptions were located at two points**
- **A linear transform model is correct given previous work**
- **Optimizing directly at the array face would appear productive**



# Waveform Assumption Summary

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- **General for MIMO or SIMO**
  - Autocorrelation
  - Low out-of-band energy to meet NTIA requirements
  - Efficient (spectral shaping in-band)
  - Constant modulus
- **MIMO specific assumptions**
  - Compact uniform spatial spectrum (corresponds to low VSWR)
  - Provides MIMO observability (curvature of array manifold)
  - Cross-correlation
- **Other practical assumptions**
  - Resistant to small transmitter non-linearities
  - Ease in processing
  - Exploitation



# Summary

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- **Coherent MIMO radar range equation developed**
- **MIMO and SIMO have equivalent SNR, but with significant assumptions**
- **All assumptions are unlikely to be met for MIMO radar**
- **The most difficult assumptions to meet are related to target characteristics and waveforms**