

Identifying and Eliminating Single Points of Failure

Presented by: Thomas King

Course Objectives

- Identifying and Eliminating Single Points of Failure
 - **Training**
 1. Appropriate use of equipment
 2. Fire Prevention
 3. Appropriate use of PPE
 - **Maintenance and Upgrades**
 1. Thermal Scans
 2. Cutting Edge Circuit Breaker Technology
 3. Diesel Fuel and Battery Maintenance
 - **Design**
 1. Sequence of Operation of mechanical and electrical controls
 2. Redundancy of power paths and mechanical and electrical equipment
 3. Transient Voltage Mitigation
 4. Generator loading and paralleling

Training



Emergency Power Off (EPO)

- The “Emergency Power Off” (EPO) button is infamous in the history of IT centers as people sometimes mistake it for a door release button
- The NEC has allowed the EPO to be remotely located (not physically in the IT room) since 2011.
- Legacy installations remain. It is important to be able to tell the difference between the EPO and the Door Release button

Emergency Power Off (EPO)



Fire

- NFPA 75 was created in response to a fire in 1959 which started when magnetic tape was stored too close to an incandescent lamp in a Pentagon Data Center
- NFPA 75 includes requirements for fire alarming and fire protection and includes design requirements for both water and gas based fire suppression

Fire

Pentagon Fire Destroys Air Records and Computers



Associated Press Wirephoto

Firemen pour water through hole cut in floor of Pentagon's main concourse on fire below

Turning the Wrong Handle

- Critical Facilities are filled with buttons and handles. Turning the wrong one can lead to an outage

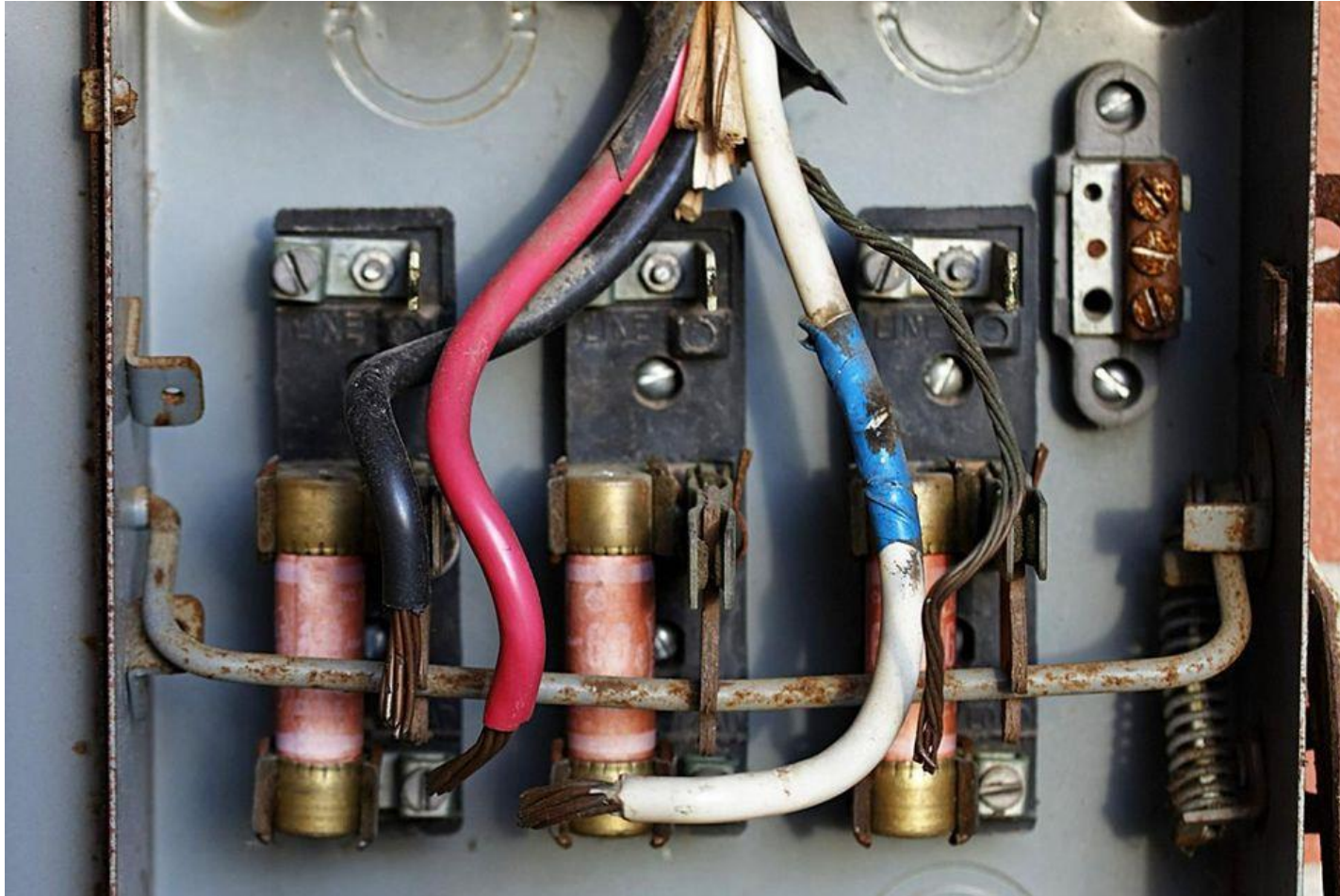
Turning the Wrong Handle



Taking Short-Cuts

- It is essential to develop and follow detailed Method Of Procedures (MOPs). Taking short-cuts or using obsolete MOPs could lead to an outage

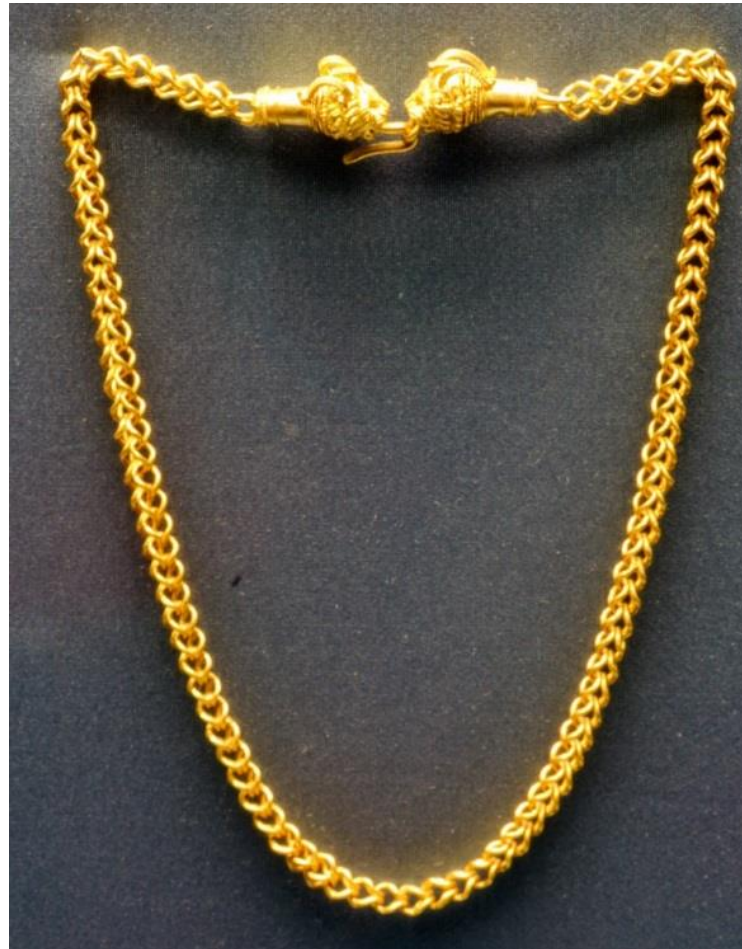
People Taking Short-Cuts



Jewelry

- OSHA 1910.333(c)(8) prohibits the wearing of conductive material where it might come into contact with energized parts

Jewelry



Not Paying Attention

- Situational awareness is mandatory. Leaning on a switchboard or carrying large objects without help could lead to an outage

Not Paying Attention



Driving Poorly

- Car accidents can result in catastrophic damage to utility distribution equipment

Driving Poorly



Maintenance



Upgrade Old Equipment

- In 1947, The fastest computer in the world had an up-time of 2 hours a week
- By 1954, this same computer had managed to operate without failure for 116 hours—close to five days
- Solid State equipment has greatly improved the mean time between failure (MTTBF) of IT equipment

Upgrade Old Equipment

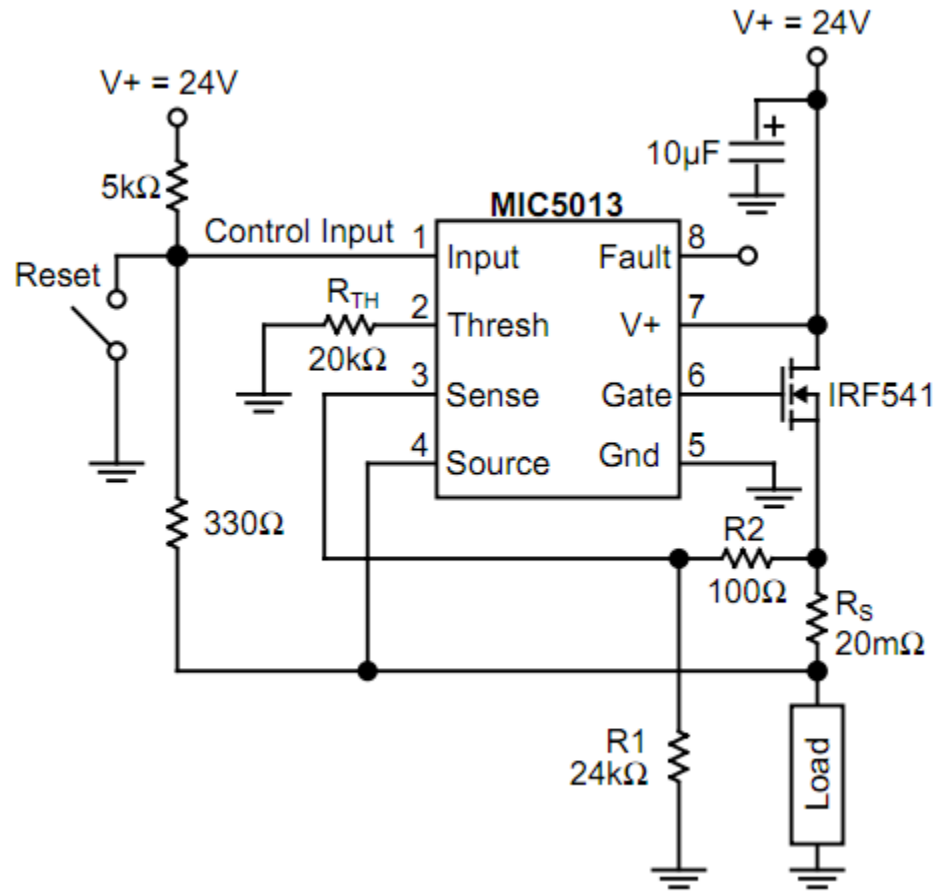


Source: U.S. Army photo

Upgrade Circuit Breakers

- Electronic Trip circuit breakers may provide better selectivity than thermal magnetic circuit breakers
- Solid State circuit breakers provide nearly instantaneous circuit interruption - ensuring selectivity and making Arc Flash a thing of the past

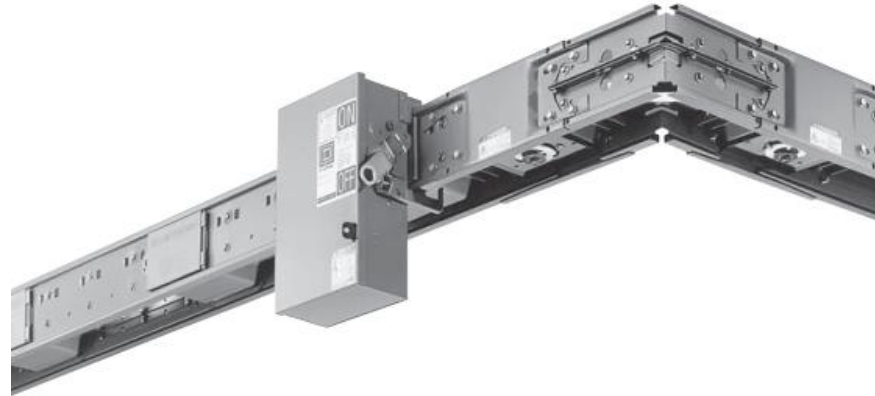
Upgrade Circuit Breakers



Torque

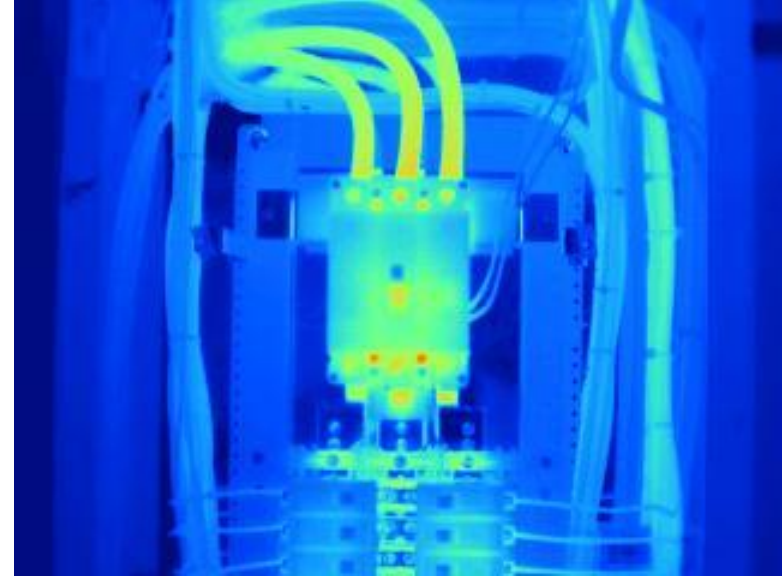
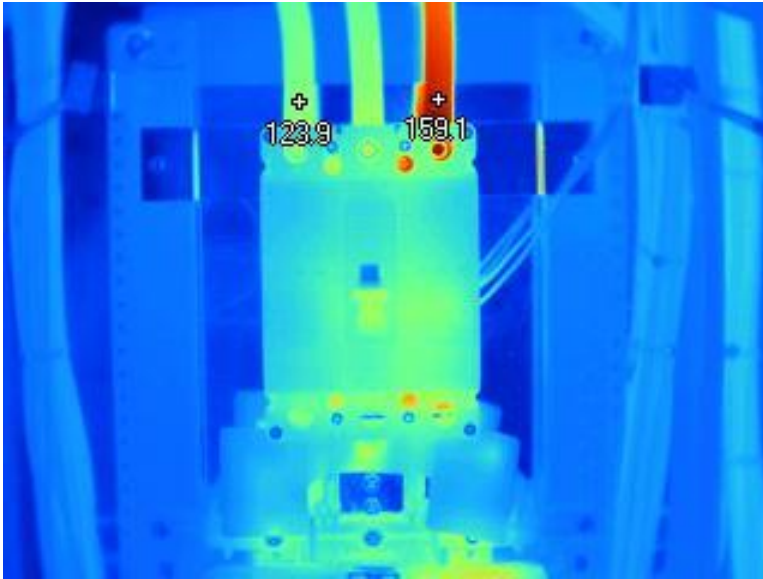
- Infrared cameras allow us to see heat
- Infrared scanning of electrical busway and circuit breaker lugs may indicate hot spots before they become a point of failure

Torque



Source: <http://www.fssb.my/buswaymaintenance.html>

Torque

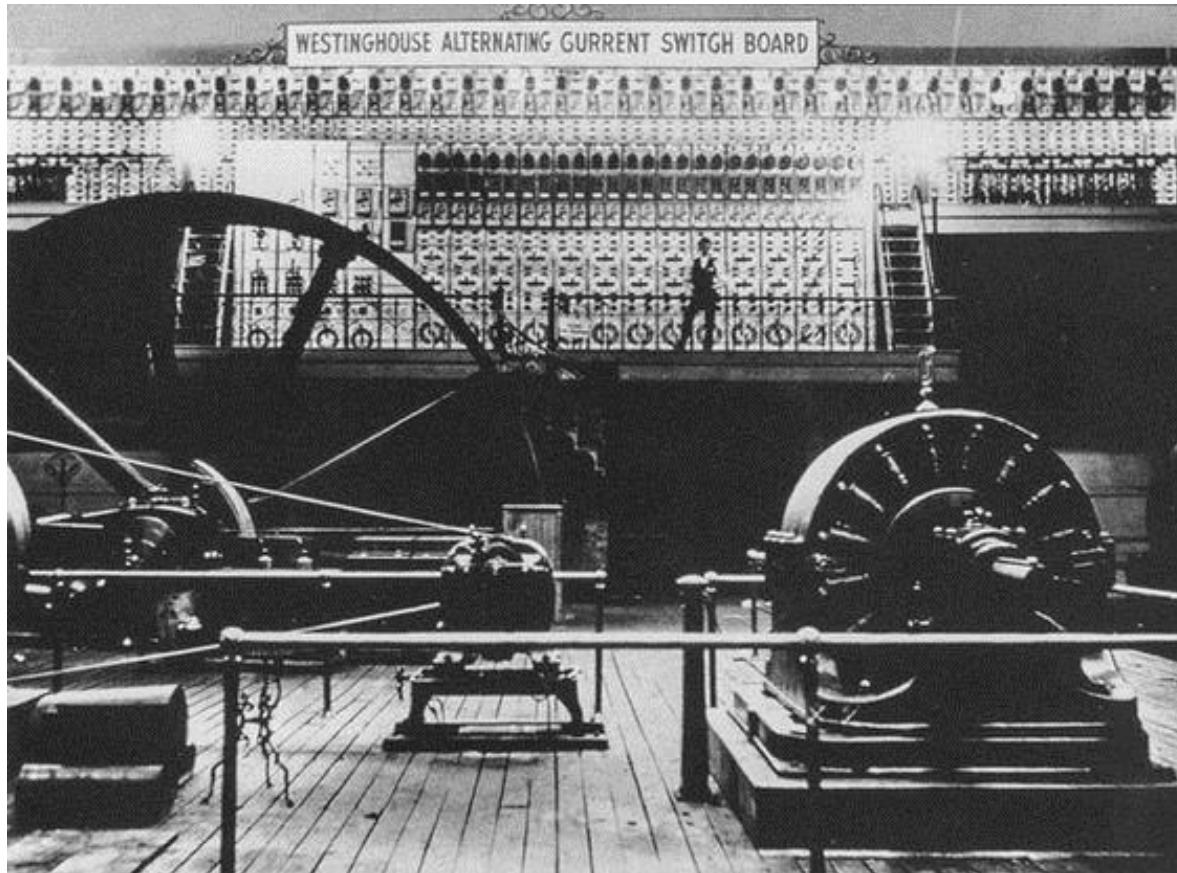


Source: <http://www.circuitbreakersblog.com>

Replace Existing Equipment

- Some equipment cannot be upgraded and must be replaced in order to improve reliability
- Electrical AC power distribution first gained popularity for lighting in the 1893 world's fair and has improved in the last 123 years

Replace



Source: <https://teslauniverse.com>

Maintain Existing Equipment

- Regular Maintenance of critical mechanical and electrical systems can prevent outages
- Chemical energy storage such as batteries and diesel fuel requires special regular attention

Maintain Existing Equipment

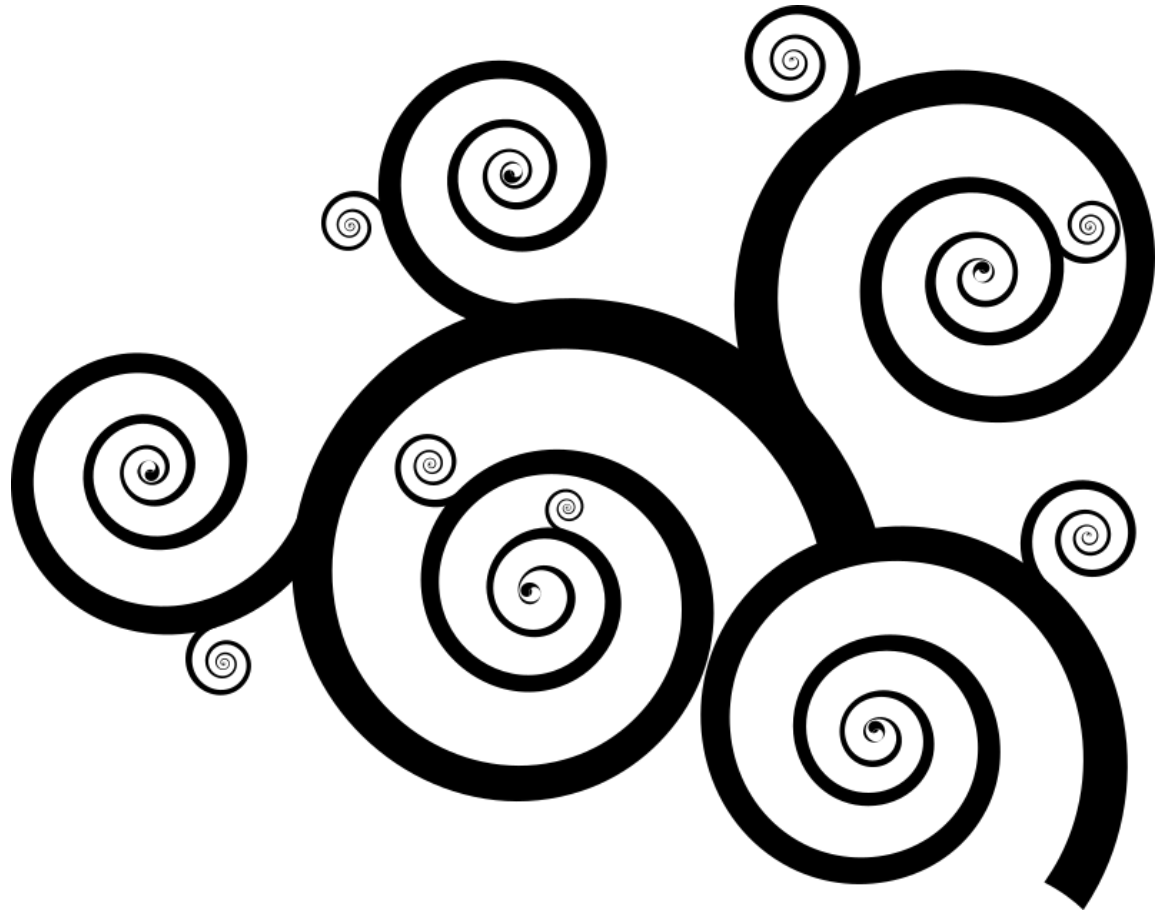


Source: <http://www.eepowersolutions.com>



Source: CNBC.com

Design



DCIM/BAS Redundancy

- Consider providing a dedicated BAS for each chiller and its associated pumps and cooling tower
- It may be best if only one controller is required for each chiller system since controller-to-controller communications may degrade redundancy
- Redundant differential pressure sensors are recommended where multiple chillers feed a common loop
- Redundant common control sequences in each controller is recommended for the chilled water pump VFD/pressure controls

DCIM/BAS Redundancy

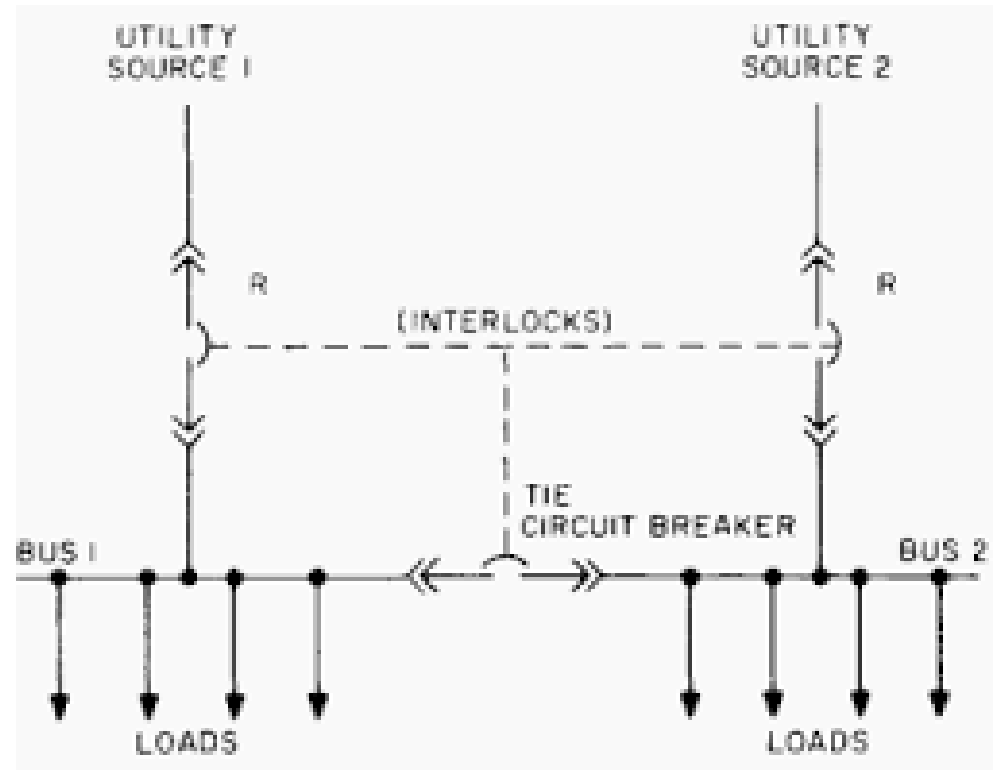
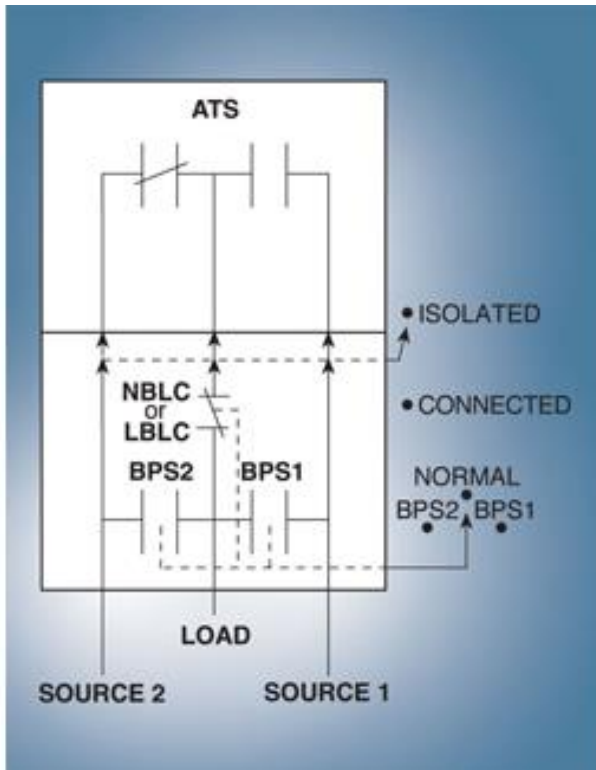


Source: <http://berg-group.com>

Sequence of Operation

- Where there are multiple sources of power, ensure coordination of ground fault delays to prevent the non-energized source from nuisance tripping
- In Emergency Backup systems, ensure that any engine start delay does not put you outside of the 10 second emergency range
- Coordinate ATS delays with the following considerations in mind:
 - Emergency loads must be stable before standby loads are added
 - All generators must be paralleled and on the bus before adding standby loads

Sequence of Operation

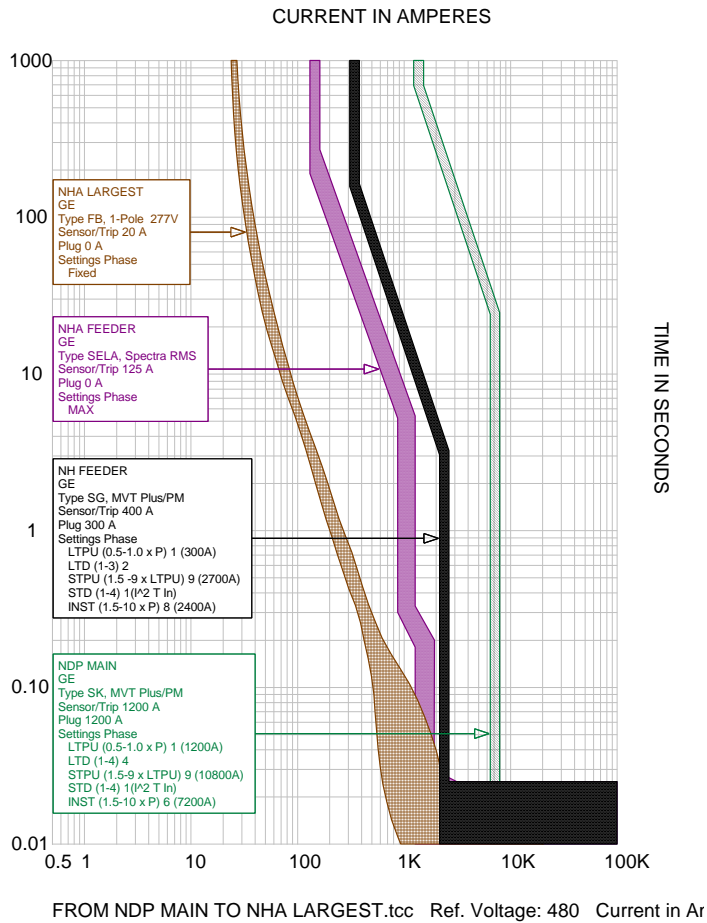


Source: <http://www.russelectric.com>

Protective Device Settings

- Selective coordination of all protective devices is required in fault tolerant systems
- ATS switching delays need to be coordinated with motor lock-out relays to prevent chillers and other motors from locking out due to multiple transfer operations

Protective Device Settings



Source: <http://www.icmcontrols.com>

Power Quality Tolerances

- The ATS Sync-Check relay (ANSI device 25) needs to be set with special consideration to both surge current and the practical limitations of the system
- New IT power supplies have improved “ride-through” capabilities as compared to first generation equipment
- Reverse power relays (32R) may be required to prevent back-feeding the utility transformers. Utility network protectors will open on reverse power but do not have sync check capability. If out of sync power is applied to a utility network protector, it may fail catastrophically, leading to a indeterminate power outage.

Power Quality Tolerances

Calculate Out of Phase Voltage and Surge Current

$$\Delta := 10^\circ$$

$$Motor_{kva} := 3660$$

$$V_{diff.pu} := 2 \cdot \sin\left(\frac{\Delta}{(2)}\right)$$

$$V_{diff.pu} = 0.174$$

$$V_{diff} := V_{diff.pu} \cdot 480 \text{ V}$$

$$V_{diff} = 83.67 \text{ V}$$

$$X_{d''} := .144$$

$$I_{surge.pu} := \frac{V_{diff.pu}}{X_{d''}}$$

+

$$I_{surge.pu} = 1.21$$

$$I_{amps} := I_{surge.pu} \cdot \frac{Motor_{kva}}{(\sqrt{(3)} \cdot 480)} \cdot 1000$$

$$I_{amps} = 5.329 \cdot 10^3$$


Source: “Managing risks, benefits with closed transition transfer switches”
Cummins Power Generation

Power Quality Tolerances


'Dirty Power' Fells Computers

Power Disturbances That Can Play Havoc With Computers

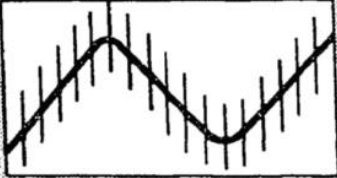
Diagrams depict the waveforms of electric current and how they are affected by some common disturbances



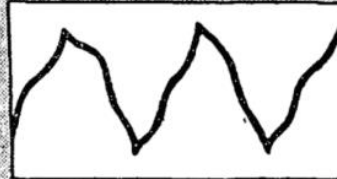
Voltage Dip: A momentary, sometimes barely discernible drop in voltage that can be caused by a short circuit or power outage somewhere in the utility system.



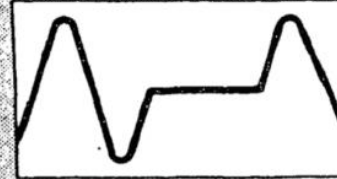
Power Line Noise: Static interference caused by lightning, motors, or welders that is fed back into the system because there is no isolating transformer.



Voltage Flicker: Distorted electric current waveforms that are caused by unstable current flow. These distortions can be monitored and corrected.



Brown Out: A deliberate reduction in voltage that is engineered by the electric utility company.

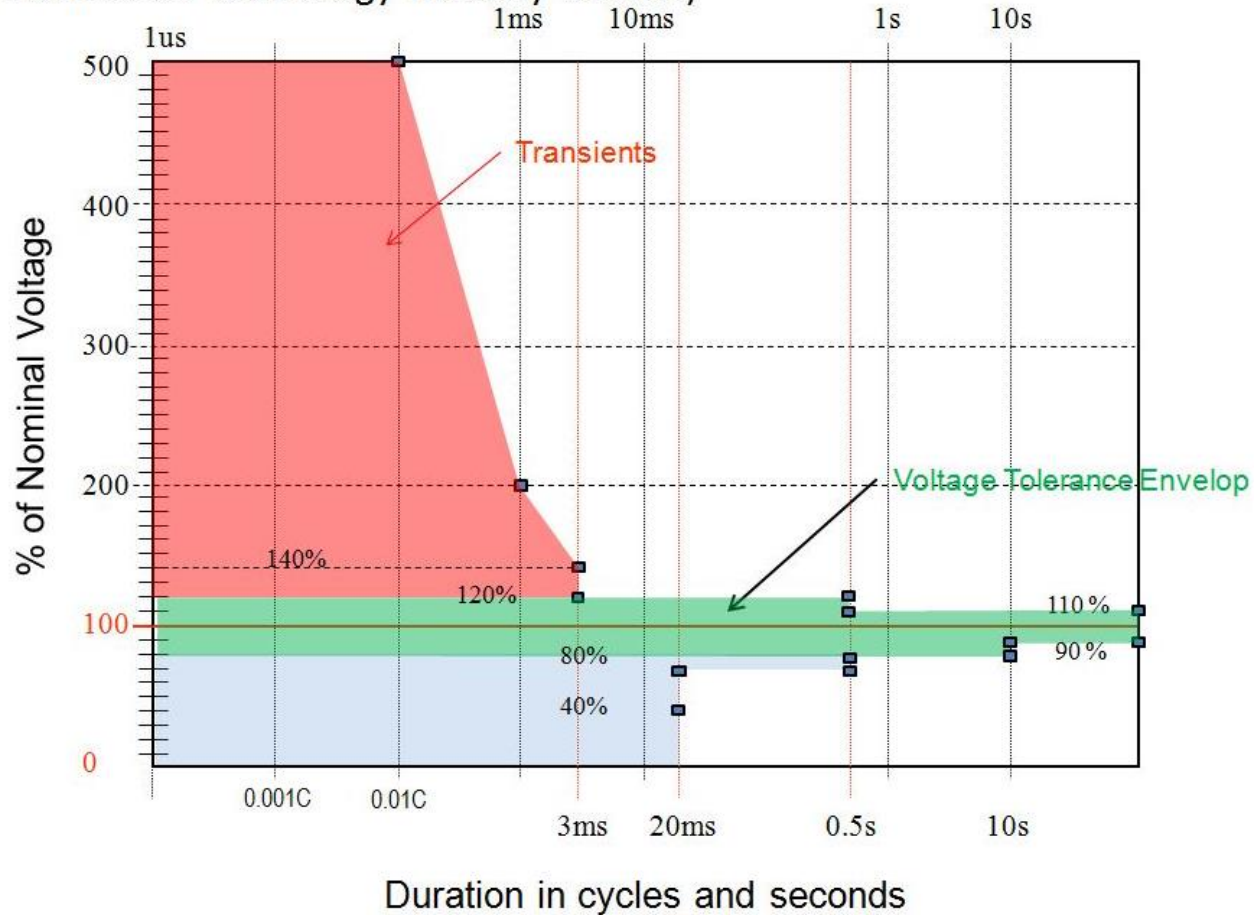


Source: Creative Strategies International

Source: The New York Times, April 17, 1982

Power Quality Tolerances

(Information Technology Industry Council)



Source: Information Technology Industry Council (ITI)

Power Quality Tolerance

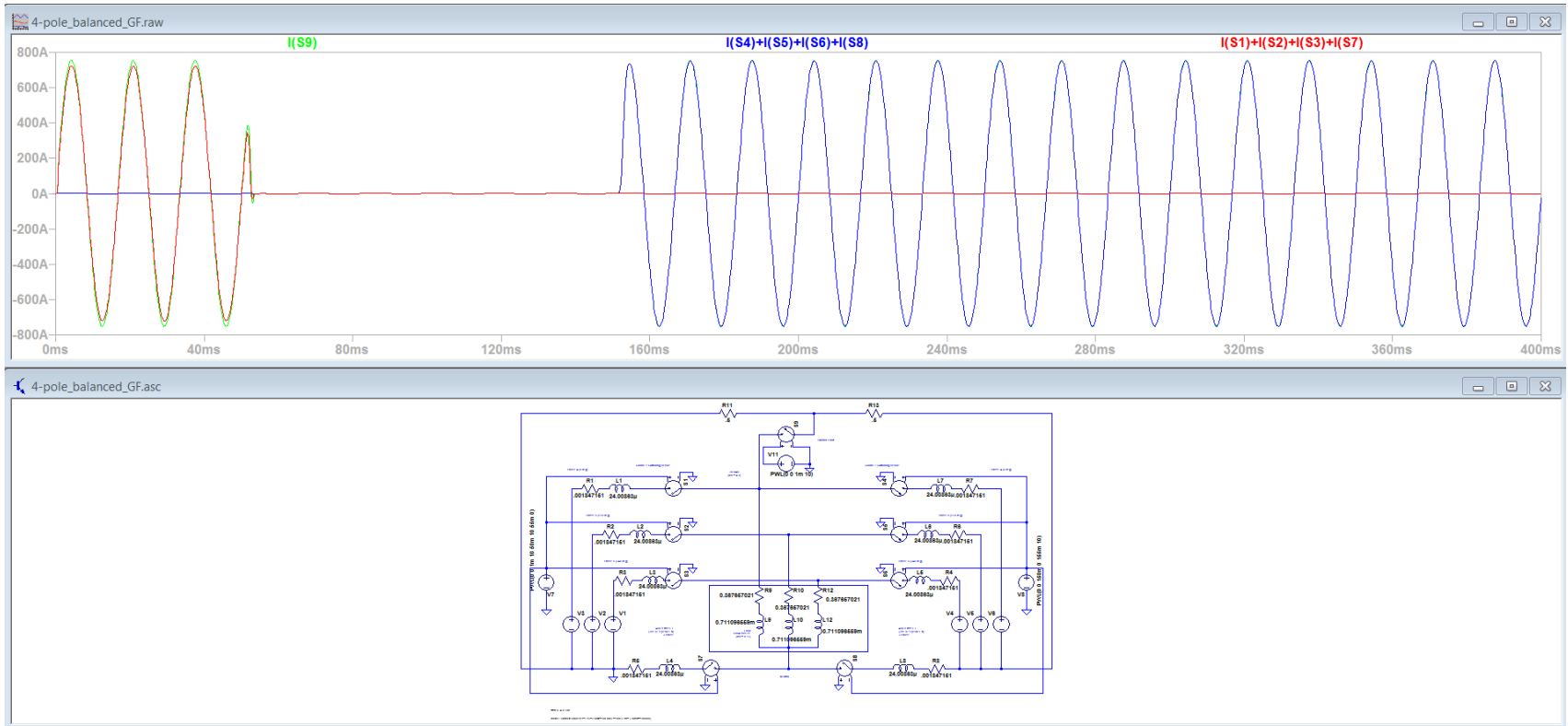


NETWORK
PROTECTOR

4-Pole Open Transition ATS

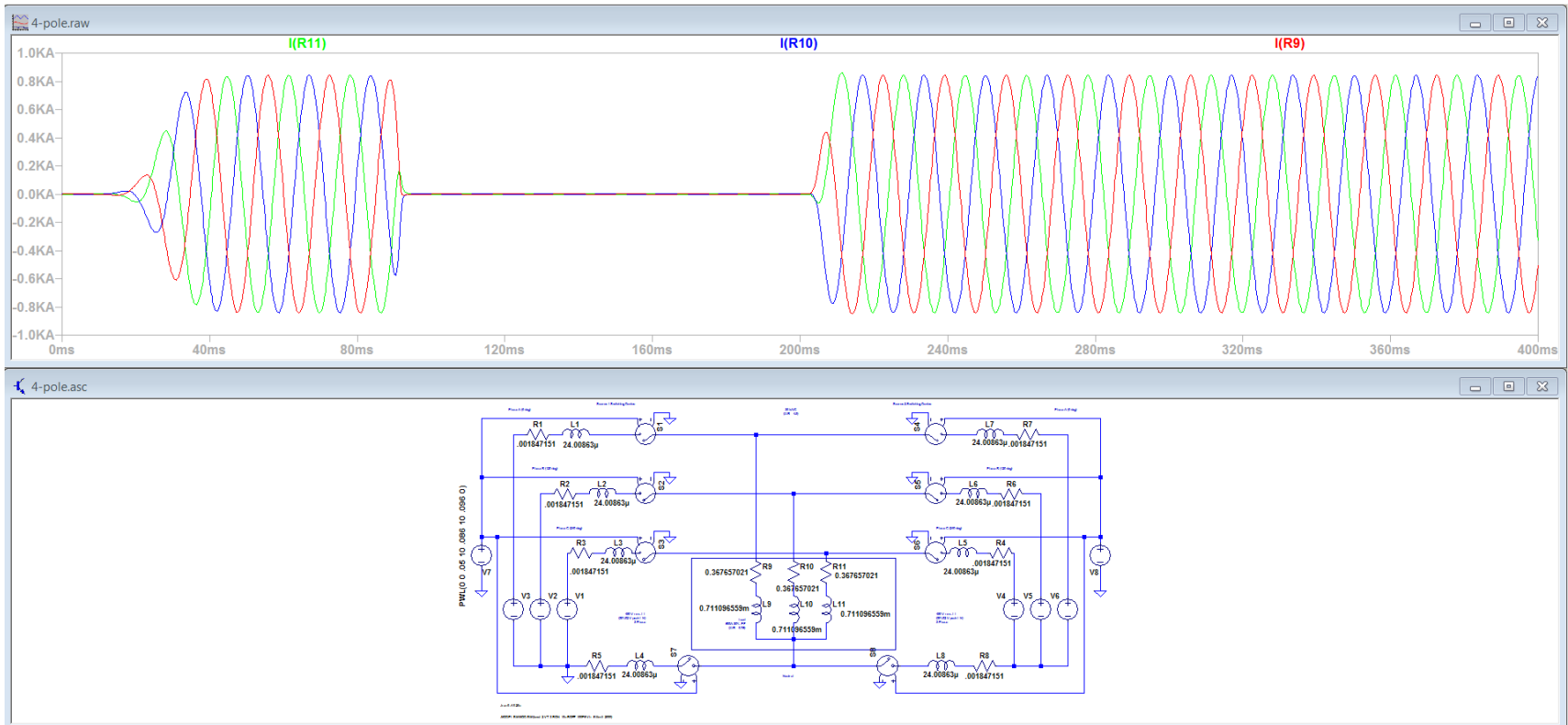
- The 4-Pole Open Transition ATS prevents the flow of ground fault current back to the de-energized source
- The 4-Pole Open Transition ATS can be specified to include a “delayed off” position to allow the motor contribution to decay
- The 4-Pole Open Transition ATS may experience a transient rise in voltage across the neutral contact if an unbalanced load is being switched

4-Pole Open Transition ATS



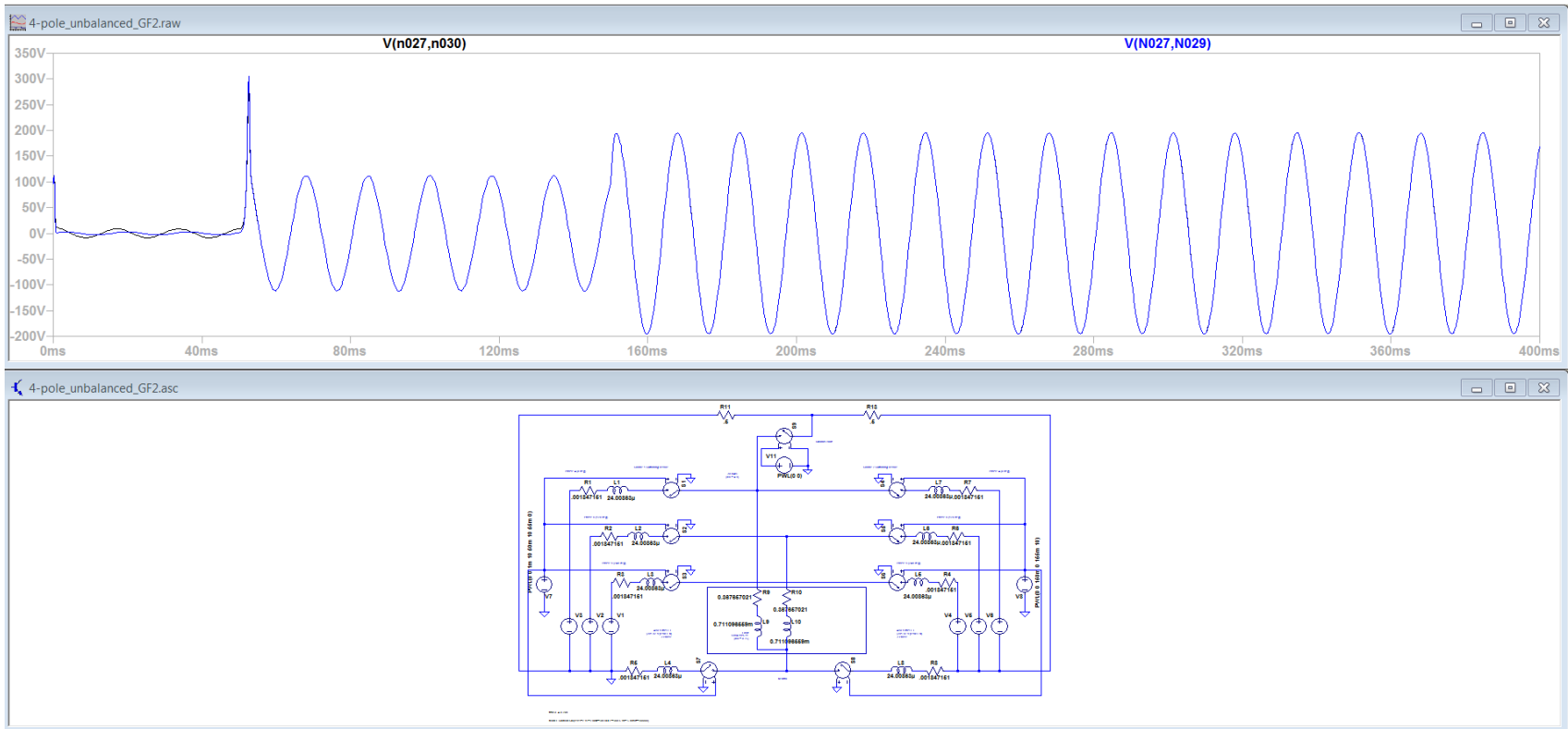
Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

4-Pole Open Transition ATS



Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

4-Pole Open Transition ATS

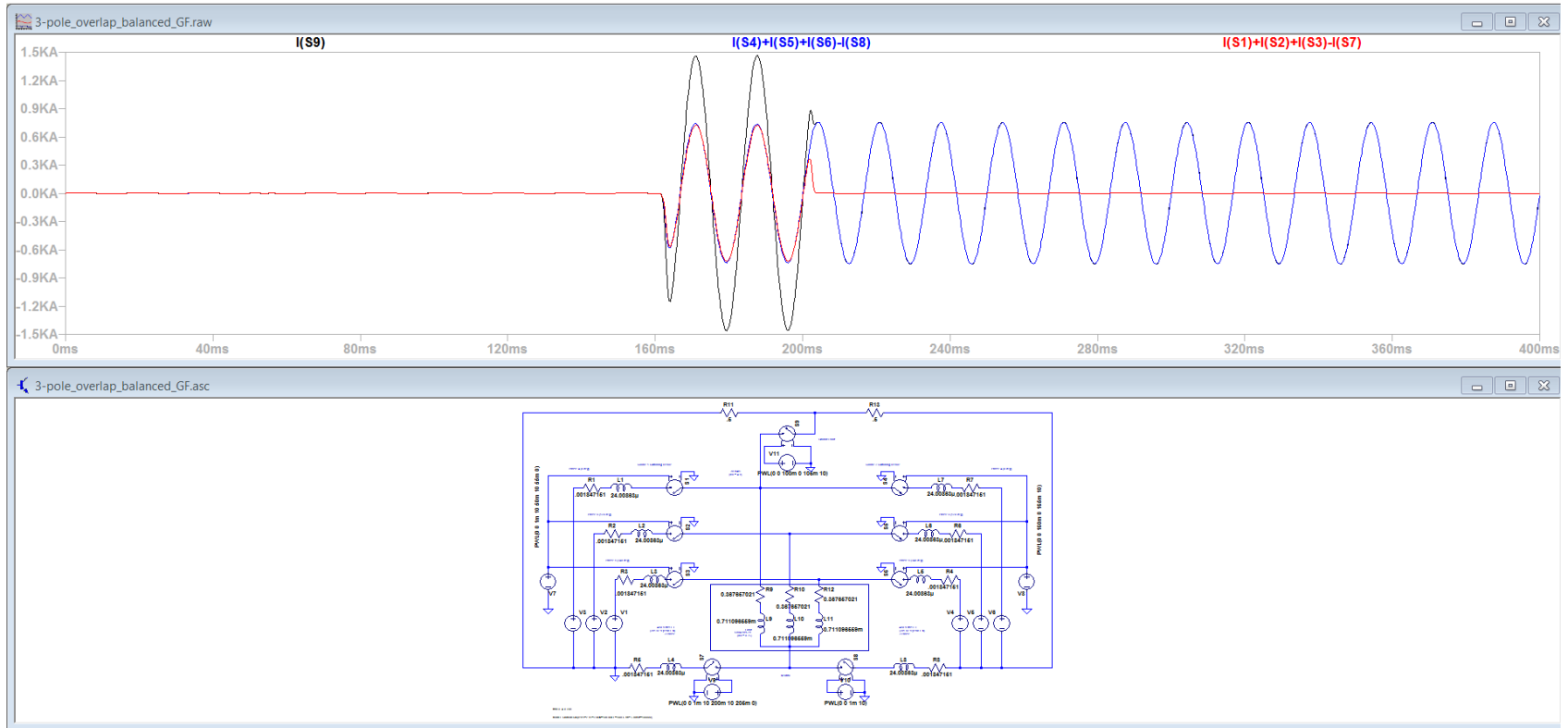


Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

Overlapping Neutral 4-Pole ATS

- The Overlapping Neutral 4-Pole ATS allows ground fault current to flow back to the de-energized source – potentially resulting in a nuisance trip
- The Overlapping Neutral 4-Pole ATS maintains a solid neutral during the switching operation – similar to the 3-pole ATS
- The Overlapping Neutral 4-Pole ATS does not experience a rise in potential across its neutral contact during a switching operation

Overlapping Neutral 4-Pole ATS

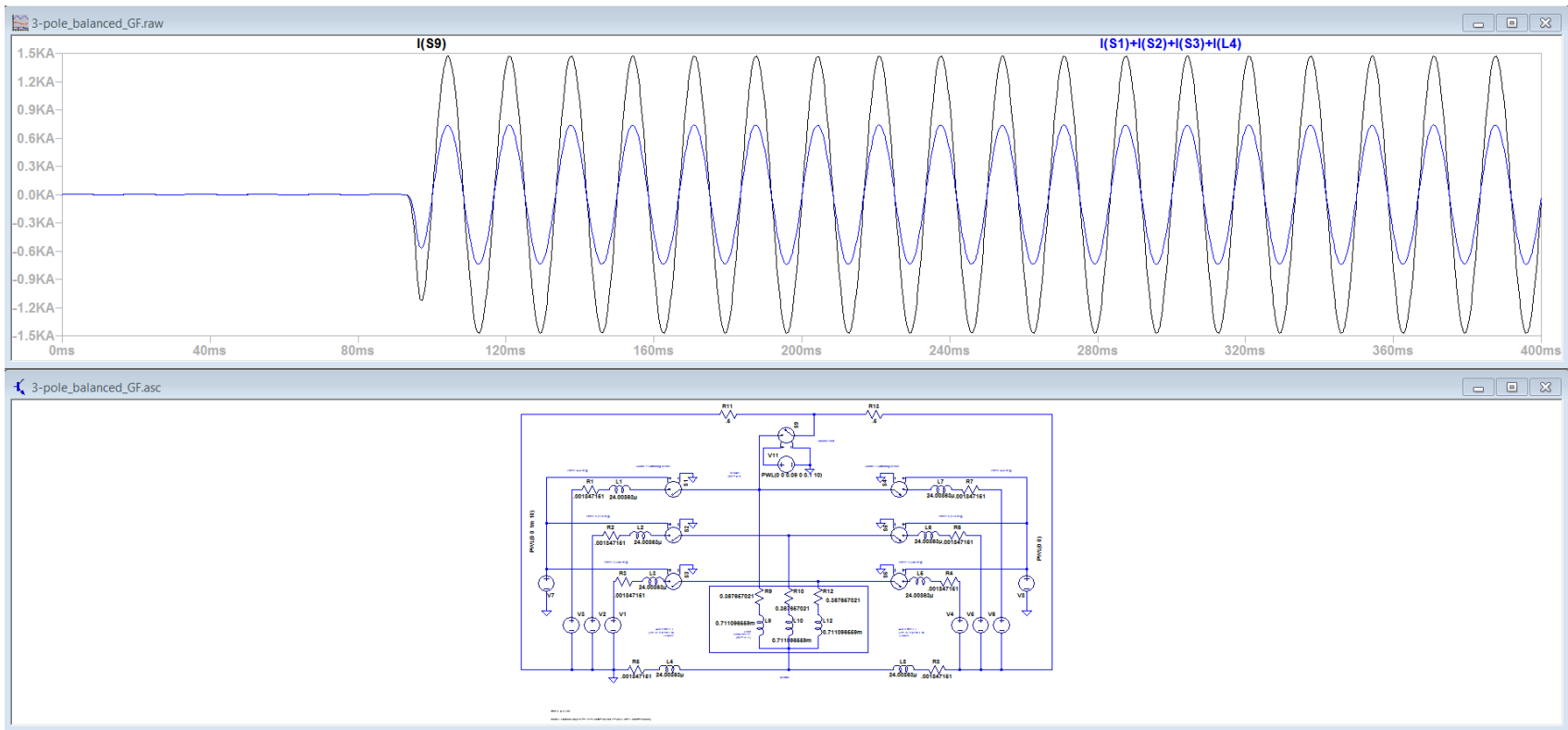


Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

3-Pole ATS with Modified Ground Fault Protection

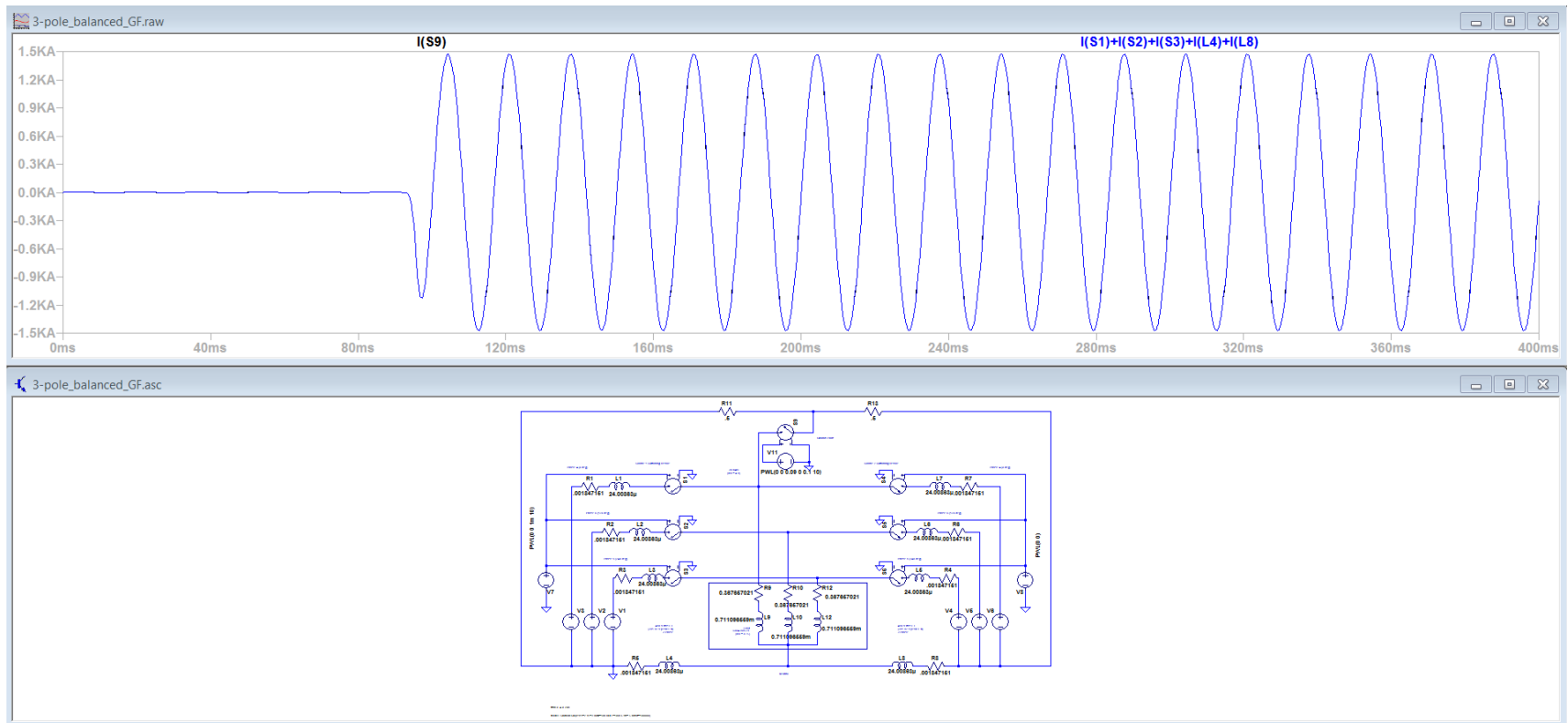
- The 3-Pole ATS allows ground fault current to flow back to the de-energized source. This can cause:
 - A decrease in the magnitude of ground fault current sensed by the energized source's zero sequence CT's
 - An increase in the opening time delay of the energized source protective device
- Adding Modified Differential Ground Fault Protection may prevent a nuisance trip of the de-energized source on a system with a 3-Pole ATS

3-Pole ATS with Modified Ground Fault Protection



Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

3-Pole ATS with Modified Ground Fault Protection



Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

Transient Voltage Mitigation

- Causes of Transient Voltage spikes can include:
 - Lightning Strikes
 - Re-striking voltage caused by disconnecting an inductive load
 - Resonance caused by circuit switching
 - Switch Mode power supplies
- Consider high-end VFDs or installation of dV/dT and sinusoidal filters to reduce transients
- Consider Snubber Circuits and Transient Voltage Surge Suppression to filter out transients

Re-striking Voltage

$$V := 480 \cdot \sqrt{2} = 678.823$$

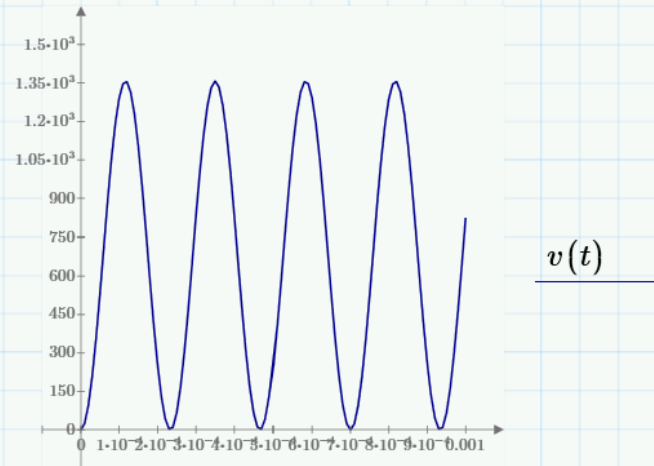
$$XR := 1.77$$

$$C := .00001$$

$$L := .000138$$

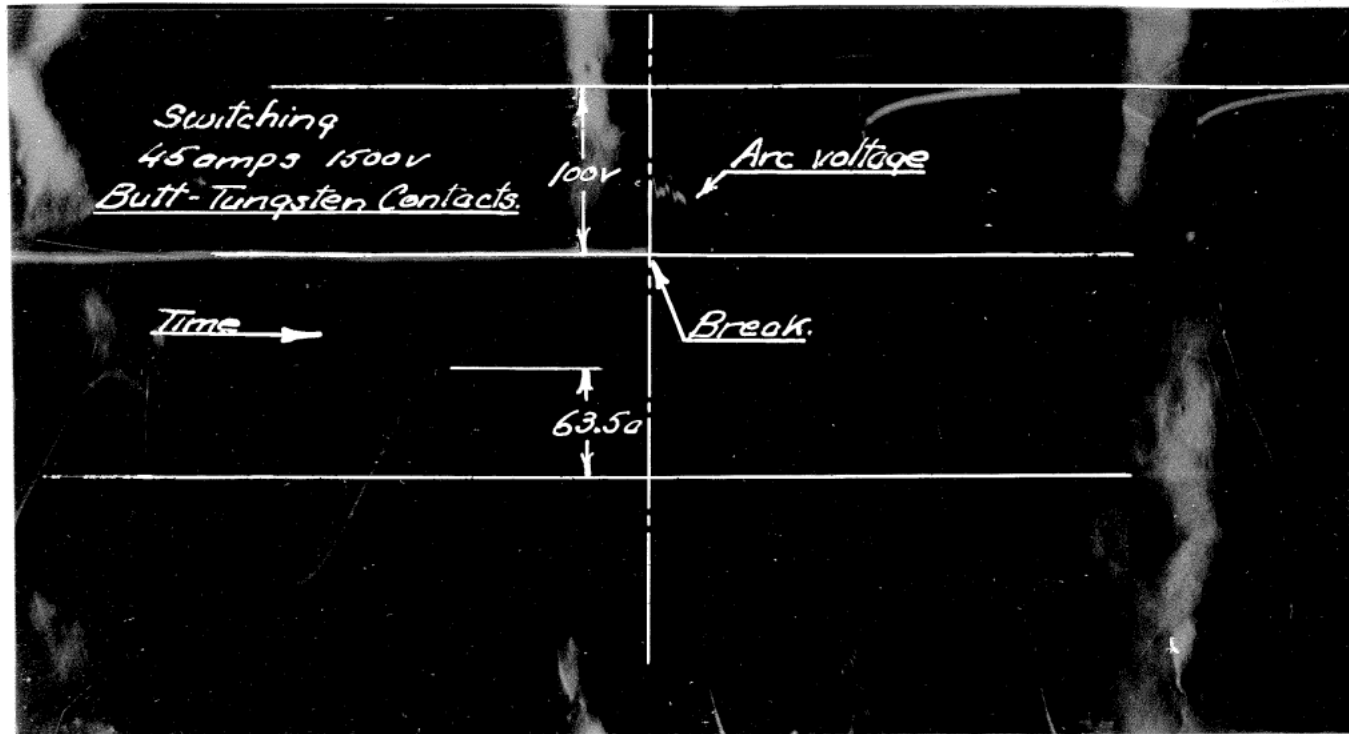
$$v(t) := V \cdot \left(1 - \cos \left(\frac{t}{\sqrt{L \cdot C}} \right) \right)$$

$$t := 0, .00001 \dots .001$$



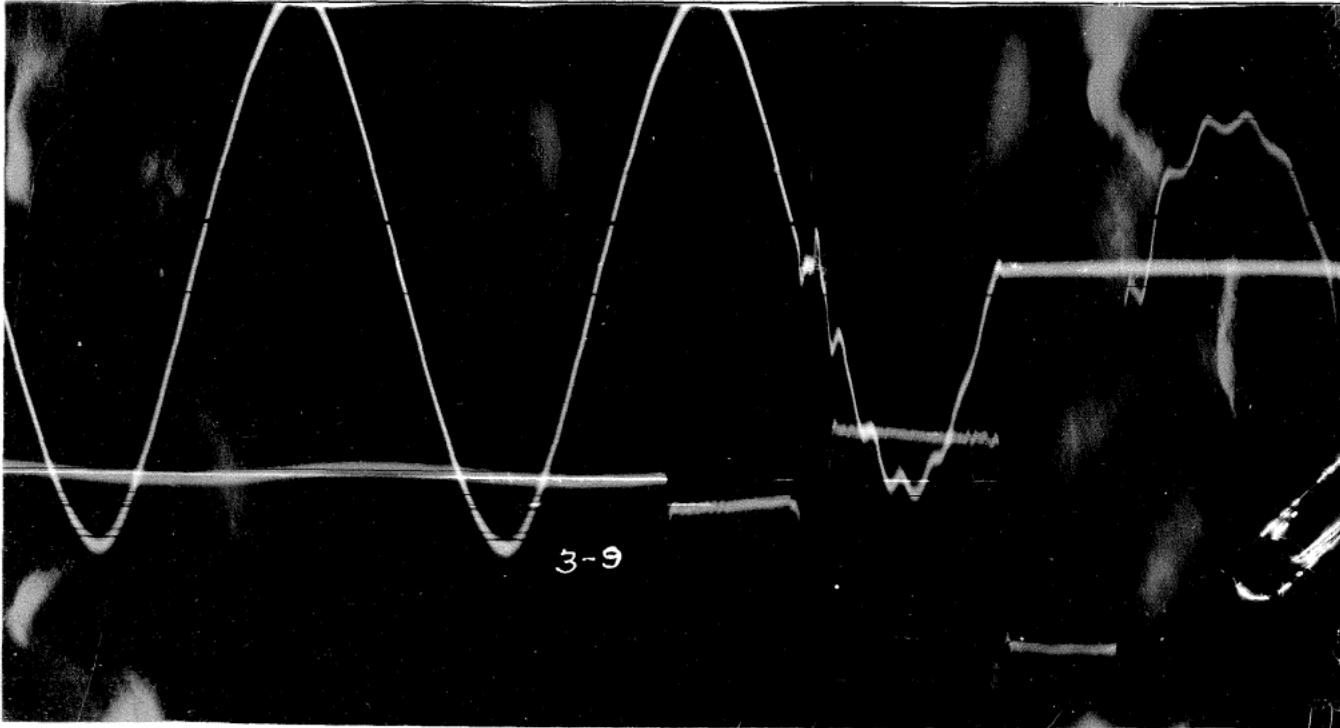
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Re-striking Voltage



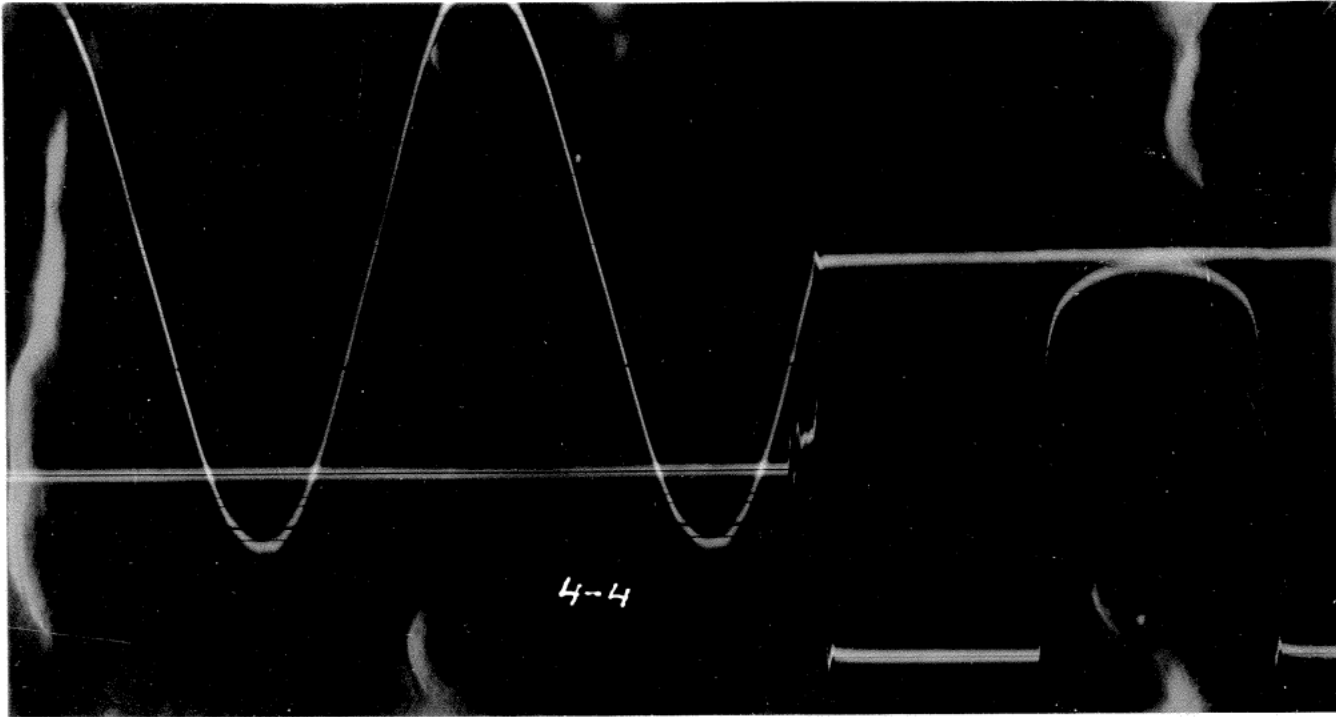
Source: Thesis paper by James Hugh Hamilton
California Institute of Technology 1928

Re-strike Voltage



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Re-strike Voltage



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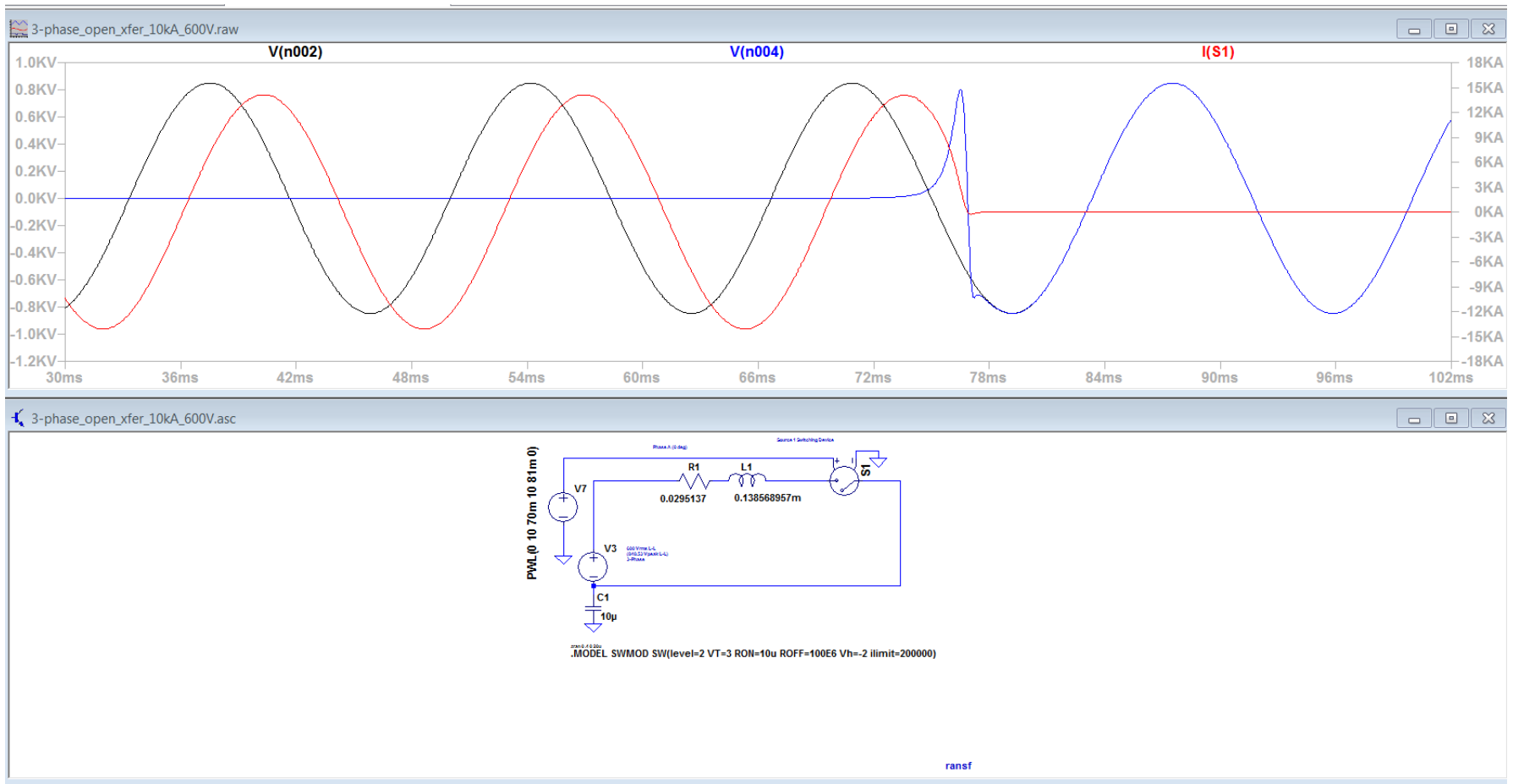
Re-strike Voltage

	<u>Vacuum Switch</u>	<u>Oil Switch</u>
I_{rms}	58.1 amp.	56 amp.
E_{line}	16.2 Kv.	16.2 Kv.
Time	0.008 sec.	0.05 sec.
Energy	7.2	552

$$\text{Ratio of energies} = \frac{552}{7.2} = 77 \text{ to } 1$$

Source: Thesis paper by James Hugh Hamilton
California Institute of Technology 1928

Re-strike Voltage



Source: *3-Pole and 4-Pole Transfer Switch Switching Characteristics*, Eaton.com

Snubber Circuit

- Snubber Circuits can absorb harmful waveforms
- Combined with a surge Arrester, snubber circuits can prevent transformers, Circuit Breakers, and PTs from exceeding their dV/dT and BIL limits

Snubber Circuit



Source: <http://www.electricenergyonline.com/>

Snubber Circuit

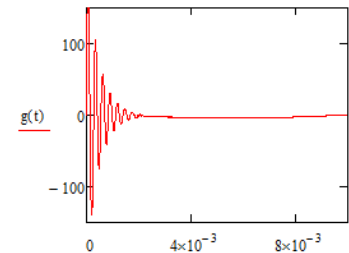
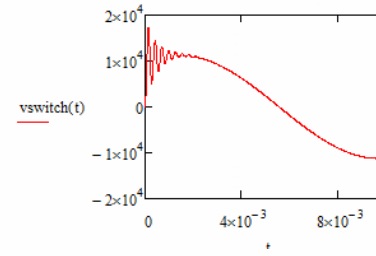
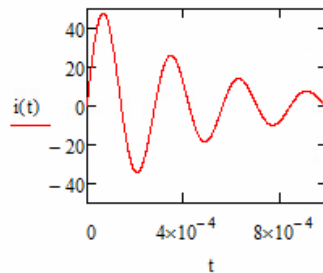
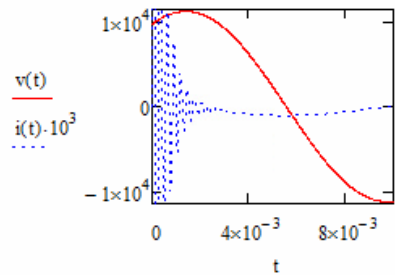
$$V_p := \frac{13800}{\sqrt{3}} \cdot \sqrt{2} = 1.127 \times 10^4 \quad \omega := 377 \quad I_{load} := 4000 \quad \theta := 4 \cdot \frac{\pi}{12} \quad \theta = 1.047 \quad PF_d := \theta \cdot \frac{180^\circ}{\pi} = 1.047$$

$$Z := \frac{V_p \cdot \sqrt{3}}{\sqrt{2} \cdot I_{load}} = 3.45 \quad R_{load} := Z \cdot \cos(\theta) \quad R_{load} = 1.725 \quad PF := \cos(PF_d) = 0.5 \quad X := Z \cdot \sin(\theta)$$

$$C := 25 \cdot 10^{-6} \quad L := \frac{X}{\omega} \quad L = 7.925 \times 10^{-3} \quad v(t) := V_p \cdot \sin(\omega \cdot t + \theta) \quad R_s := 33 \quad R_{sn} := R_{load} + R_s$$

$$V(s) := v(t) \text{ laplace, } t \rightarrow \frac{1.127 \times 10^4 \cdot (0.866 \cdot s + 188.5)}{s^2 + 1.421 \times 10^5} \quad I(s) := \frac{V(s) \cdot \frac{s}{L}}{s^2 + \frac{R}{L} \cdot s + \frac{1}{L \cdot C}} \quad \sqrt{\frac{1}{L \cdot C} - \left(\frac{R}{2 \cdot L}\right)^2} = 2.236 \times 10^4$$

$$i(t) := I(s) \text{ invlaplace, } s \rightarrow 0.534 \cdot \cos(377 \cdot t) - 0.918 \cdot \sin(377 \cdot t) - 0.534 \cdot \cos(2.236 \times 10^4 \cdot t) \cdot e^{-2.191 \times 10^3 \cdot t} + 55.032 \cdot \sin(2.236 \times 10^4 \cdot t) \cdot e^{-2.191 \times 10^3 \cdot t}$$

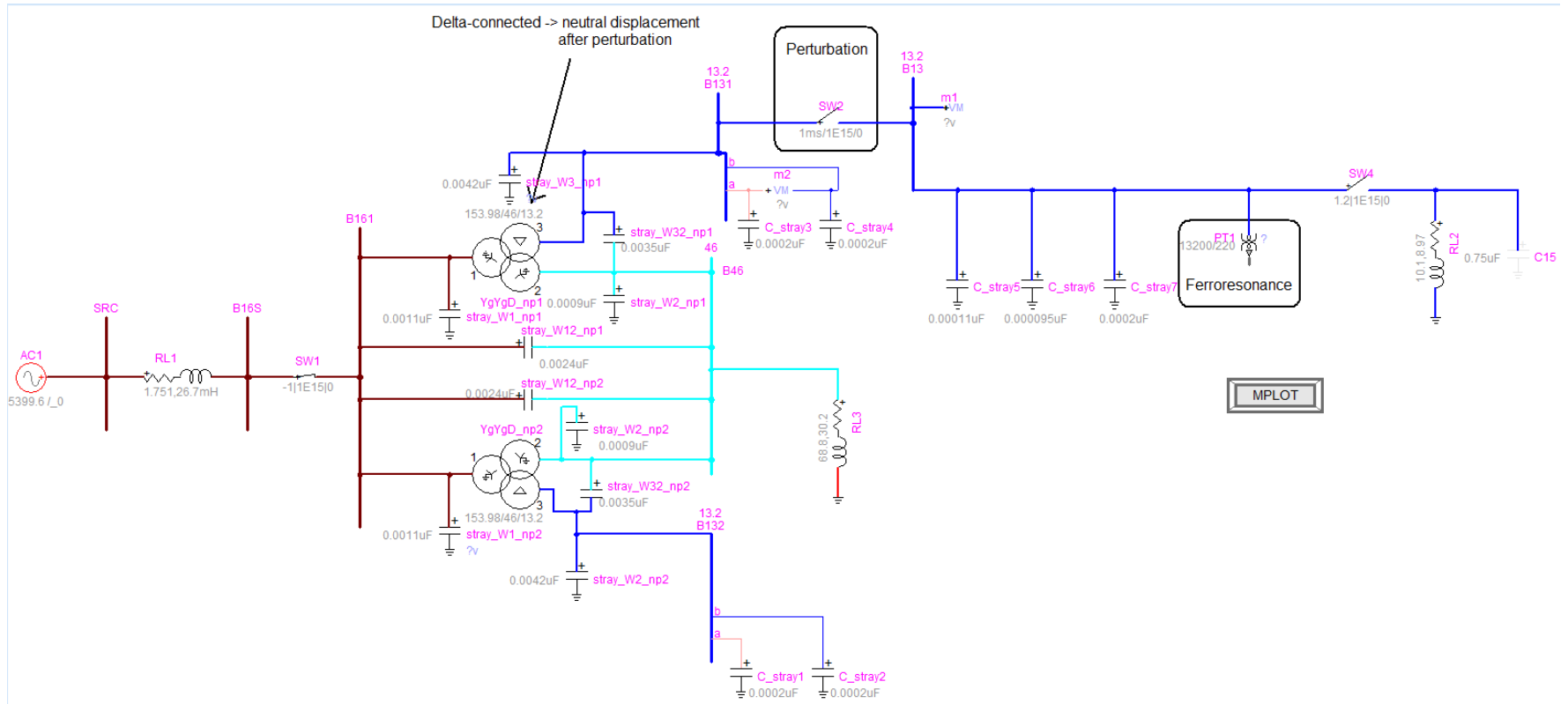


$$V_{switch}(s) := I(s) \cdot \left(R_s + \frac{1}{C \cdot s} \right)$$

$$v_{switch}(t) := V_{switch}(s) \text{ invlaplace, } s \rightarrow 9.76 \times 10^3 \cdot \cos(377 \cdot t) + 5.637 \times 10^3 \cdot \sin(377 \cdot t) - 9.76 \times 10^3 \cdot \cos(2.236 \times 10^4 \cdot t) \cdot e^{-2.191 \times 10^3 \cdot t} + 765.911 \cdot \sin(2.236 \times 10^4 \cdot t) \cdot e^{-2.191 \times 10^3 \cdot t}$$

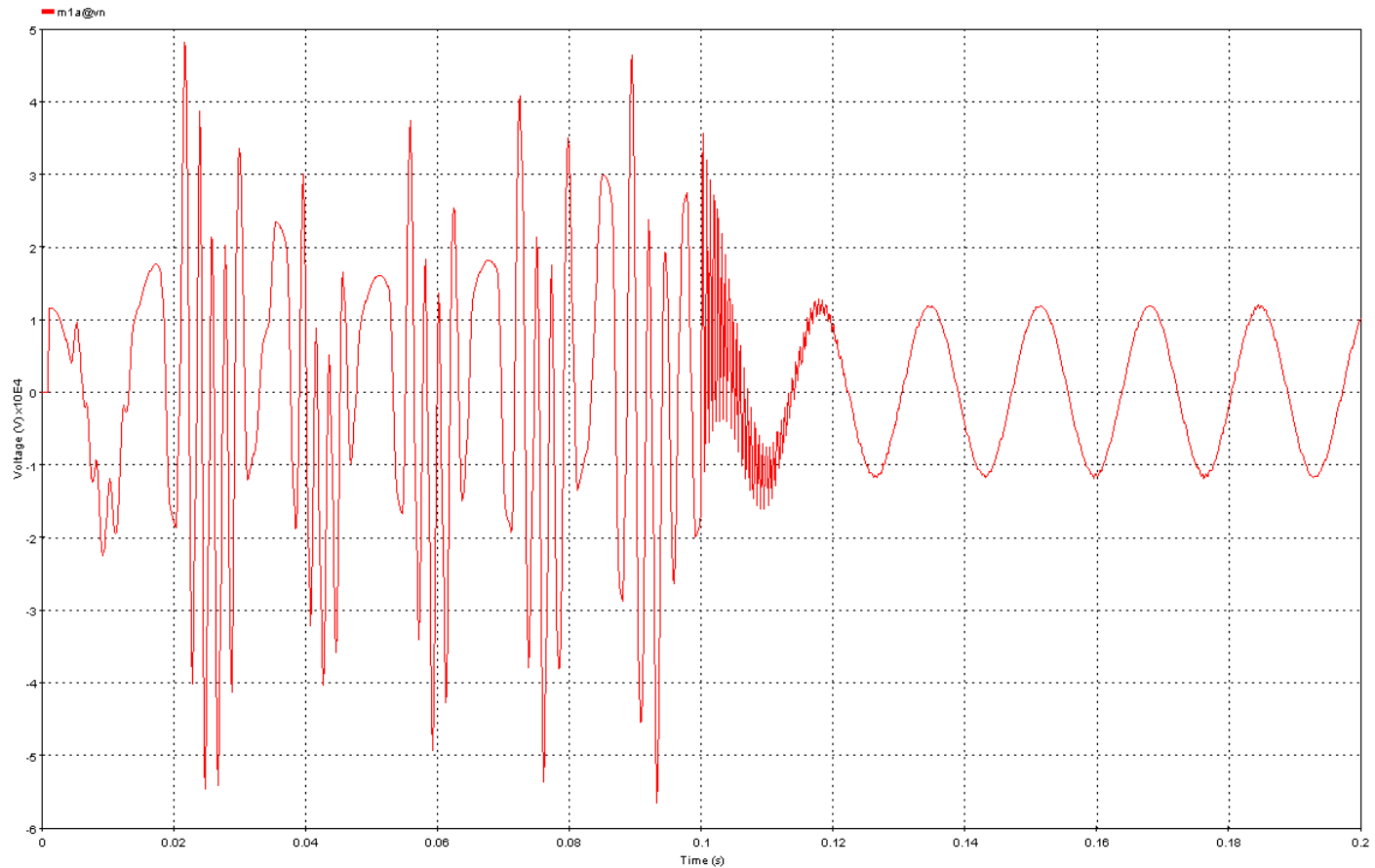
Source: www.clevenstineengineering.com

Snubber Circuit



Source: Henry GRAS, powersys-solutions.com

Snubber Circuit



[EMT1] Ferro1m - Tue Jun 06 21:20:38 EDT 2017 - C:\Users\Thomas King\1\Downloads\Ferro1_pj

Source: Henry GRAS, powersys-solutions.com

Switch-Mode Power Supplies

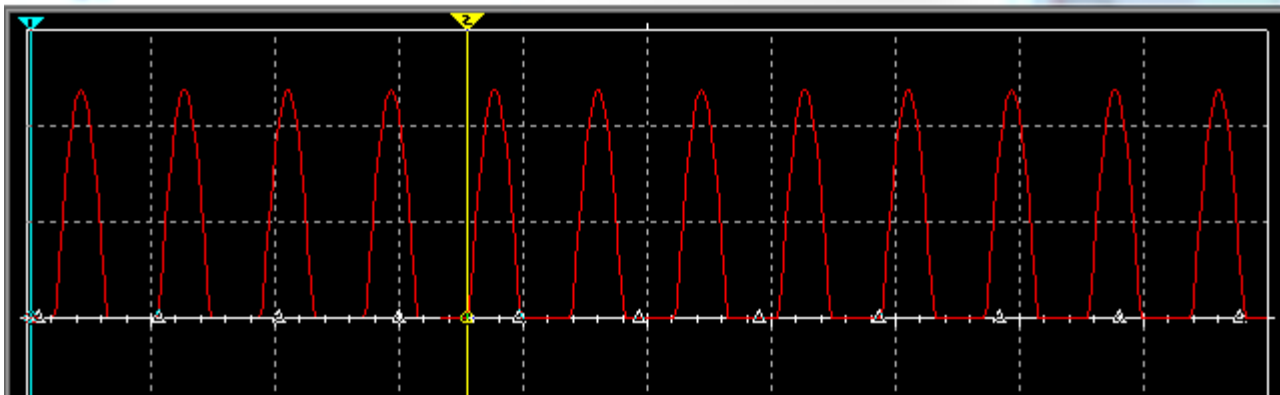
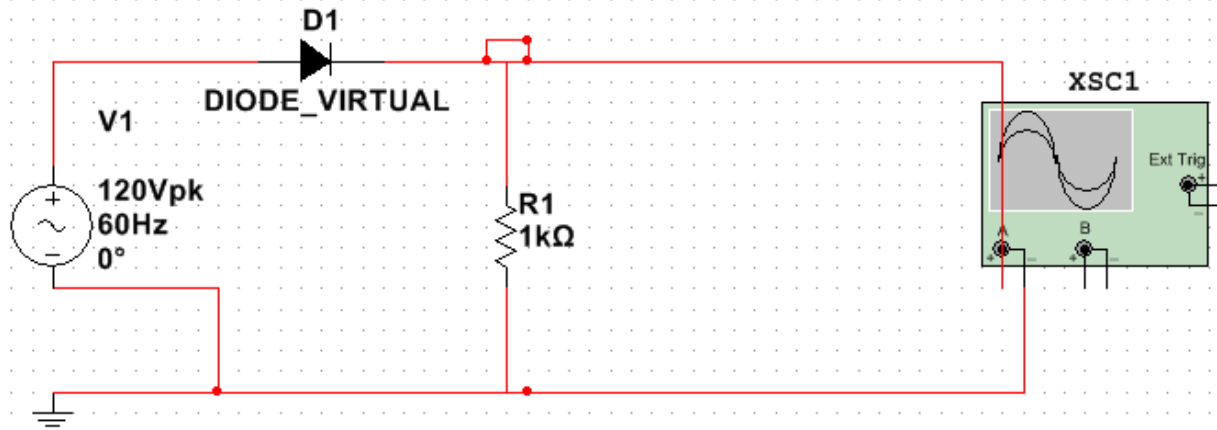


Source: Marco Bieri, Energy Management Specialist

Switch-Mode Power Supplies

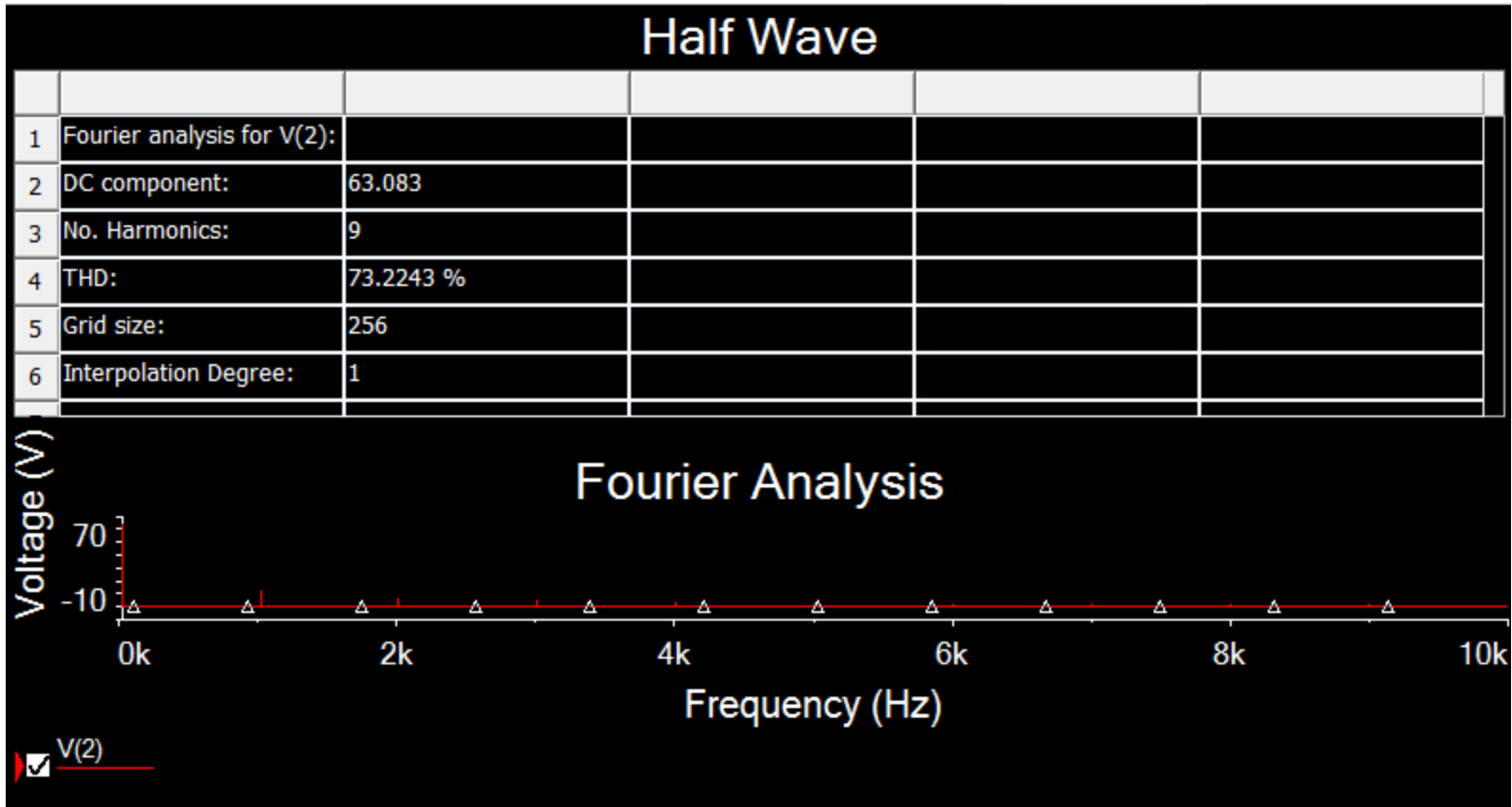
- Switch-Mode Power Supplies include:
 - Half Wave Rectifiers
 - Full Wave Rectifiers (3, 6, and 12 pulse)
 - Variable Frequency Drives
 - Pulse-Width Modulation Inverters

Half Wave Rectifier



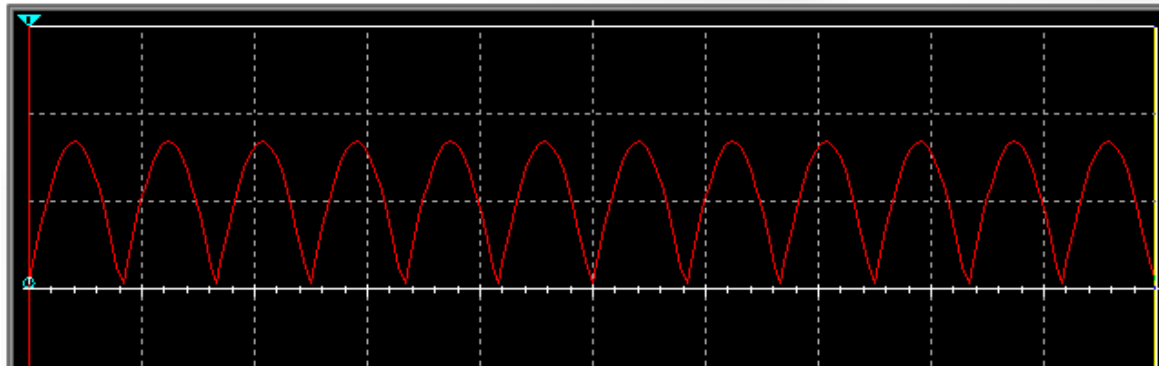
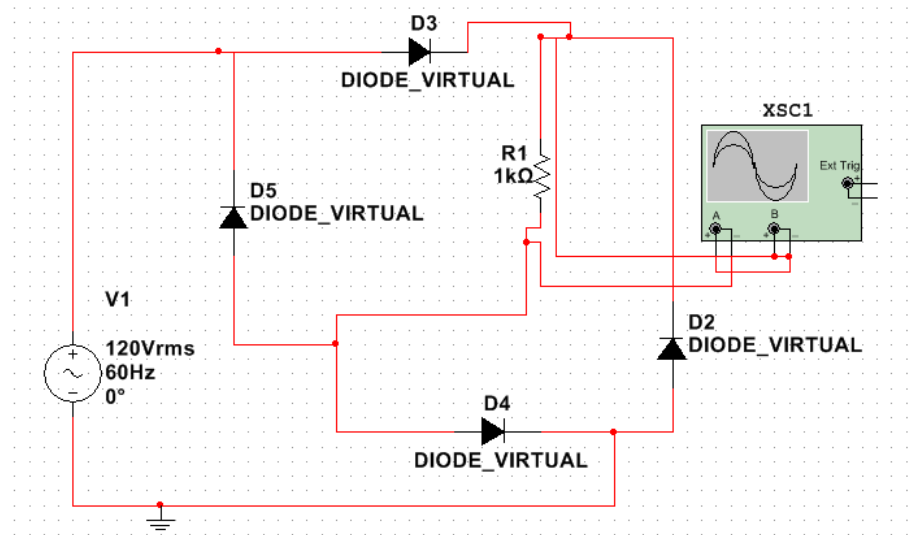
Source: <https://www.allaboutcircuits.com>

Half Wave Rectifier



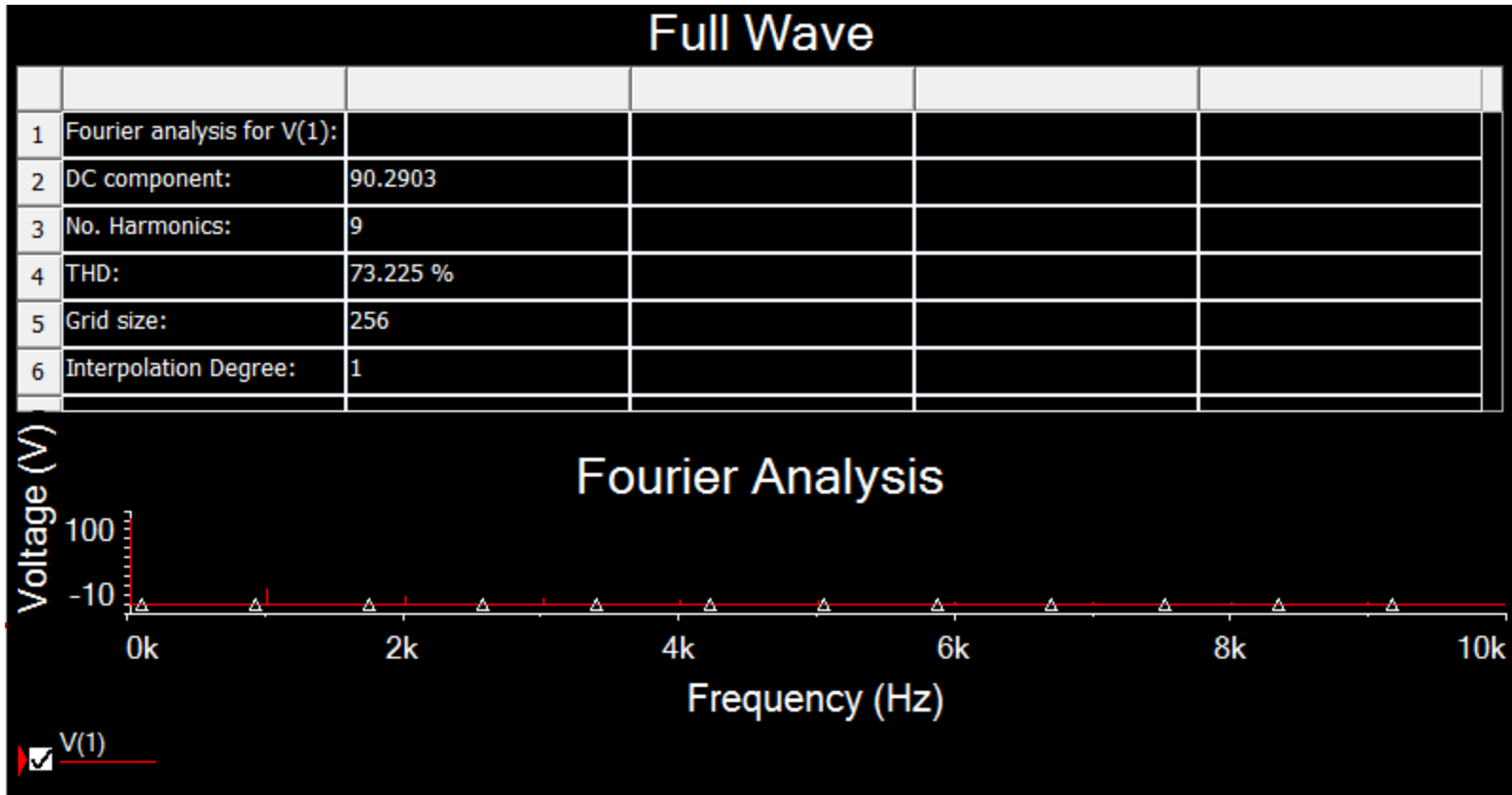
Source: <https://www.allaboutcircuits.com>

Full Wave Rectifier



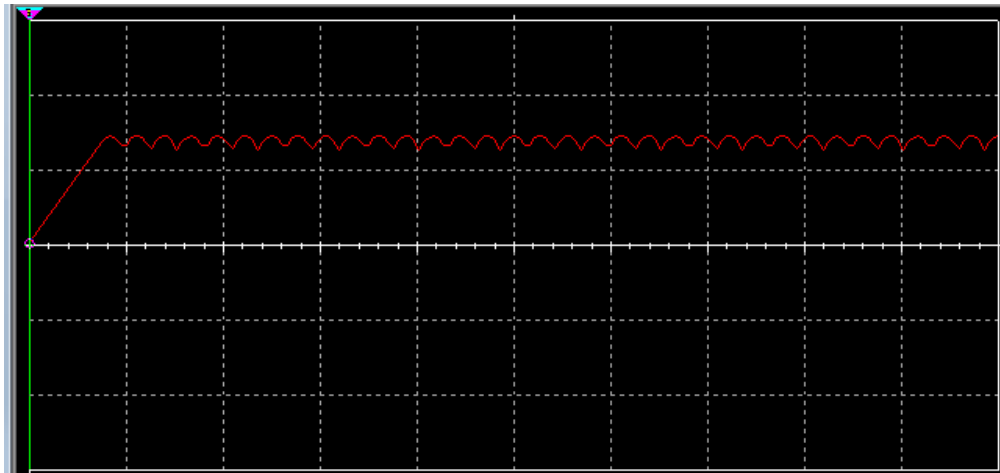
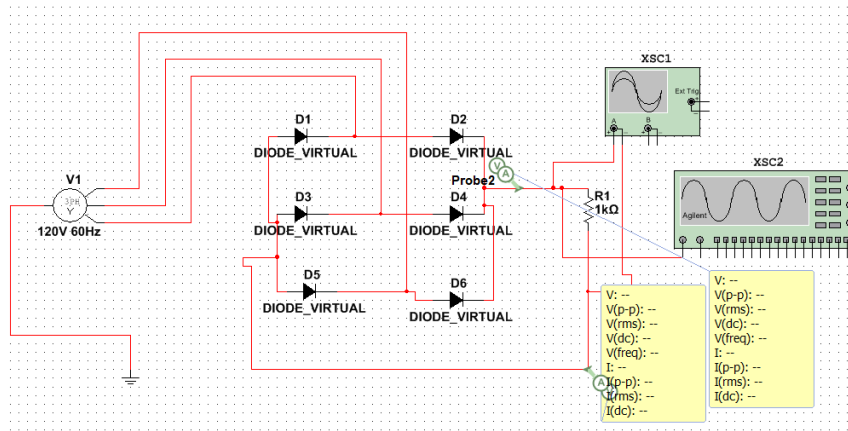
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Full Wave Rectifier



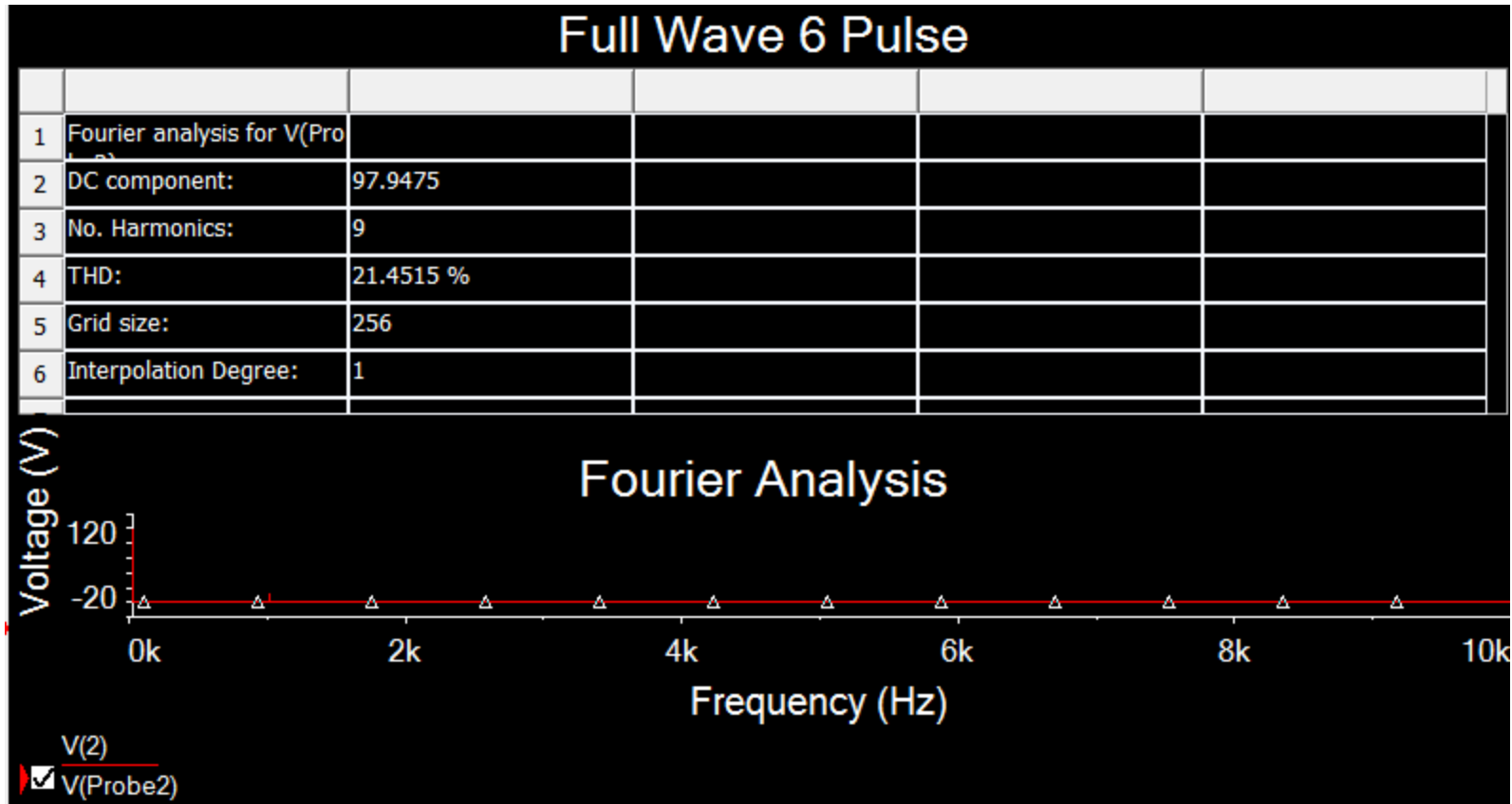
Source: <https://www.allaboutcircuits.com>

Full Wave 6-Pulse Rectifier

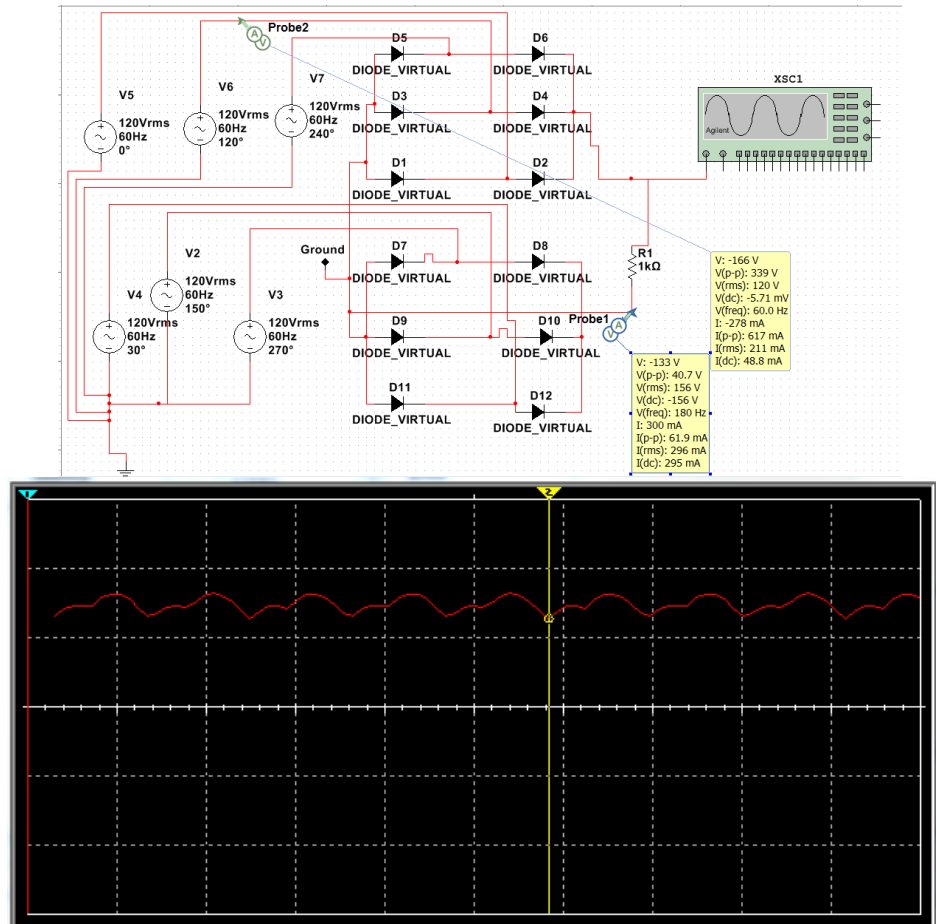


Source: <https://www.allaboutcircuits.com>

Full Wave 6 Pulse Rectifier

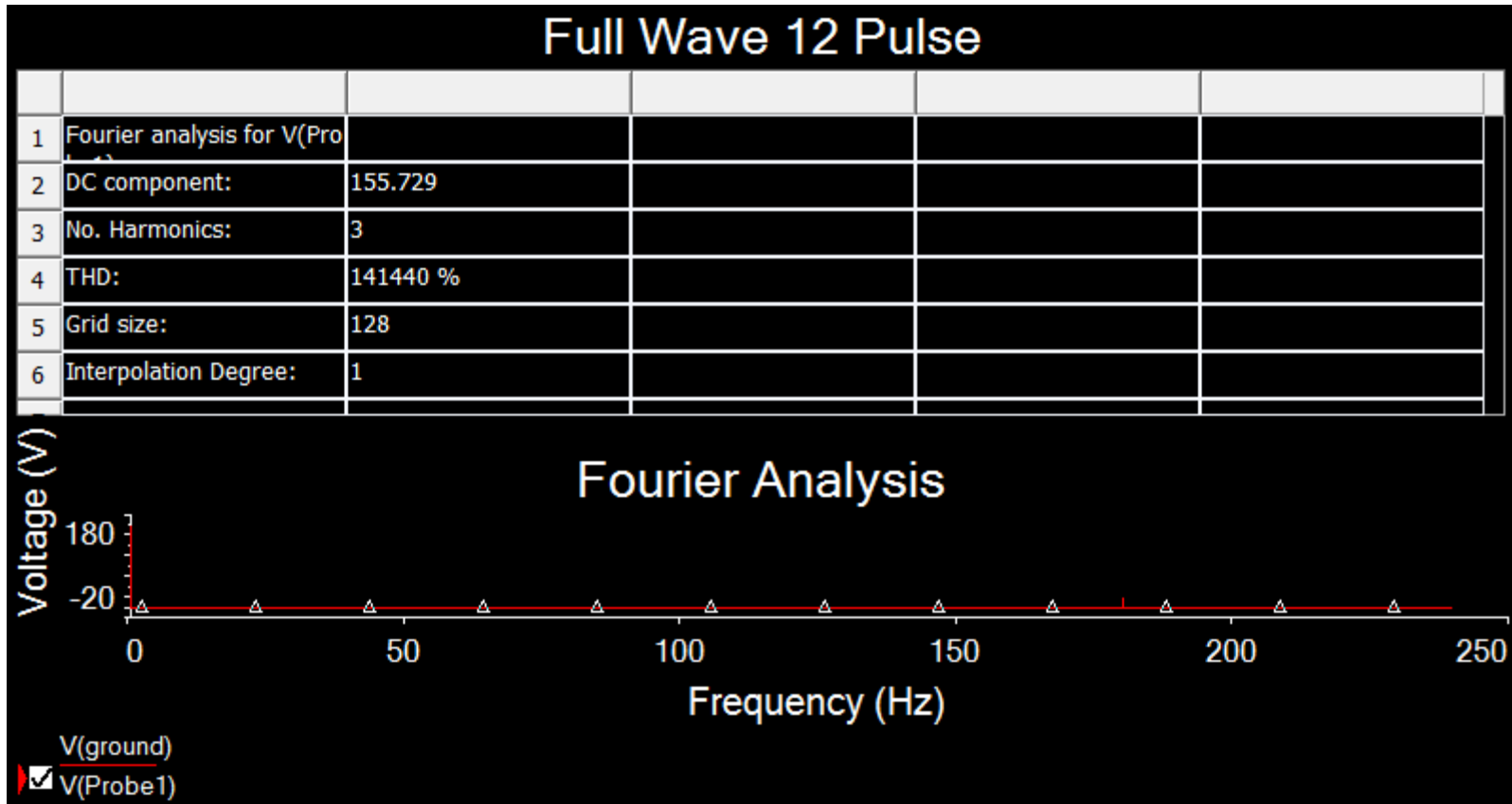


Full Wave 12 Pulse Rectifier



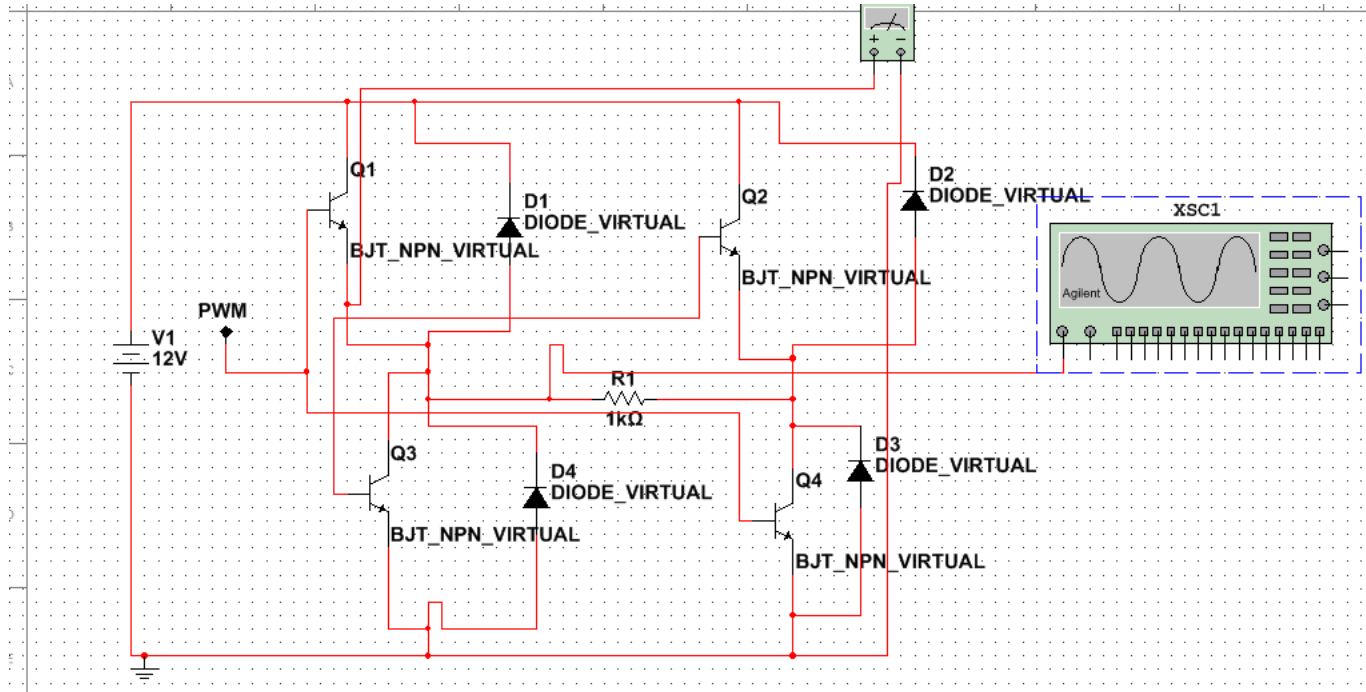
Source: <https://www.allaboutcircuits.com>

Full Wave 12 Pulse Rectifier



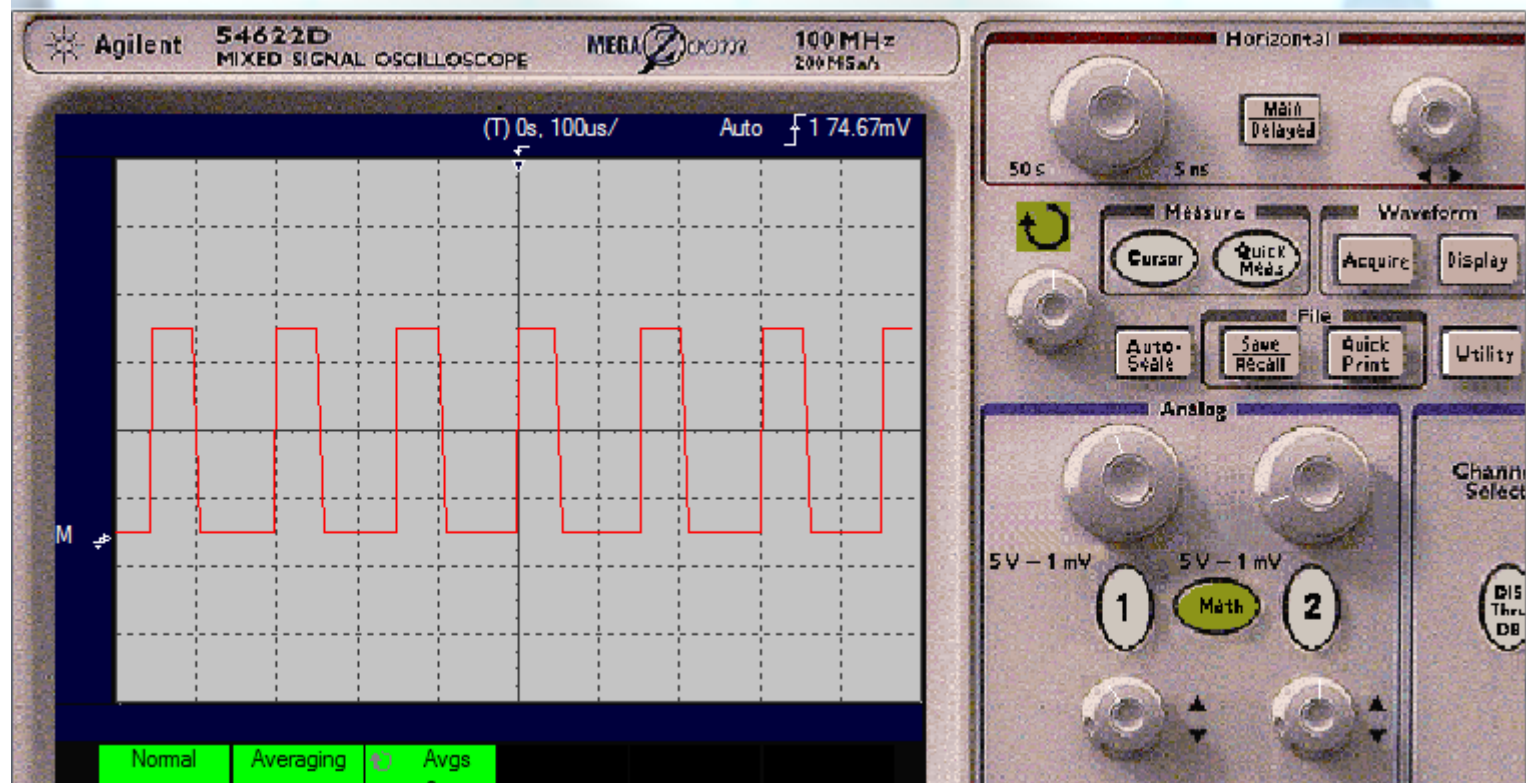
Source: <https://www.allaboutcircuits.com>

Pulse Width Modulation Inverter



Source: <https://www.allaboutcircuits.com>

Pulse Width Modulation Inverter

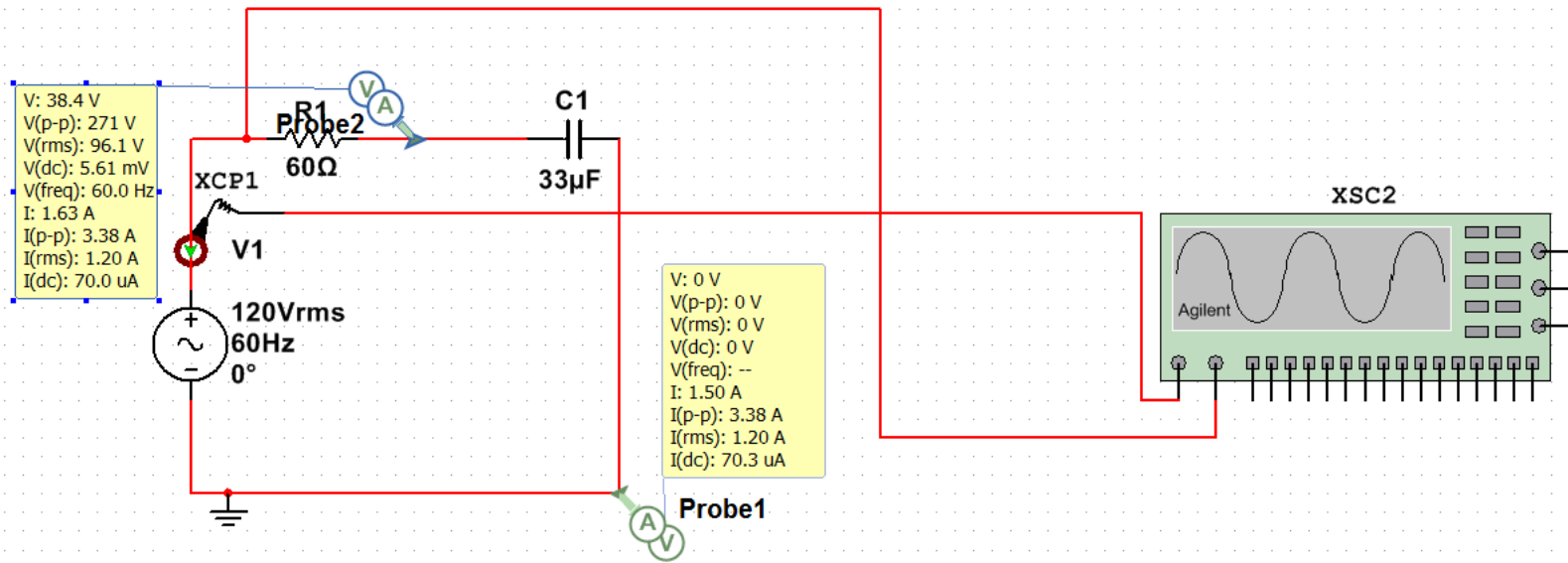


Source: <https://www.allaboutcircuits.com>

Power Factor

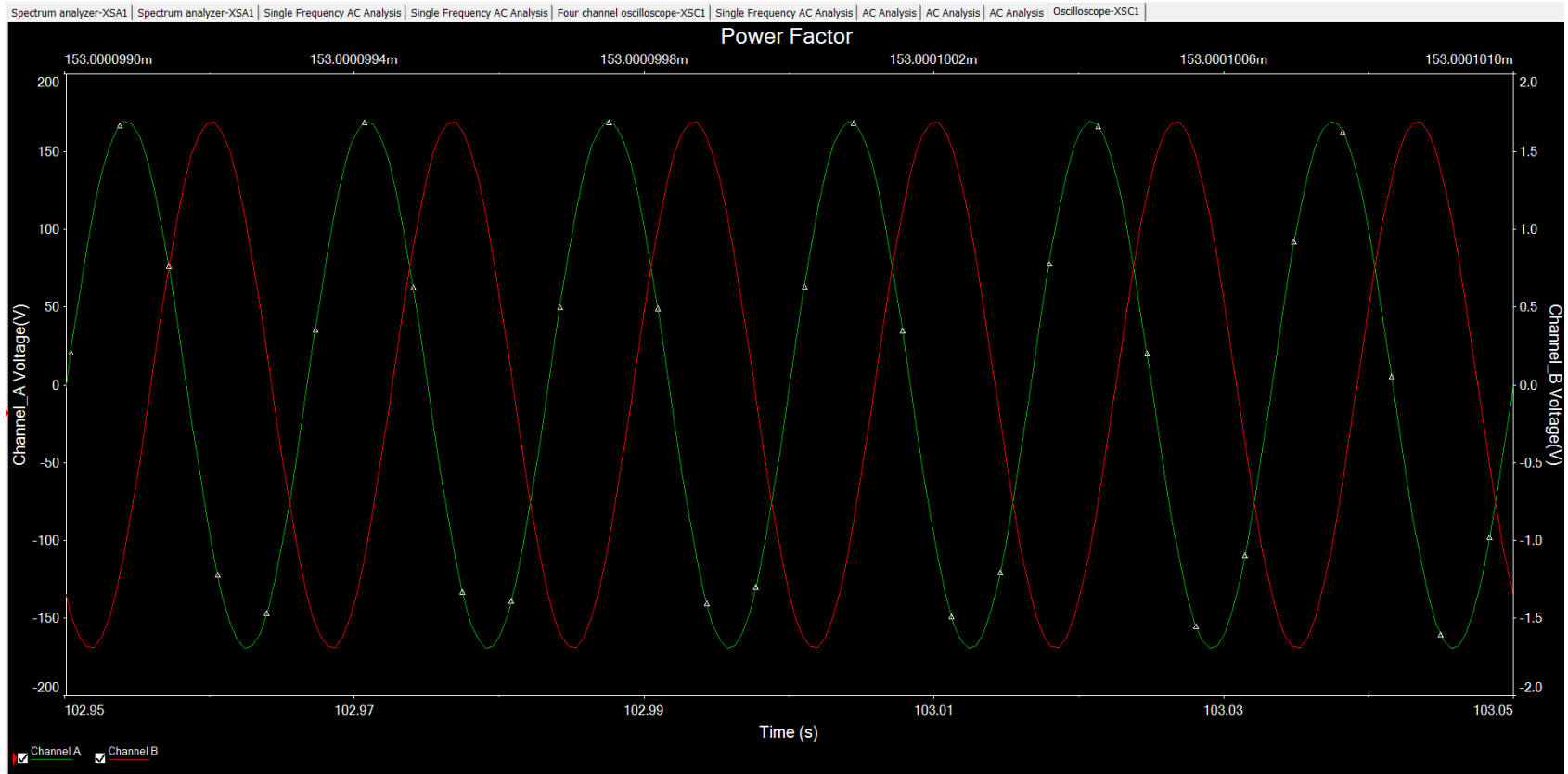
- Power factor is defined as the cosine of the phase angle between the current and voltage waveforms
- Many generators will reject a load with a leading power factor

Power Factor



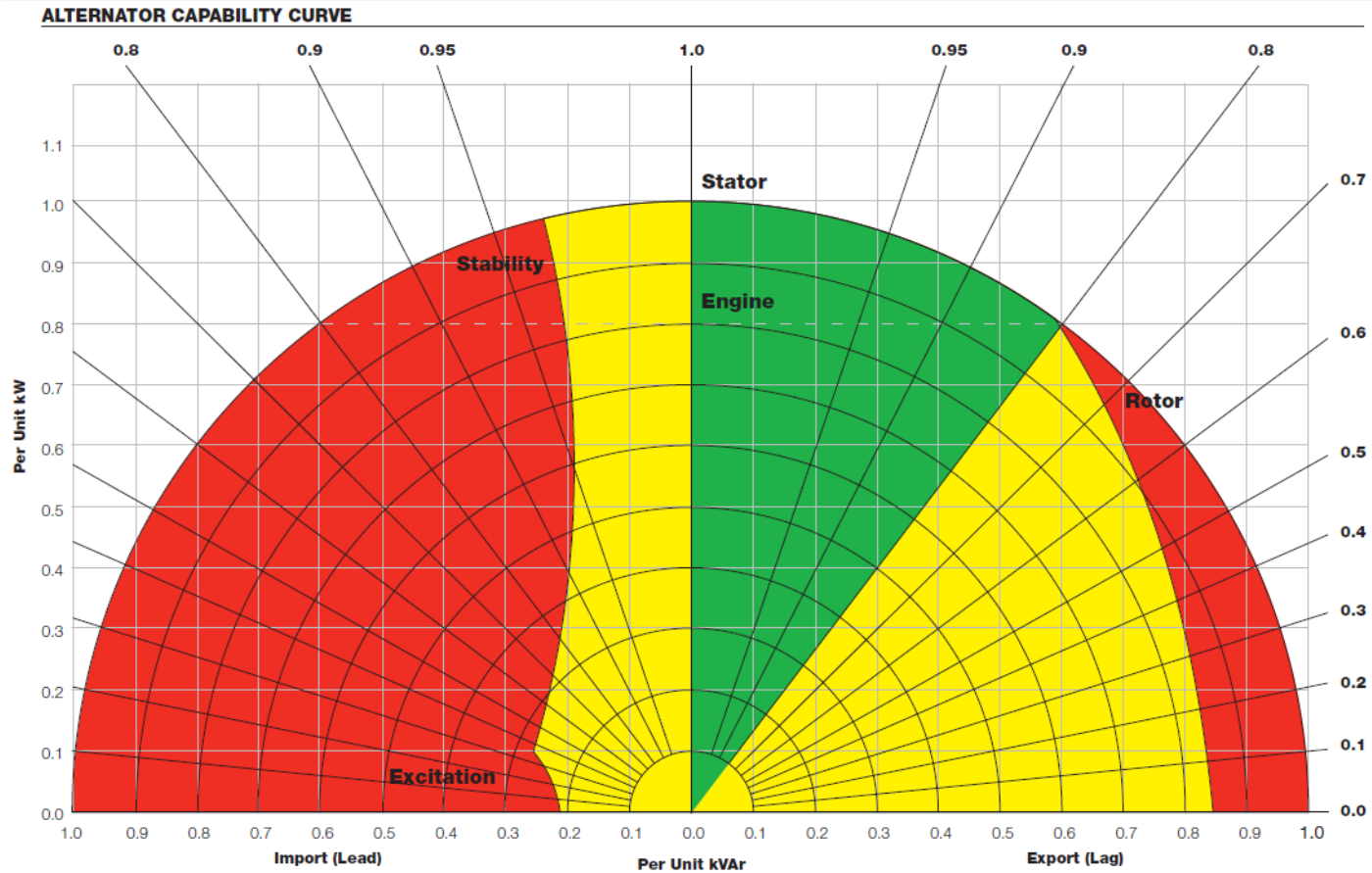
Source: <https://www.allaboutcircuits.com>

Power Factor



Source: <https://www.allaboutcircuits.com>

Power Factor

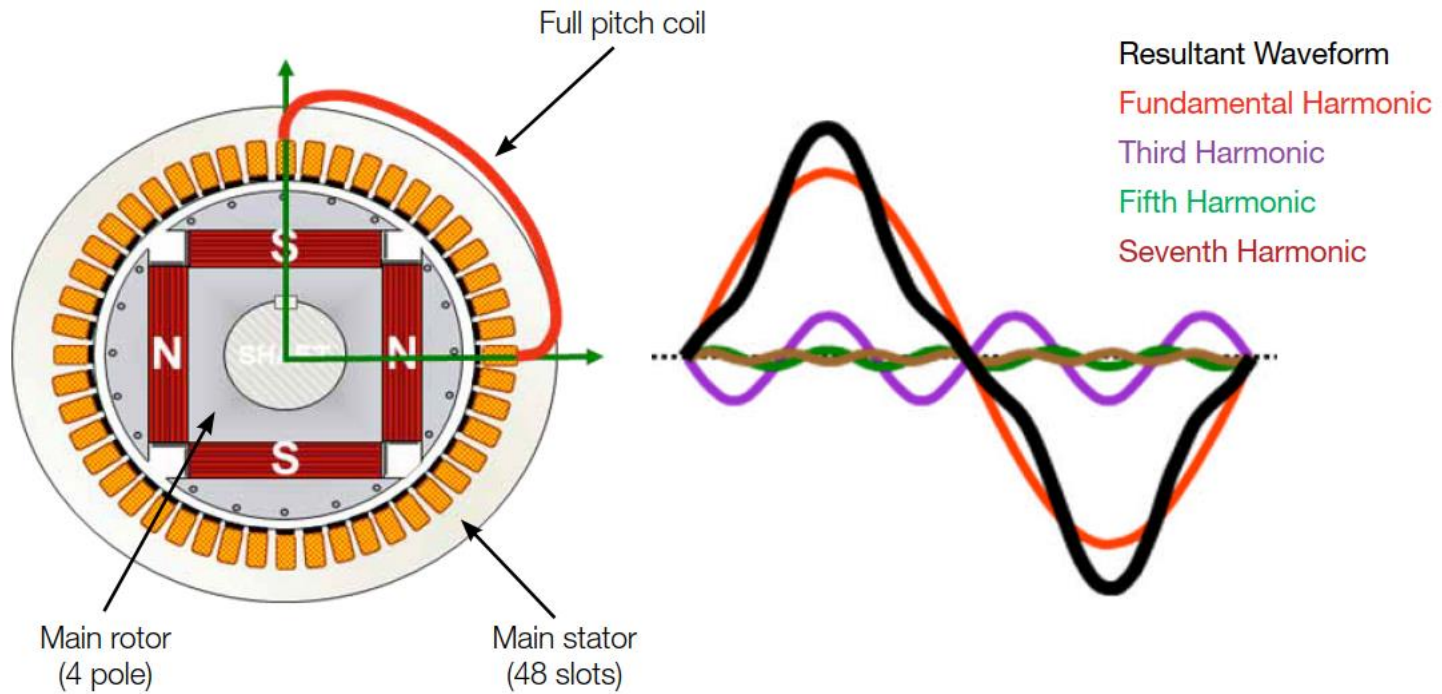


Source: <https://www.allaboutcircuits.com>

Pitch

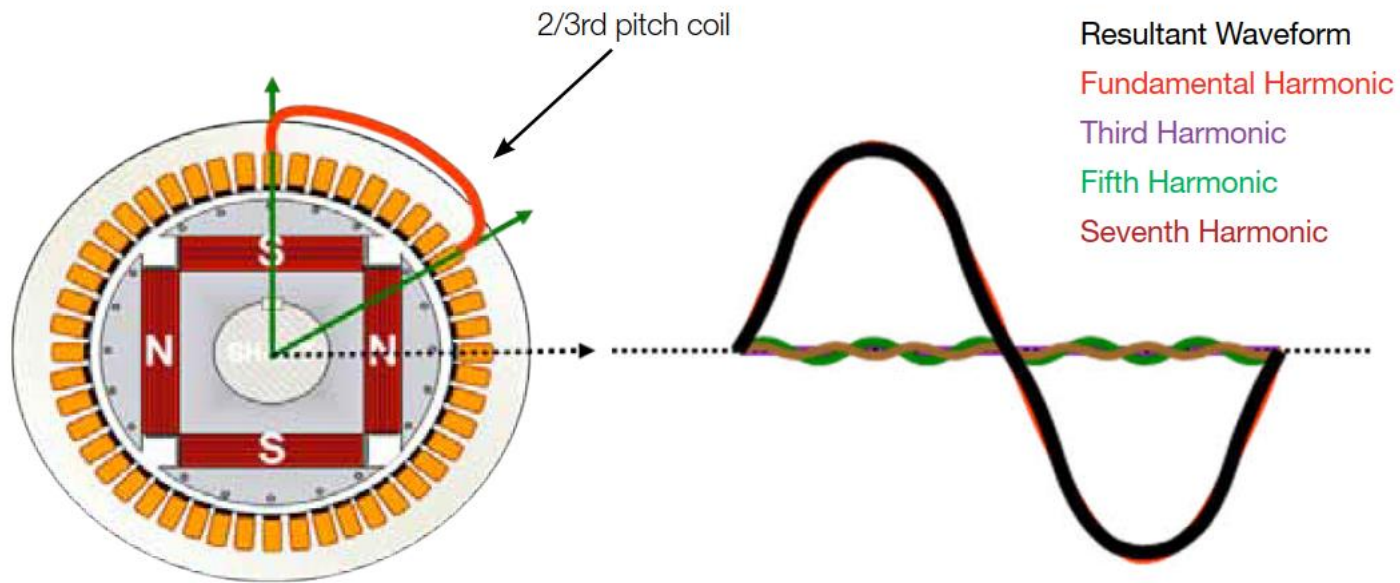
- Alternators do not generate perfect sine waves
- In order to eliminate or reduce specific harmonics, alternators are wound to a specific pitch
- If dissimilarly wound alternators are paralleled, there will be a flow of harmonic currents through the neutral conductor
- To eliminate a harmonic, divide 360 by the harmonic frequency that you want to eliminate, and then divide that by 180. The result is the desired pitch

Pitch



Source: Cummins Generator Technologies

Pitch



Source: Cummins Generator Technologies

Pitch

$$\frac{360}{3} = 120$$

$$\frac{120}{180} = \frac{2}{3}$$

$$\frac{360}{5} = 72$$

$$\frac{72 \cdot 2}{180} = \frac{4}{5}$$

$$\frac{360}{7} = 51$$

$$\frac{51 \cdot 2}{180} = \frac{4}{7}$$

Pitch

Pitch in electrical degrees

$$\rho_0 := 180\text{deg} \quad \rho_1 := 120\text{deg} \quad \rho_2 := 144\text{deg}$$

$$k_{p1} := \cos \left[N_1 \cdot 180\text{deg} \cdot \frac{\left(N_1 - \frac{2}{3} \right)}{2} \right] = 0.866$$

$$k_{p3} := \sin \left(\frac{N_3 \cdot \rho_1}{2} \right) = 0$$

$$k_{p9} := \sin \left(\frac{N_9 \cdot \rho_1}{2} \right) = 0$$

$$k_{p1} := \sin \left(\frac{N_1 \cdot \rho_1}{2} \right) = 0.866$$

$$k_{p5} := \sin \left(\frac{N_5 \cdot \rho_1}{2} \right) = -0.866$$

$$k_{p7} := \sin \left(\frac{N_7 \cdot \rho_1}{2} \right) = 0.866$$

Pitch

Pitch in electrical degrees

$$\rho_0 := 180\text{deg} \quad \rho_1 := 120\text{deg} \quad \rho_2 := 144\text{deg}$$

$$k_{p1} := \cos \left[N_1 \cdot 180\text{deg} \cdot \frac{\left(N_1 - \frac{2}{3} \right)}{2} \right] = 0.866$$

$$k_{p1} := \sin \left(\frac{N_1 \cdot \rho_2}{2} \right) = 0.951$$

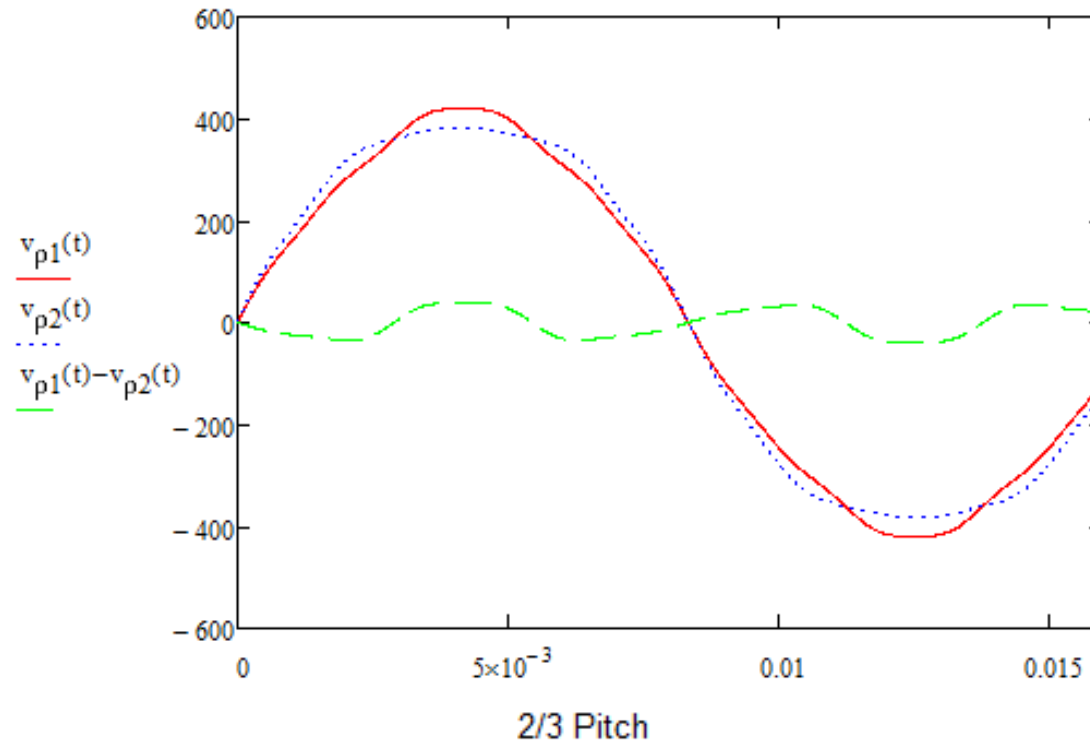
$$k_{p3} := \sin \left(\frac{N_3 \cdot \rho_2}{2} \right) = -0.588$$

$$k_{p5} := \sin \left(\frac{N_5 \cdot \rho_2}{2} \right) = 0$$

$$k_{p9} := \sin \left(\frac{N_9 \cdot \rho_2}{2} \right) = -0.951$$

$$k_{p7} := \sin \left(\frac{N_7 \cdot \rho_2}{2} \right) = 0.588$$

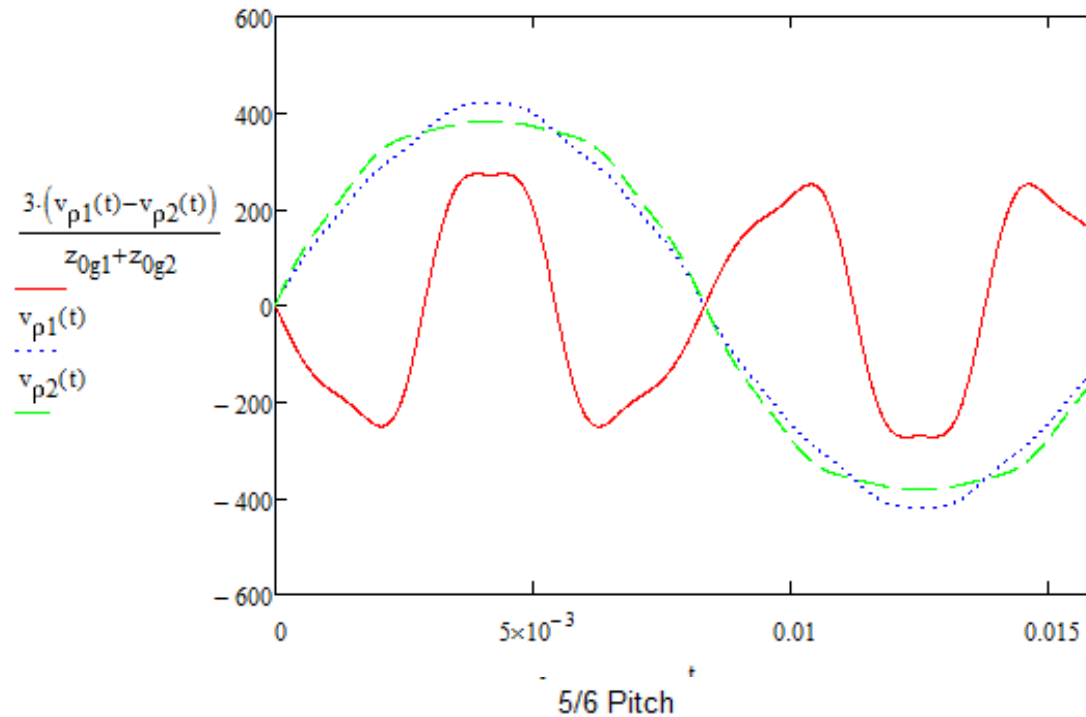
Pitch



$$\begin{aligned}
 v_{p1}(t) := & (k_{p1} \cdot V_p \cdot \sin(\omega \cdot N_1 \cdot t + \theta)) + (.0009 \cdot V_p \cdot \sin(\omega \cdot N_3 \cdot t + \theta)) \dots \\
 & + (.0211 \cdot V_p \cdot \sin(\omega \cdot N_5 \cdot t + \theta)) + (.0035 \cdot V_p \cdot \sin(\omega \cdot N_7 \cdot t + \theta)) \dots \\
 & + .0010 \cdot V_p \cdot \sin(\omega \cdot N_9 \cdot t + \theta) + (.0094 \cdot V_p \cdot \sin(\omega \cdot N_{11} \cdot t + \theta))
 \end{aligned}$$

Pitch

$$z_{pu} := \frac{21.7}{100} = 0.217 \quad z_{0g1} := .21 \quad z_{0g2} := .21^t$$

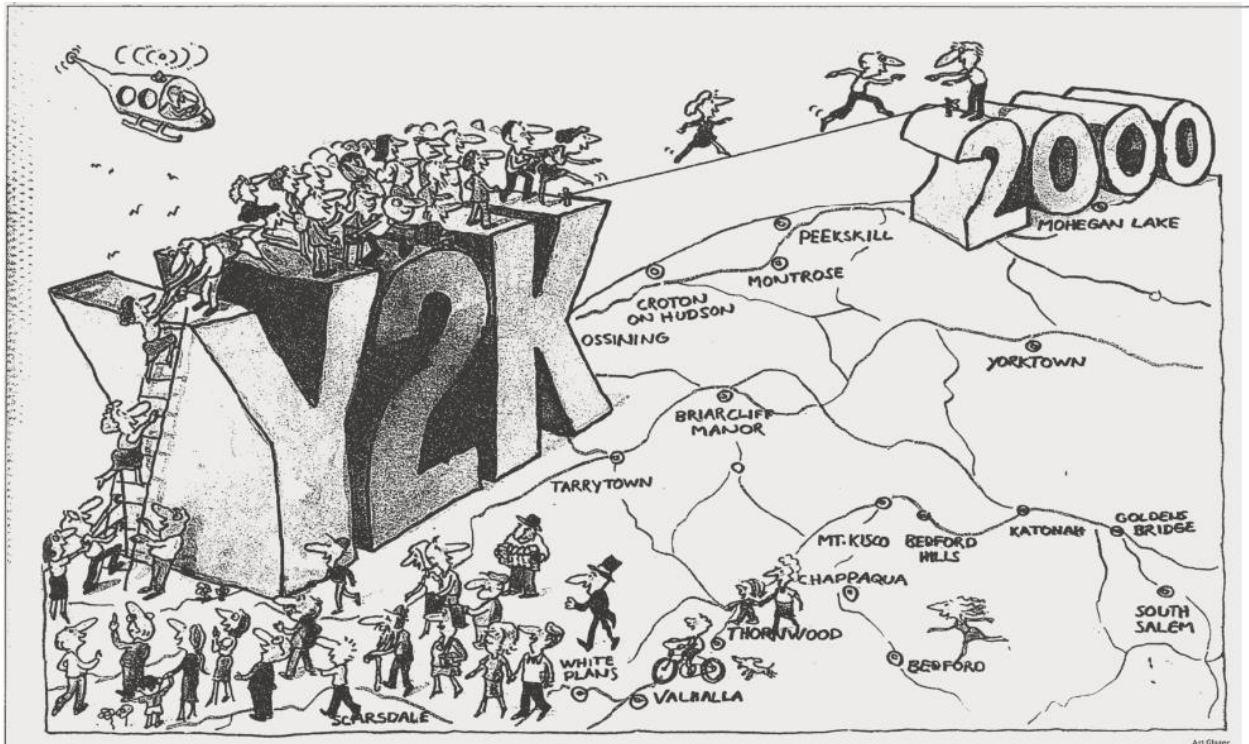


$$v_{p2}(t) := (k_{p1} \cdot V_p \cdot \sin(\omega \cdot N_1 \cdot t + \theta)) + (.0766 \cdot V_p \cdot \sin(\omega \cdot N_3 \cdot t + \theta)) \dots$$

$$+ (.0023 \cdot V_p \cdot \sin(\omega \cdot N_5 \cdot t + \theta)) + (.0018 \cdot V_p \cdot \sin(\omega \cdot N_7 \cdot t + \theta)) \dots$$

$$+ .0115 \cdot V_p \cdot \sin(\omega \cdot N_9 \cdot t + \theta) + (.0063 \cdot V_p \cdot \sin(\omega \cdot N_{11} \cdot t + \theta))$$

Avoid the Fads



Ready to Battle the Unseen

Thousands of Workers Will Be at Their Stations or on Call if Computers Fail