

Hybrid PLL Architectures and Implementations

Presenter: Daniel Friedman

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Technical Team

- Mark Ferriss
- Bodhisatwa Sadhu
- Alexander Rylyakov
- Jose Tierno
- Herschel Ainspan
- Alberto Valdes Garcia
- Daniel Friedman

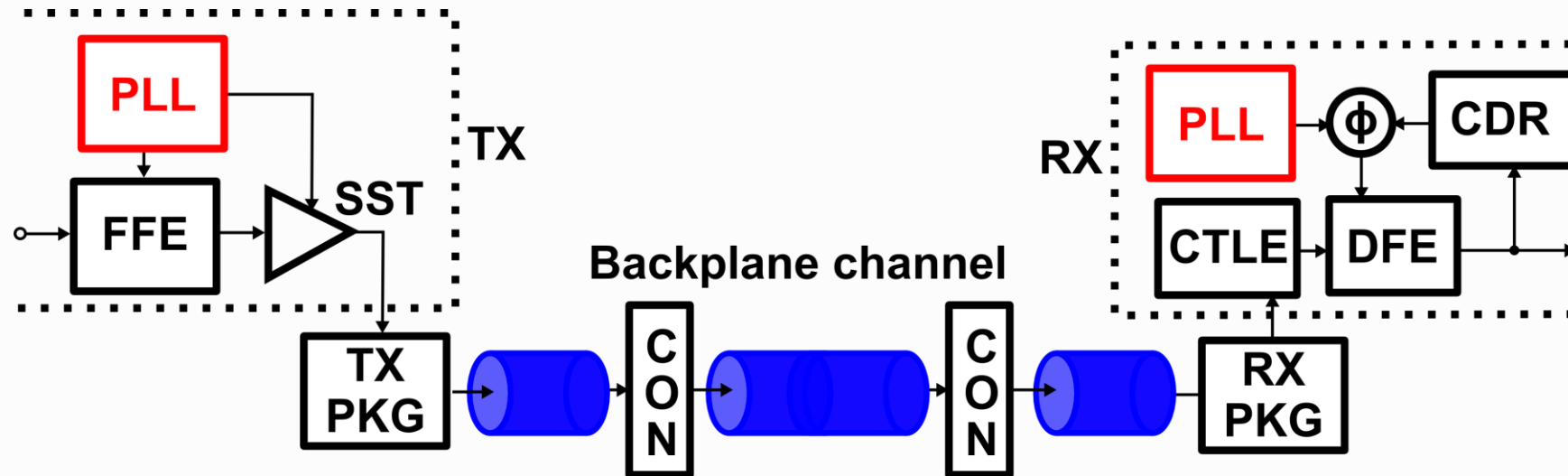
Outline

- Introduction and motivation: hybrid architectures
- Initial implementation: proof-of-concept
- Flexible synthesizer: frac-N w/ noise cancellation
- Flexible synthesizer: coarse band elimination
- Flexible synthesizer: flicker noise suppression exploration
- Summary/conclusion

Motivation: Application challenges

Context/relevant applications:

- High speed serial links
- Clock synthesis for mm-wave wireless



Opportunities for hybrid analog/digital PLLs:

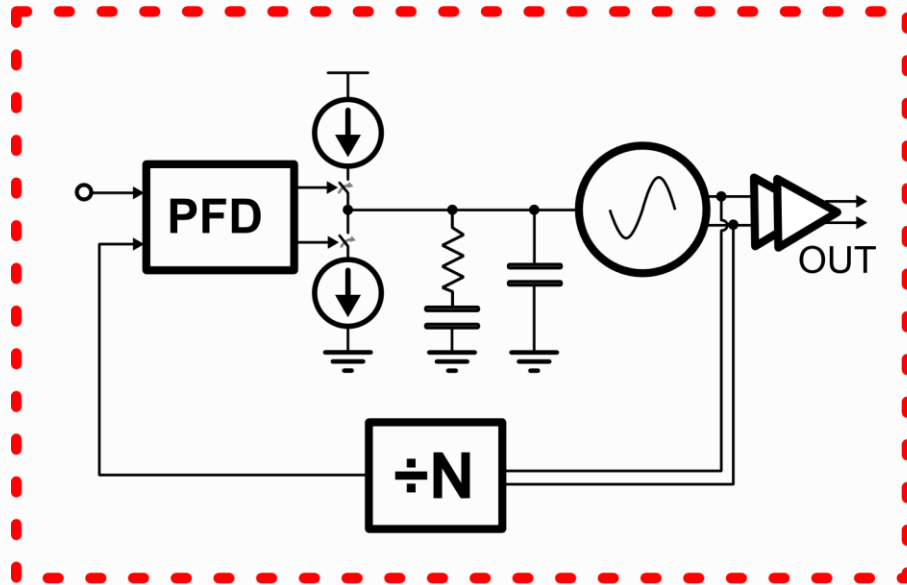
- Reduce dependence on special technology elements
- Reduce PLL area
- Introduce new functionality and improve testability

Challenges:

- *must continue to meet stringent phase noise, tuning range, and robustness requirements set by application*

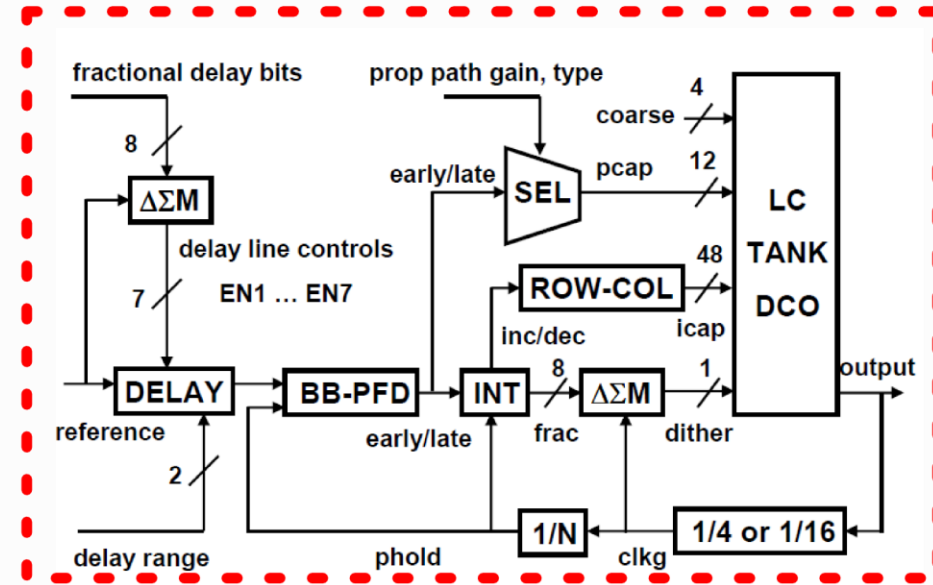
Architecture tradeoff: Analog versus digital

Conventional analog PLL



- Requires large, low leakage capacitor (unfriendly to digital process)
- Requires wide dynamic range charge pumps

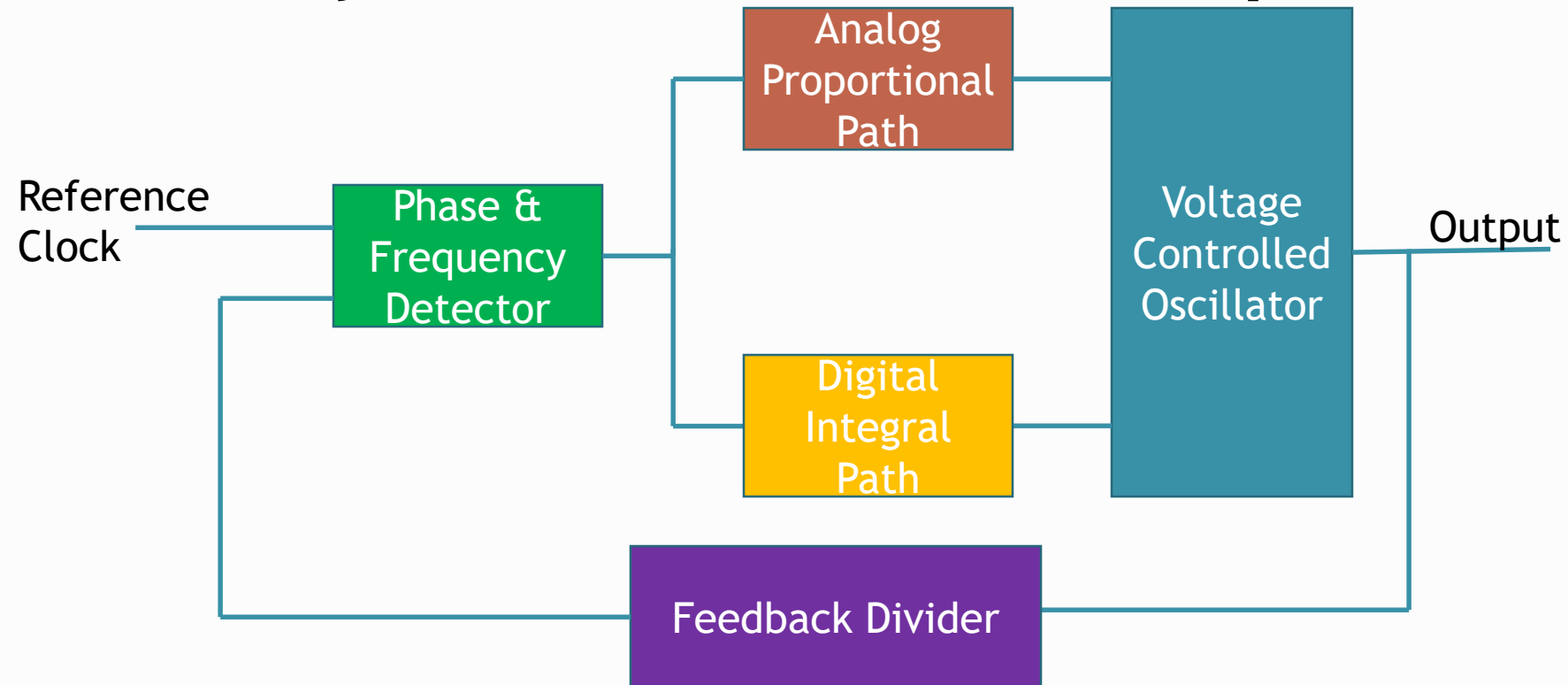
Prior art digital PLL [1]



A. Rylyakov et al., ISSCC 2009.

- Nonlinearity of digital components leads to spurs in the output spectrum
- PLL can slew in response to small phase errors
- Transfer function of all digital PLL is noise-dependent

Hybrid PLL: Core Concept

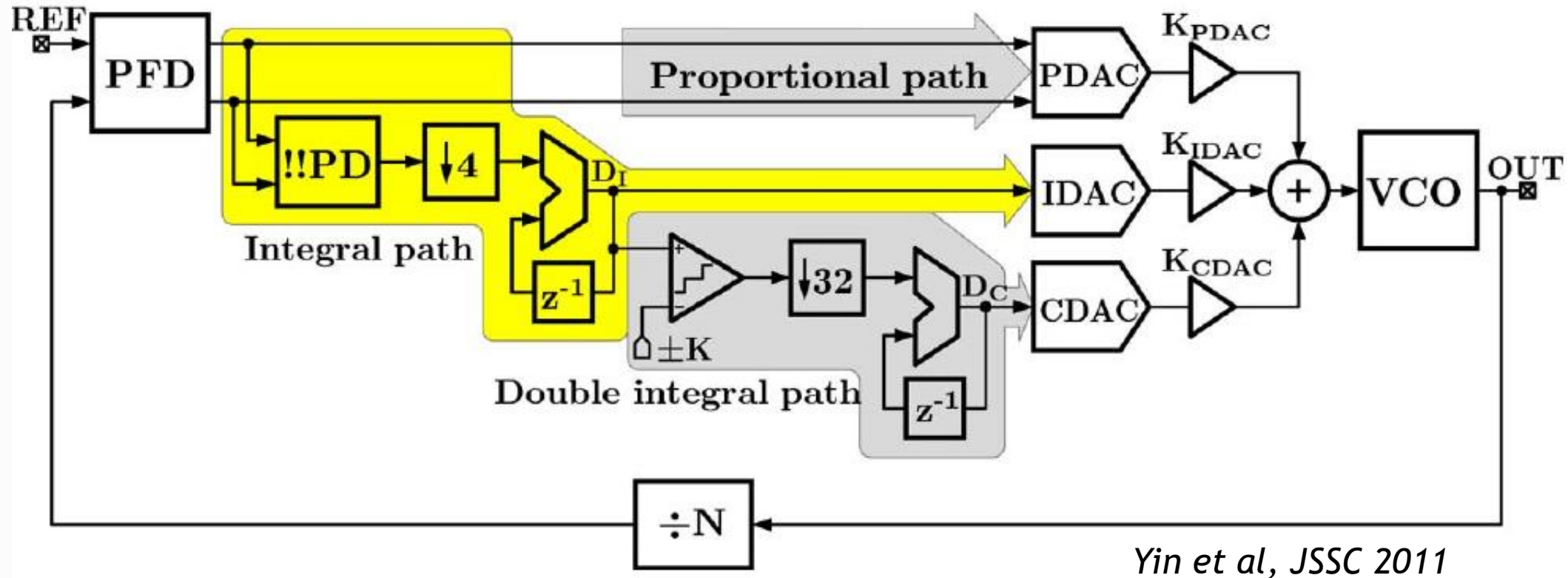


- Proportional path: pulse width modulated signal as in analog PLL
- Integral path: create control word using DSP as in digital PLL

Opportunity to achieve best-of-both worlds properties

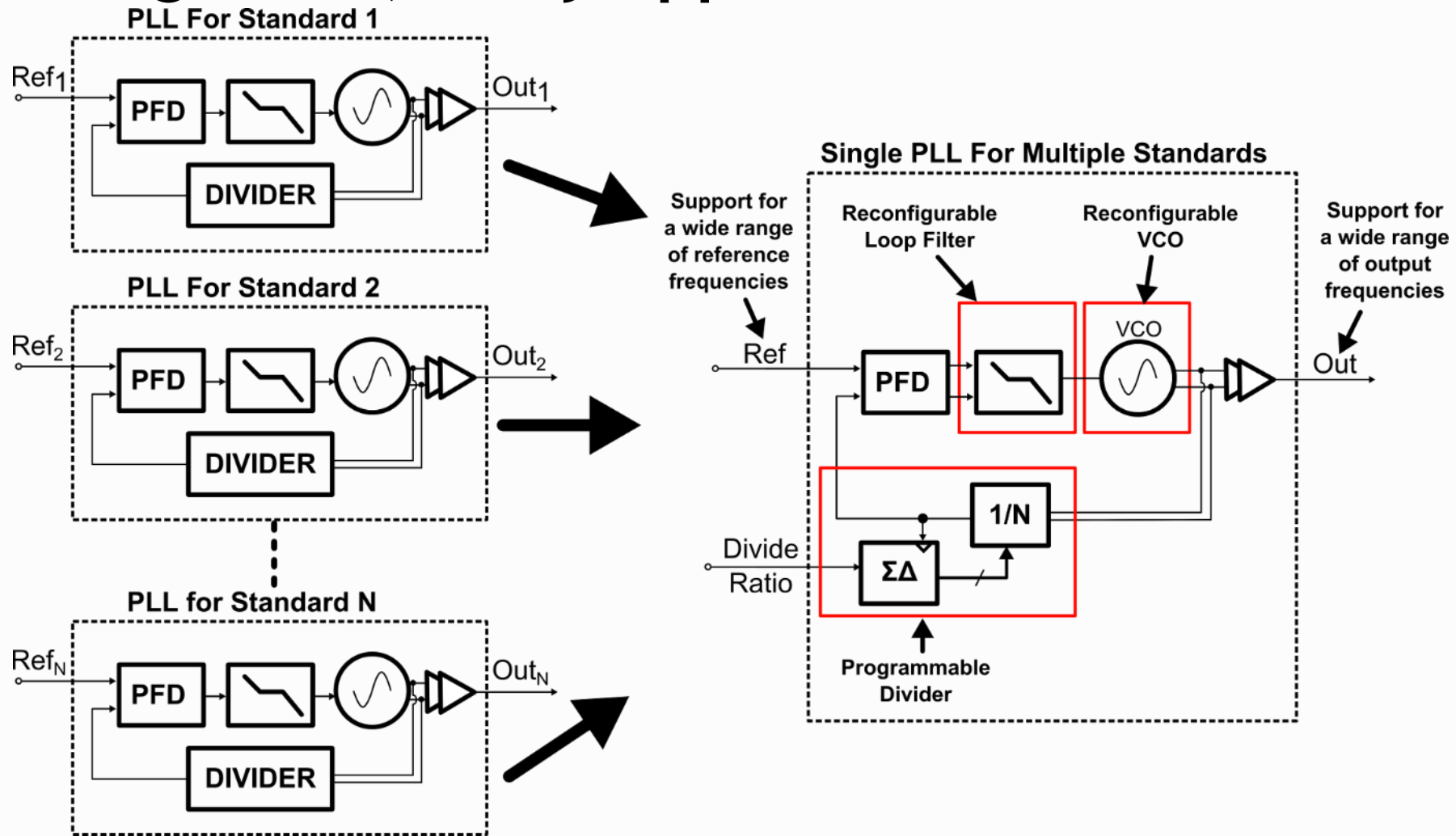
- Linear proportional path with simplified charge pump versus analog PLL
- Compact digital integral path with extensive digital domain sensing and actuation enablement

Example Hybrid PLL Architecture



- Proportional path drives a scaled pulsewidth modulated signal into VCO control node
- Integral path drives a digital control word to the IDAC/CDAC path
- Oscillator is current-controlled ring

Hybrid PLL Opportunity: Single PLL, Many Applications- 2 - 26GHz



Vision: Replace multiple custom synthesizers with a single, flexible, dynamically reconfigurable PLL for wireless and wireline high performance applications

Preview: Flexible Synthesizer Features Achieved Using Hybrid PLL Approach

Characteristic	Objectives	Implementation Approach
Tuning range 2-26GHz	Continuous tuning range to maximum frequency	Wide-range dual linearized transconductance VCO complex
Loop transfer function control	High programmability over wide range through digital control	Leverage highly digital architecture of dual-path HPLL
Supported reference rate	Flexible without sacrificing performance	Fractional-N synthesis
Fractional-N quantization noise	Active noise cancellation scheme that does not limit bandwidth	Proportional & integral path highly digital cancellation architecture
Area	Less than 1 mm ² total	Single PLL with wide-range dual VCO complex
Fast frequency hopping	Fast settling time based on digital memory	Leverage digital memory/parameter replay
Spurious content	Minimize to enable broader use model	Reduced by utilization of digital/predictive techniques
Extended range in main loop	Eliminate need for coarse bands in supporting wide tuning range	Enhance and extend digital integral path approach to include full VCO range

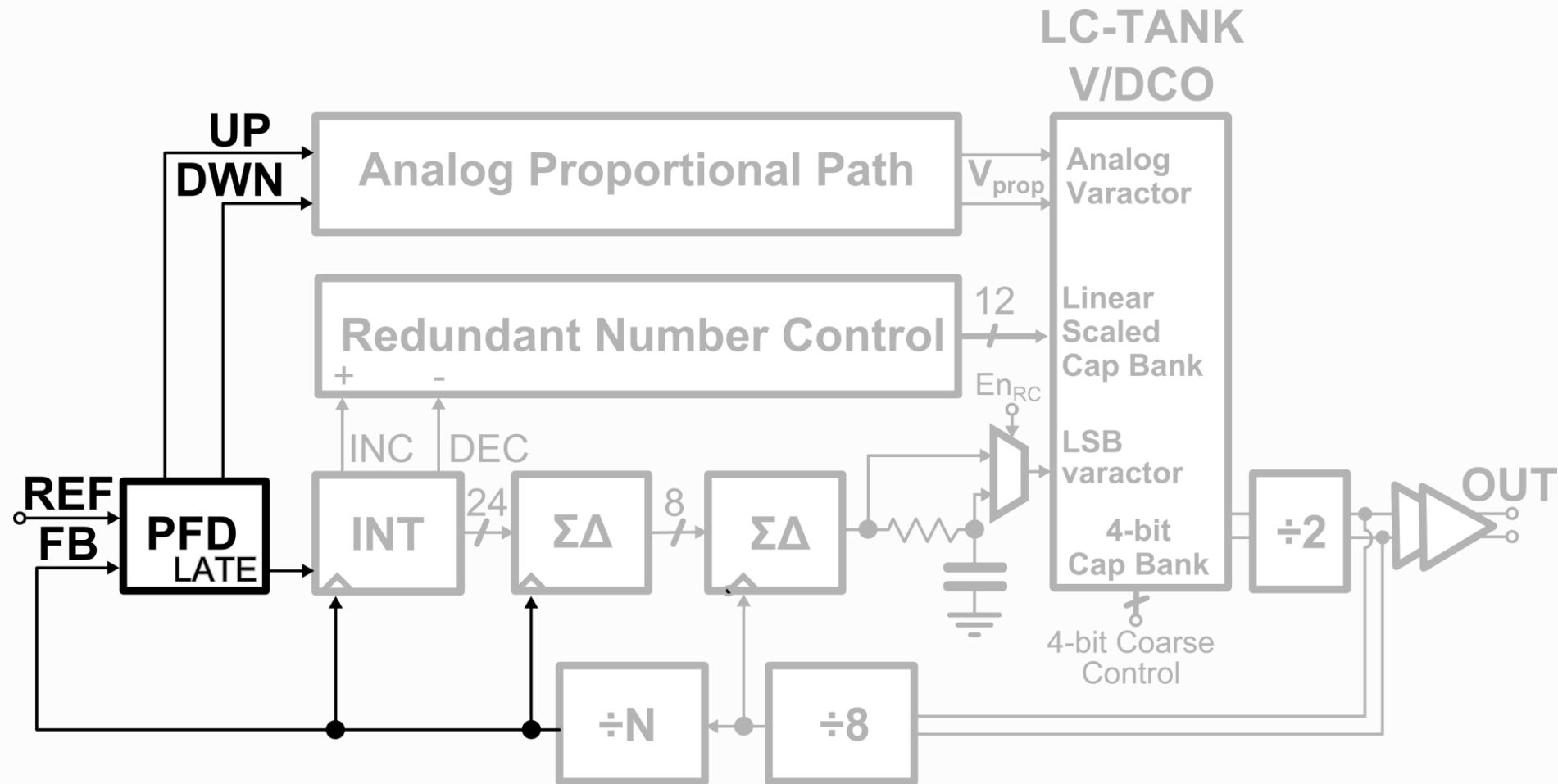
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High Performance Hybrid PLL

- Objective: demonstrate hybrid PLL in high performance (LC-VCO-based) context while maintaining tuning range of analog implementation
- Approach
 - Proportional path varactor driven by simplified PWM path
 - Integral path controls fixed and $\Sigma\Delta$ modulated switched capacitance in D/VCO (implicit DAC)
 - Coarse band architecture to enable wide tuning range without sacrificing phase noise performance
- Key challenges
 - Integral path design
 - D/VCO integration

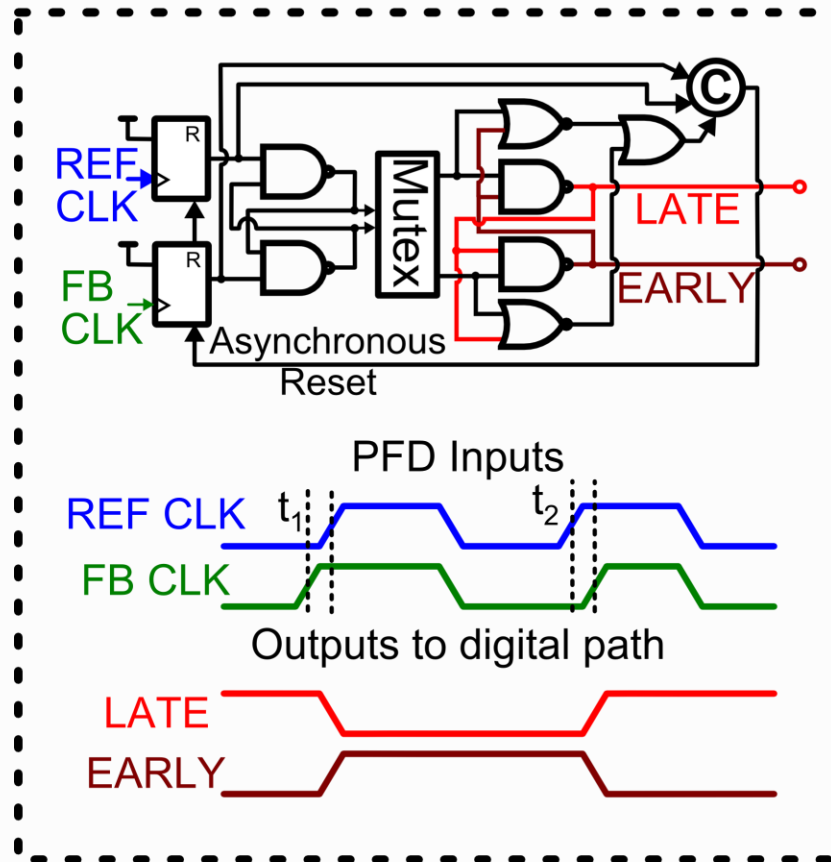
HPLL Phase and frequency detector (PFD)



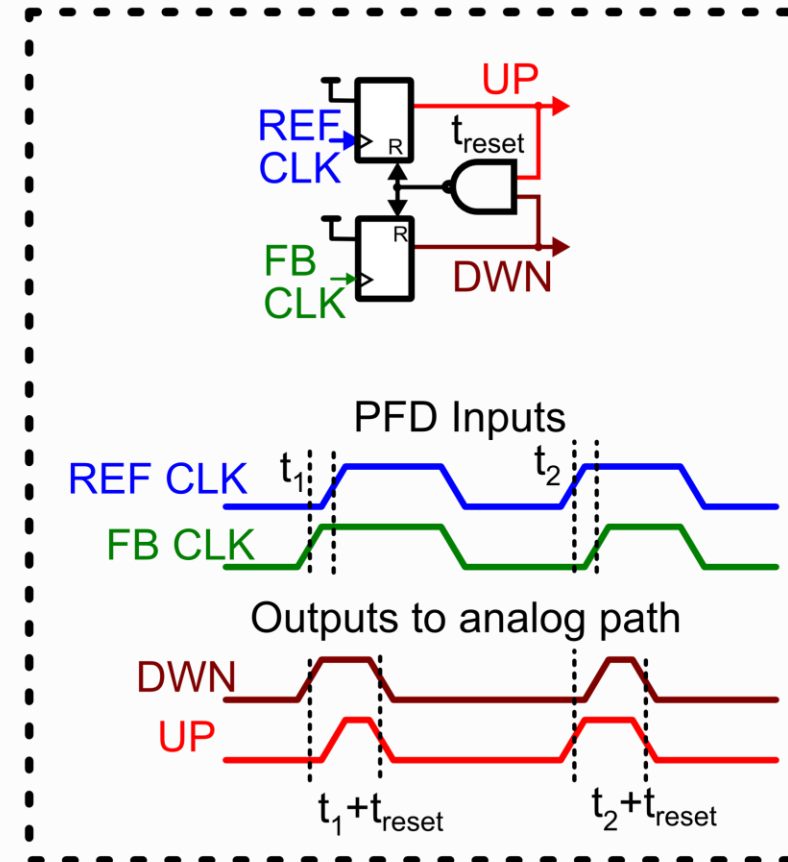
- Requires phase detector with analog (linear) and digital (bang-bang) outputs
- Do we need two phase detectors?

Example phase detectors for digital and analog PLLs

Prior art BB-PFD [2] for digital PLL



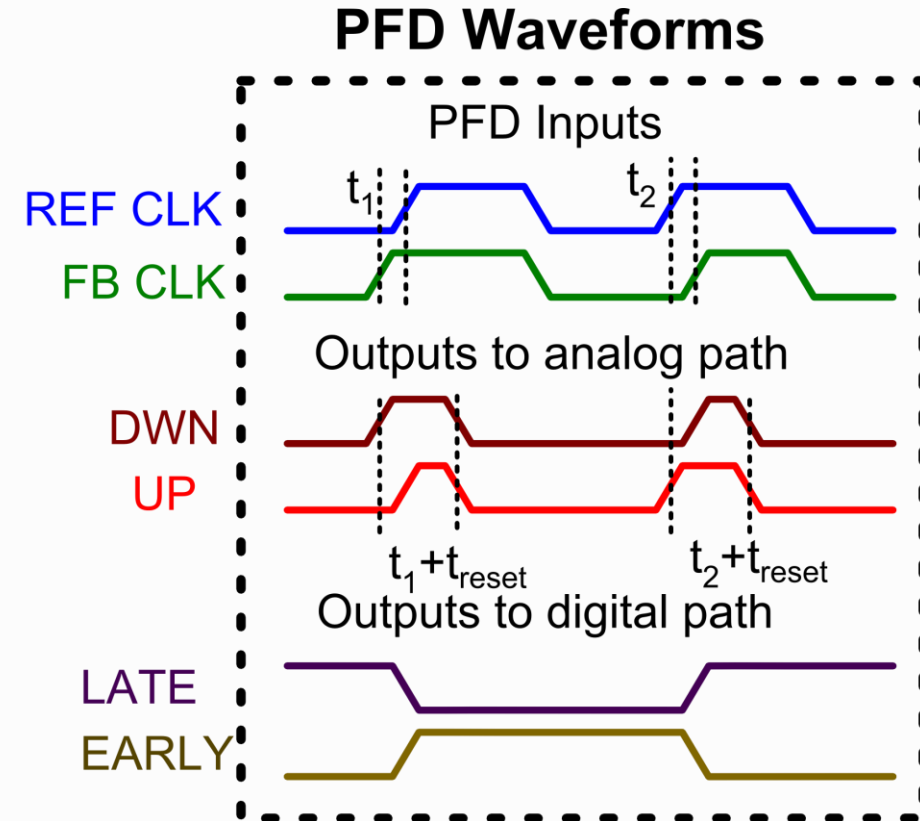
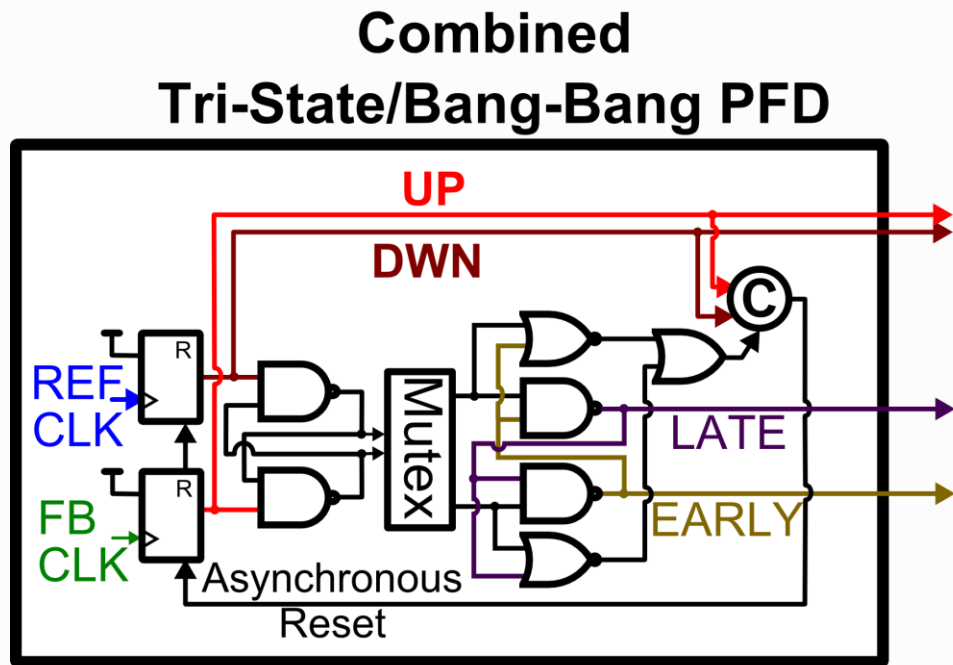
Conventional tri-state PFD for
charge pump based PLL



© -Muller C element. If all inputs have the same logic value, then the output matches inputs.

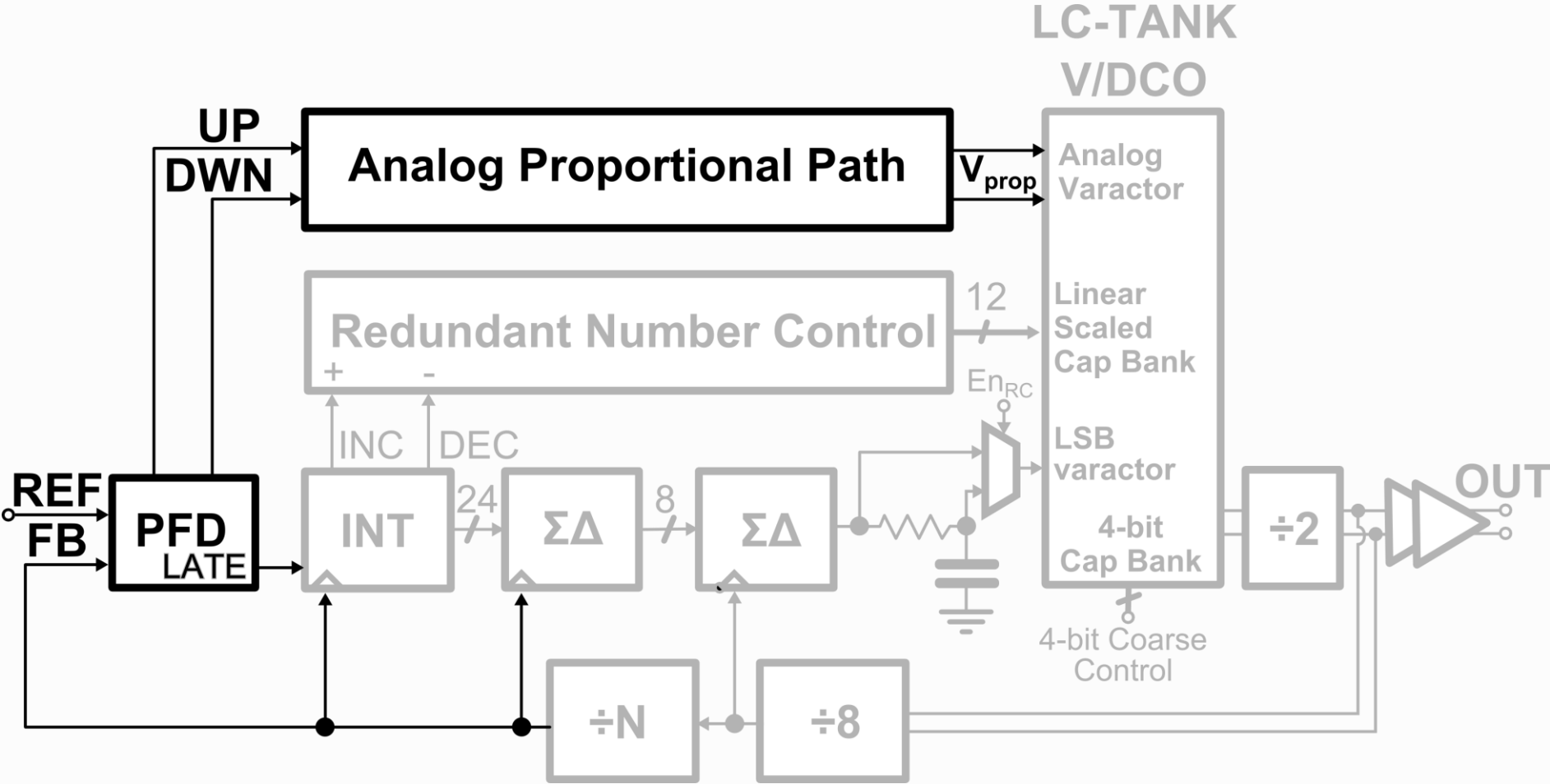
Mutex -Mutex for metastability rejection.

Hybrid PLL Approach: Single PFD with two sets of outputs

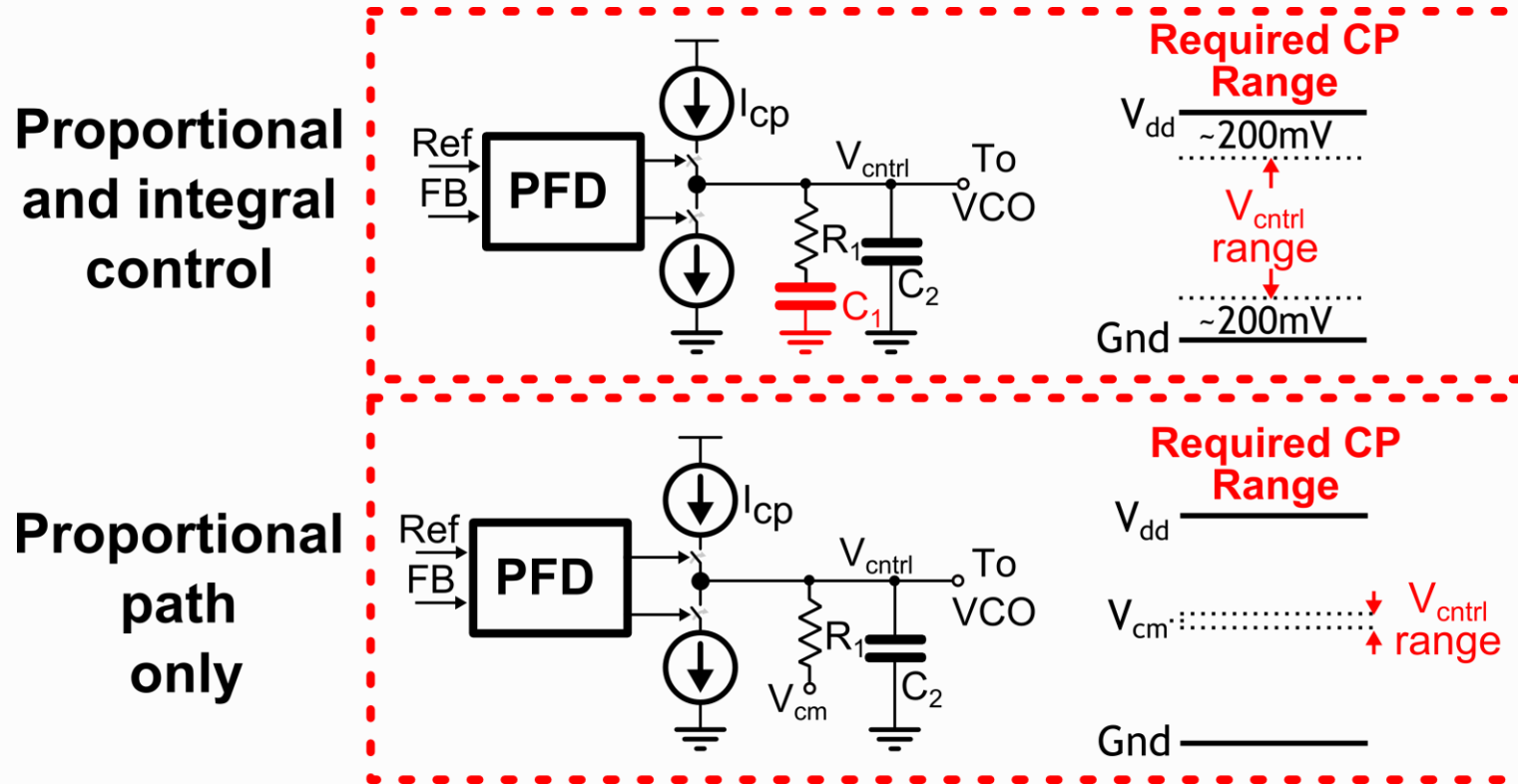


- Offset of input latches is common to both paths
- Digital discriminator takes time to resolve - similar to delay path in tri-state PFD

Analog proportional path



Dual path architecture enables proportional path simplification



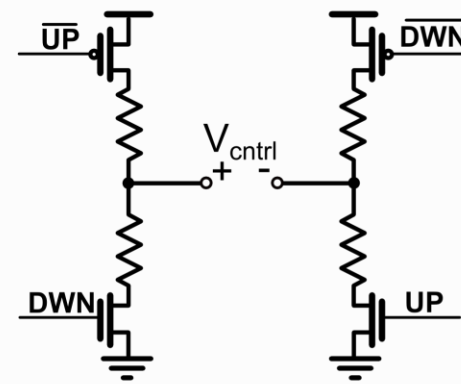
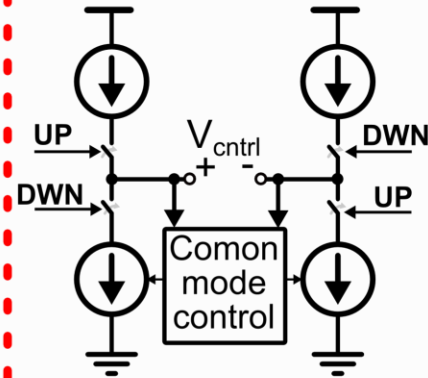
- **Proportional/Integral control path** operates over large voltage range → requires charge pump to operate across wide voltage range
- **Proportional path** stays close to common-mode (once PLL is locked) → relaxes charge pump performance requirements

Proportional path simplifications enabled by dual path architecture

Conventional Analog

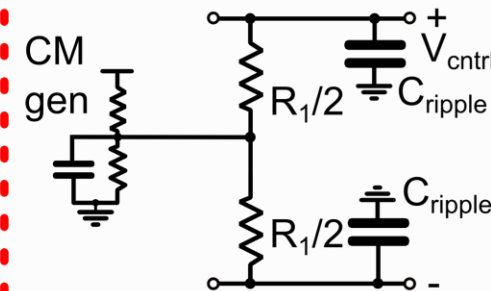
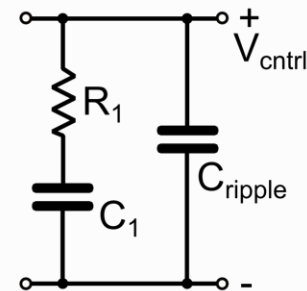
Simplified Analog

Differential charge pump



Simplified switched resistor scheme

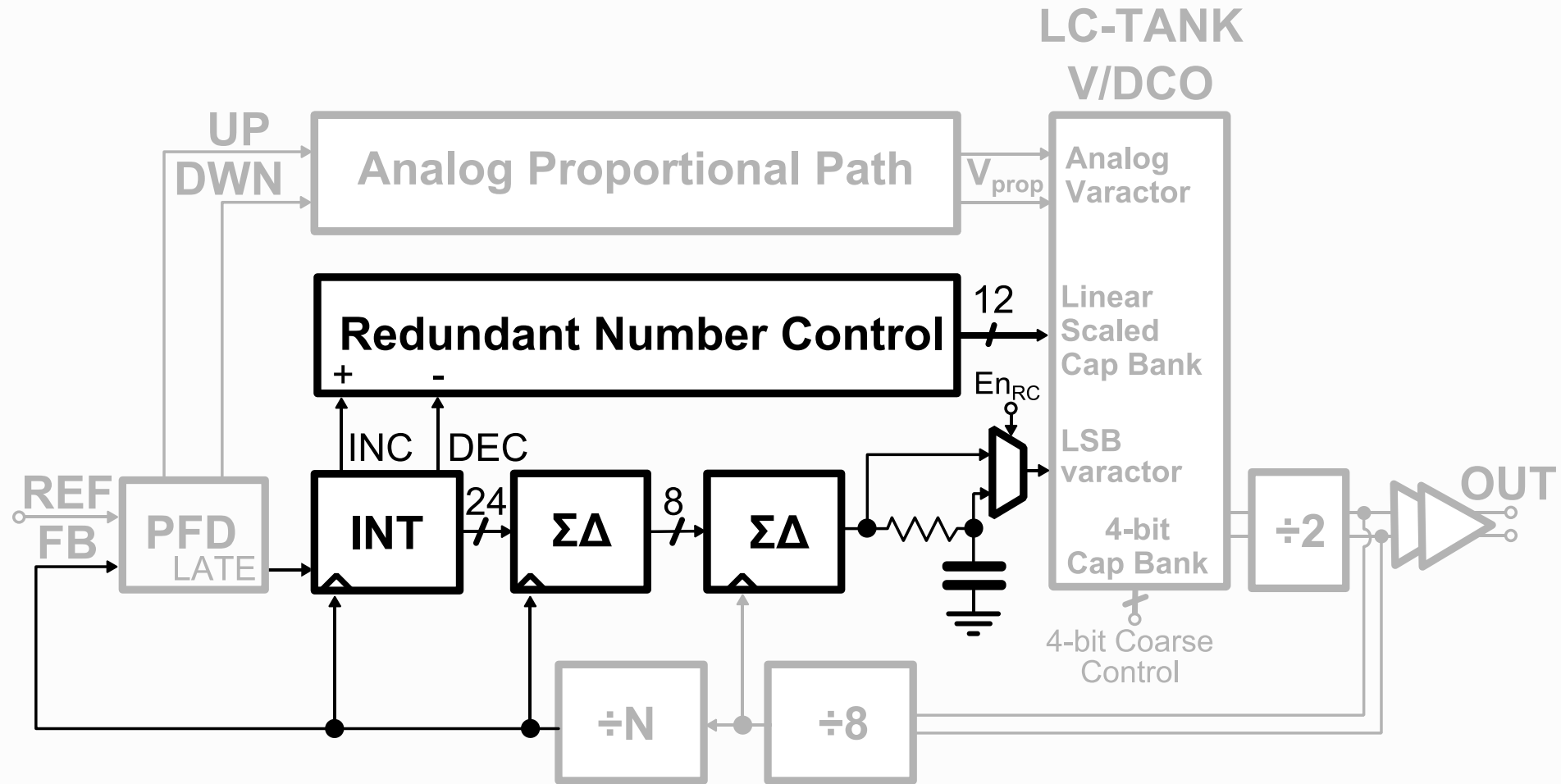
Prop/Int differential loop filter



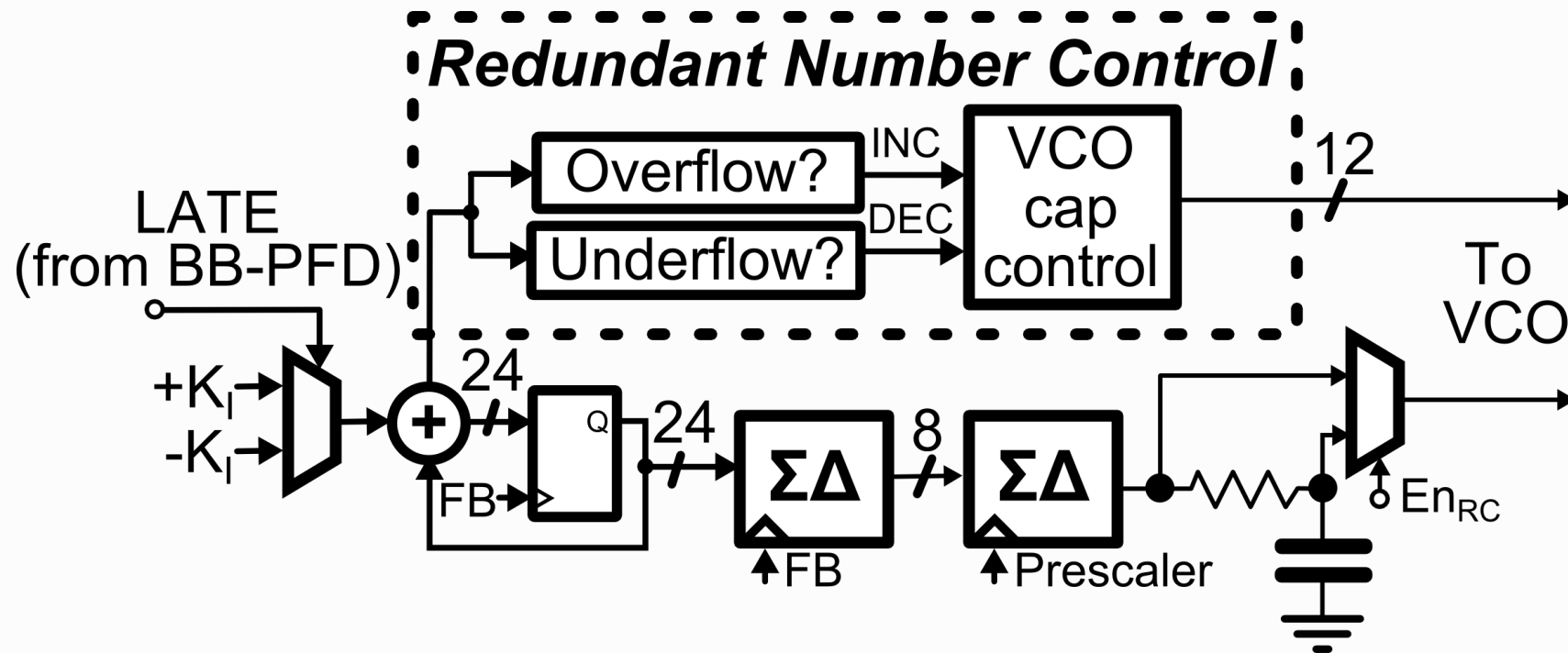
Proportional differential loop filter

- Switched resistor scheme has lower flicker noise than conventional CP
- Common mode control greatly simplified

PLL integral path control



Integral path overview

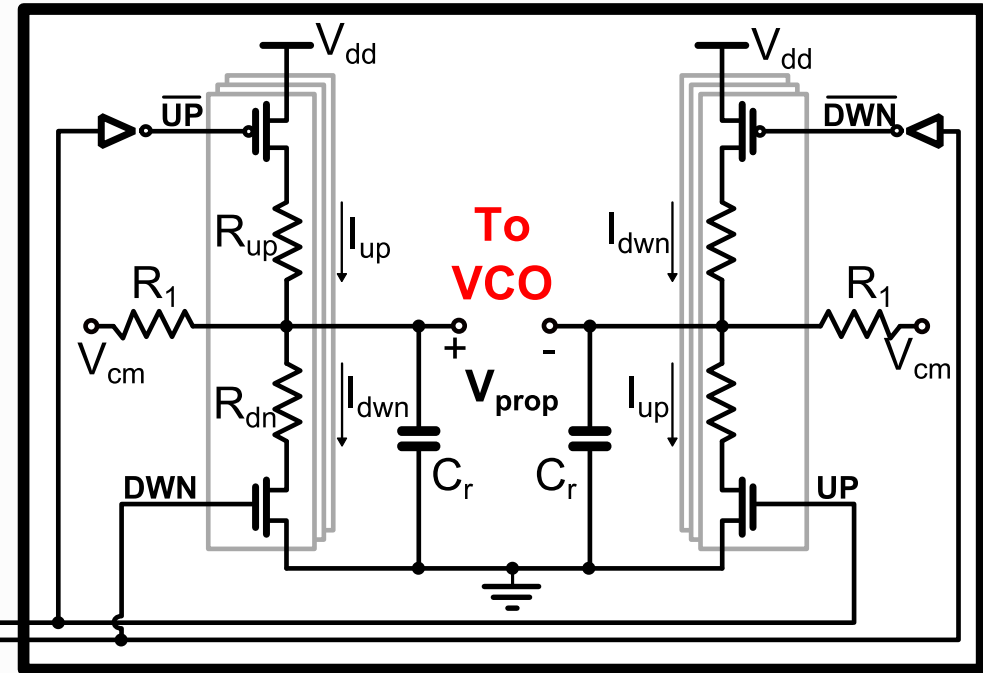
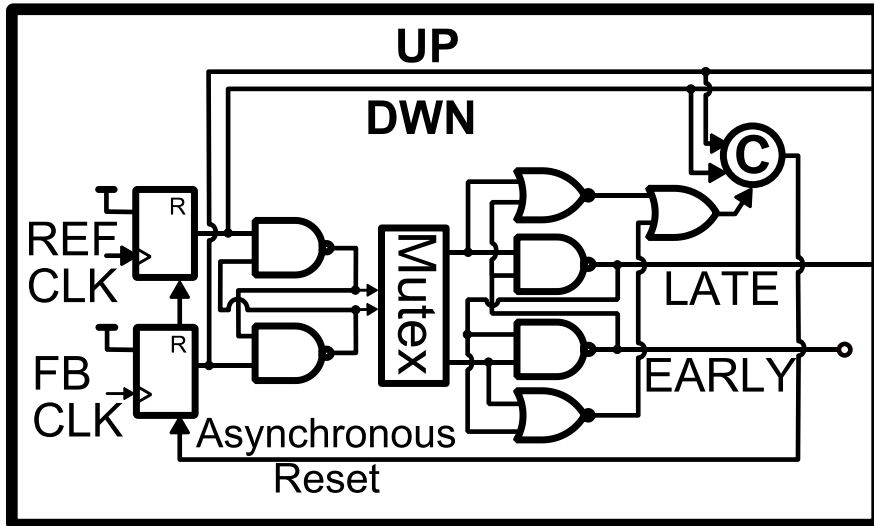


- Digital accumulator step size, K_I , programmable using serial interface
- VCO frequency control split into two paths
 - A 12-bit digitally switched capacitor bank
 - A $\Sigma\Delta$ -controlled analog varactor

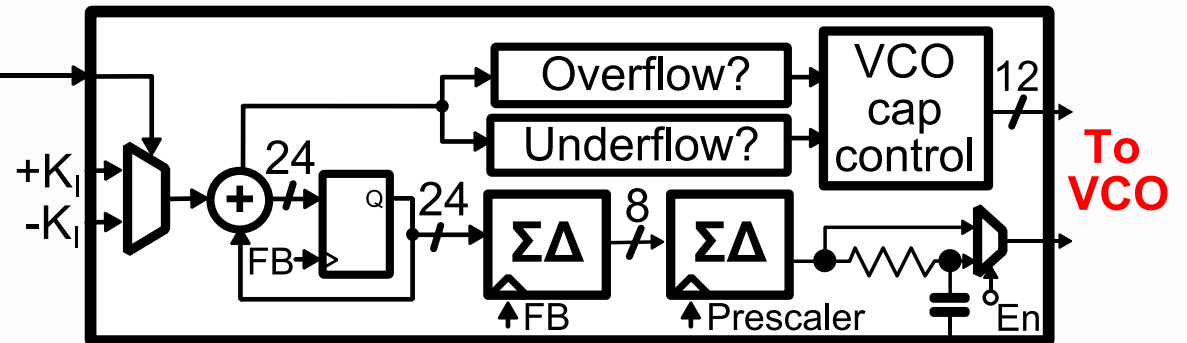
Composite hybrid PLL control path

Analog Proportional Path

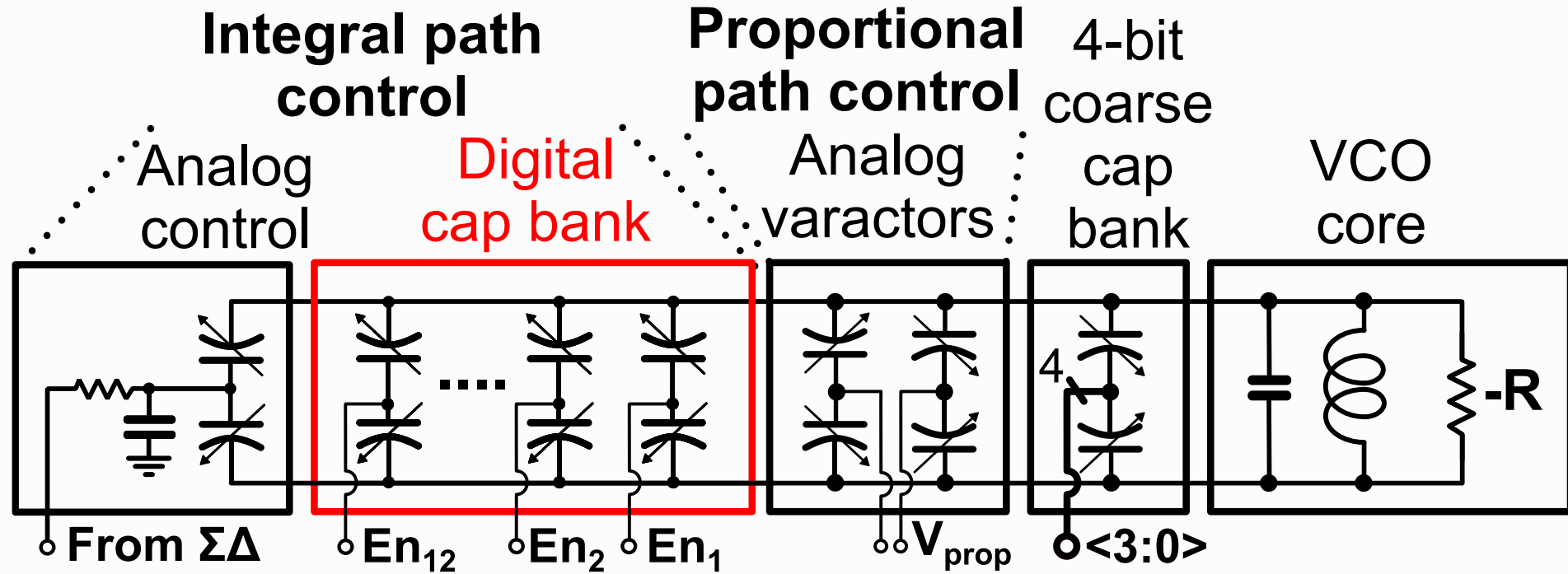
Combined Tri-State/Bang-Bang PFD



Integral Path Control



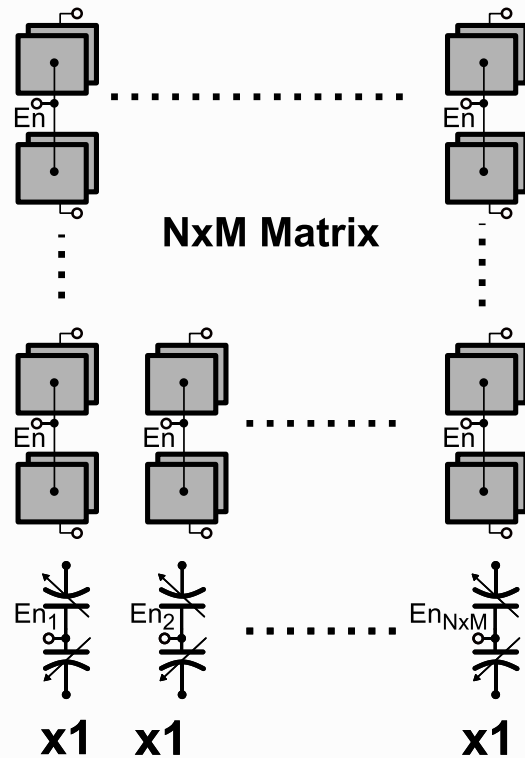
VCO conceptual diagram



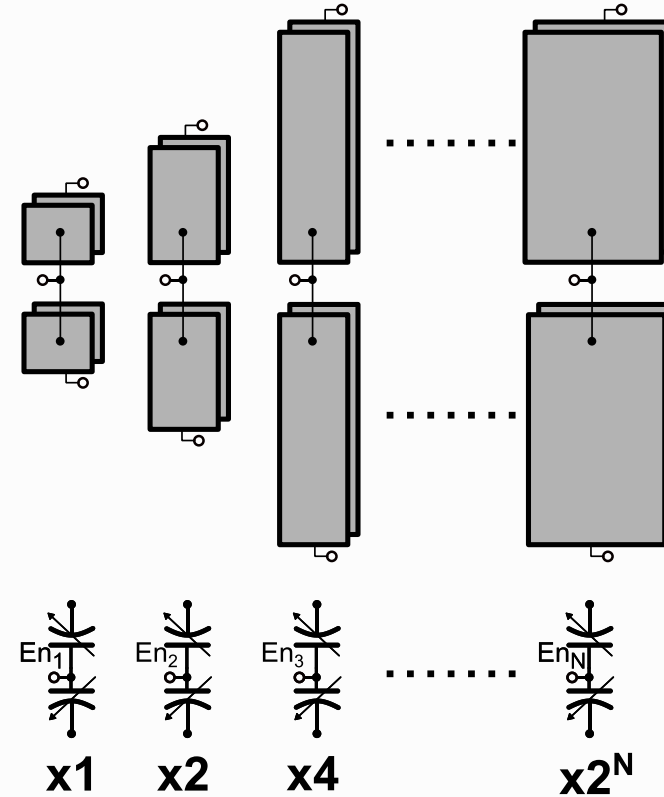
- Control of VCO comprised of a mixture of digitally switched capacitors and varactors
- Implementation strategy for integral path digital cap bank: *redundant numbering*

The VCO capacitor bank: options

Thermometer Weighted



Binary Weighted



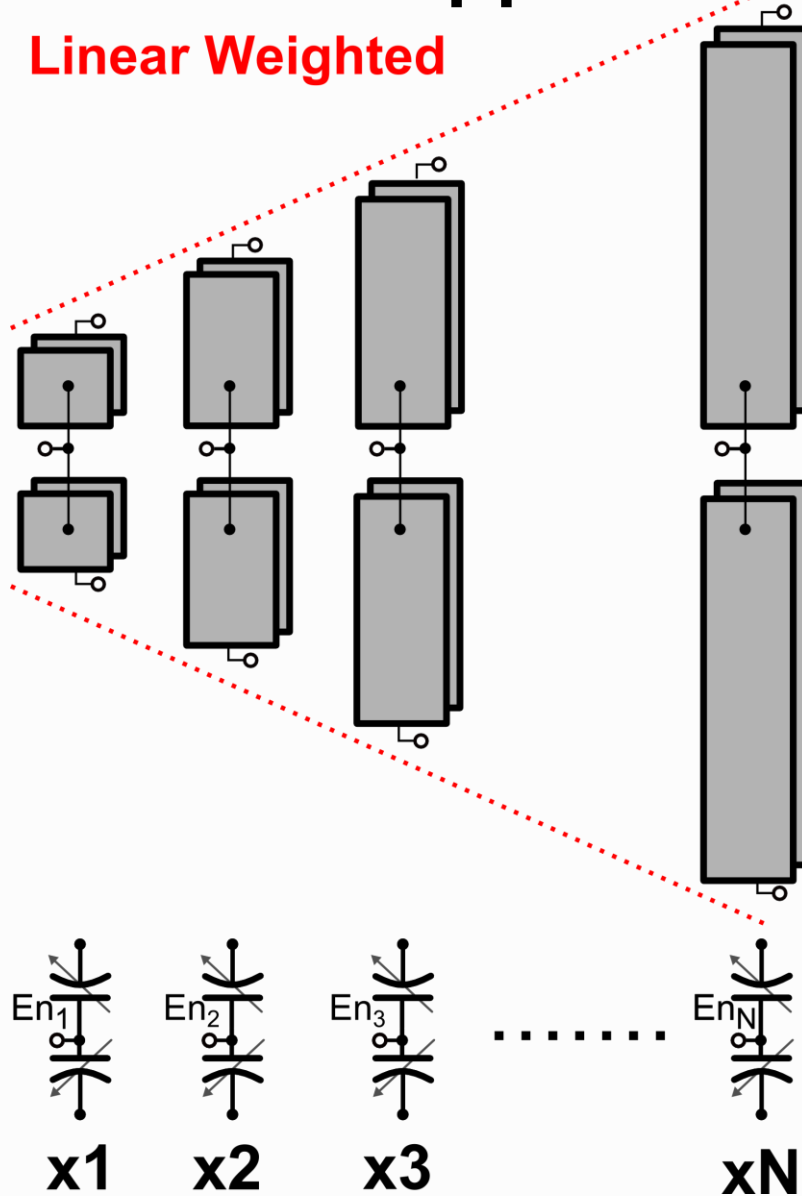
- Very large number of control lines
- Complex interconnect inductance, difficult to extract and simulate

- Stringent matching requirements
- Major code transition problem
 - 01111 \rightarrow 10000

Is there a better way?

Chosen approach: redundant numbering

Linear Weighted



- Fewer control lines than thermometer weighted
- Matching requirements easier than binary
- Many capacitor configurations can result in the same total capacitance: *scheme is redundant*
- Major code transitions can be avoided by utilizing redundancy

Integral path digital control options

<i>Coding Scheme</i>	Redundant numbering	Thermometer	Binary
<i>Steps</i>	78	78	64-128
<i>Control wires</i>	12	78	6-7
<i>Matching requirements</i>	moderate	trivial	extreme
<i>Simultaneous switching events per inc/dec</i>	2	1	Up to 7 1000000→0111111

Redundant numbering based capacitor bank

→ Fewer switching events than binary

→ Fewer control lines than thermometer

Switching sequence example

Example Control Sequence

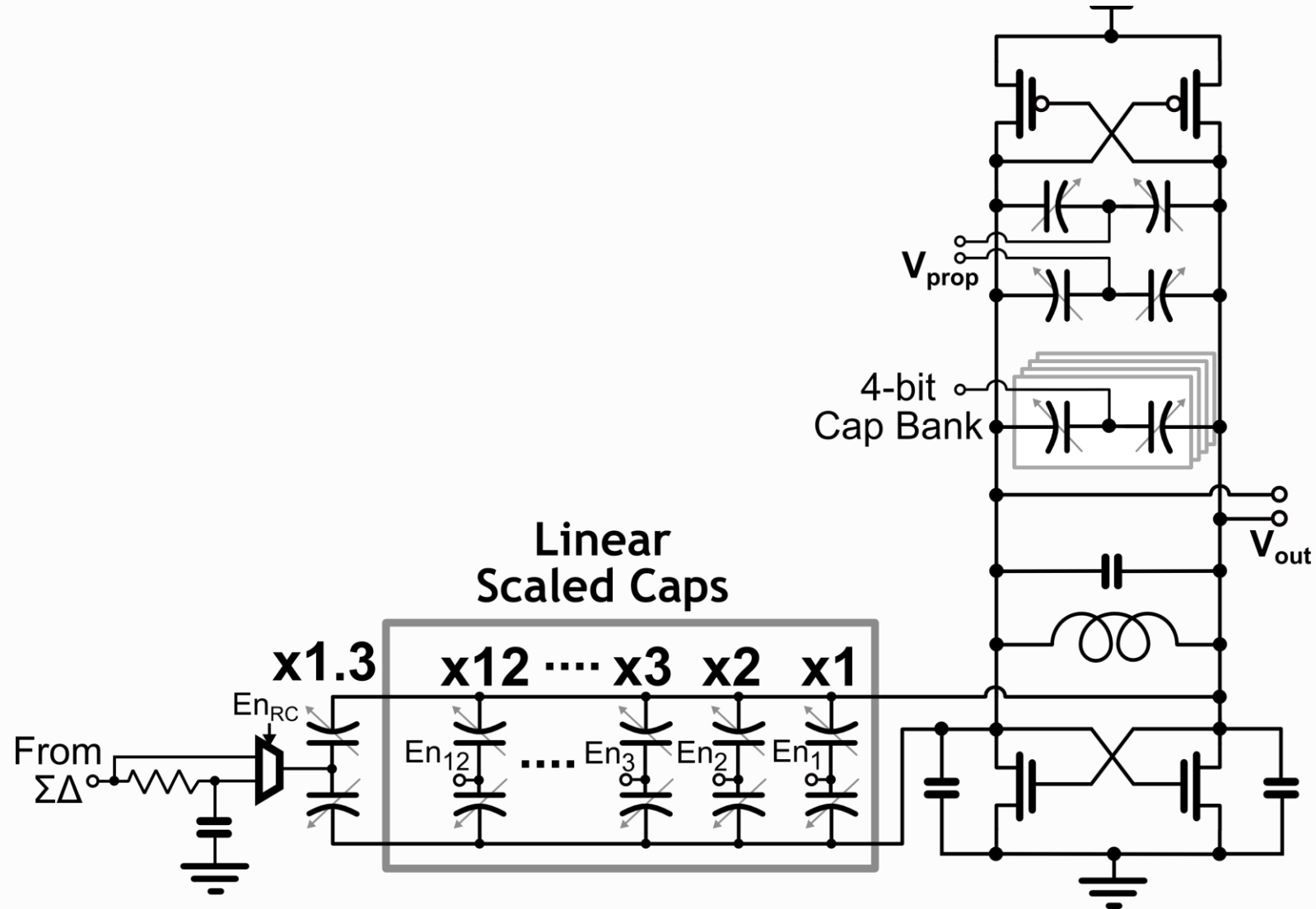
INC/ DEC	Capacitor Control	Net Capacitance	Simultaneous switching events
	Weight 12, ,4,3,2,1		
+INC	0000 0000 0001	$C+1\Delta C$	
+INC	0000 0000 0010	$C+2\Delta C$	2
+INC	0000 0000 0011	$C+3\Delta C$	1
+INC	0000 0000 0101	$C+4\Delta C$	2
+INC	0000 0000 0110	$C+5\Delta C$	2
+INC	0000 0000 0111	$C+6\Delta C$	1
+INC	0000 0000 1011	$C+7\Delta C$	2
-DEC	0000 0000 1010	$C+6\Delta C$	1
-DEC	0000 0000 1001	$C+5\Delta C$	1

Different configurations
produce the same net capacitance

We can increment or decrement with at most 2 capacitor changes → mitigates major code transition problem

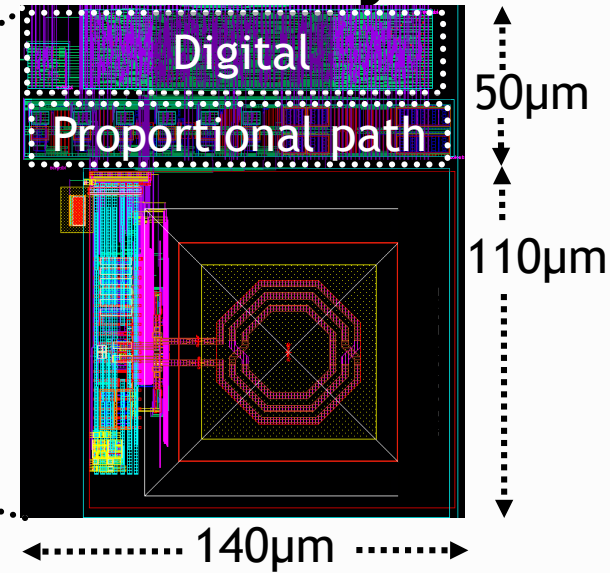
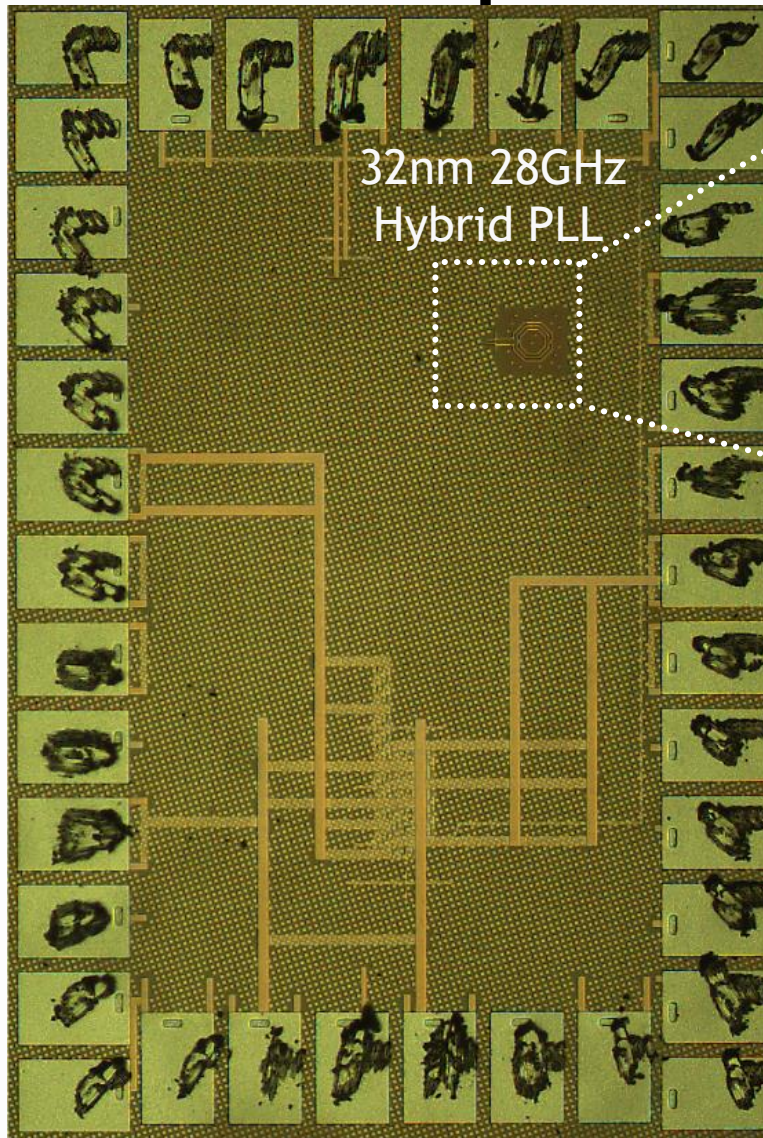
... *But transition problem remains—better solutions described later in talk*

VCO schematic view



$\Sigma\Delta$ path varactor oversized to prevent gaps in tuning range

Die microphotograph, physical design, and performance summary

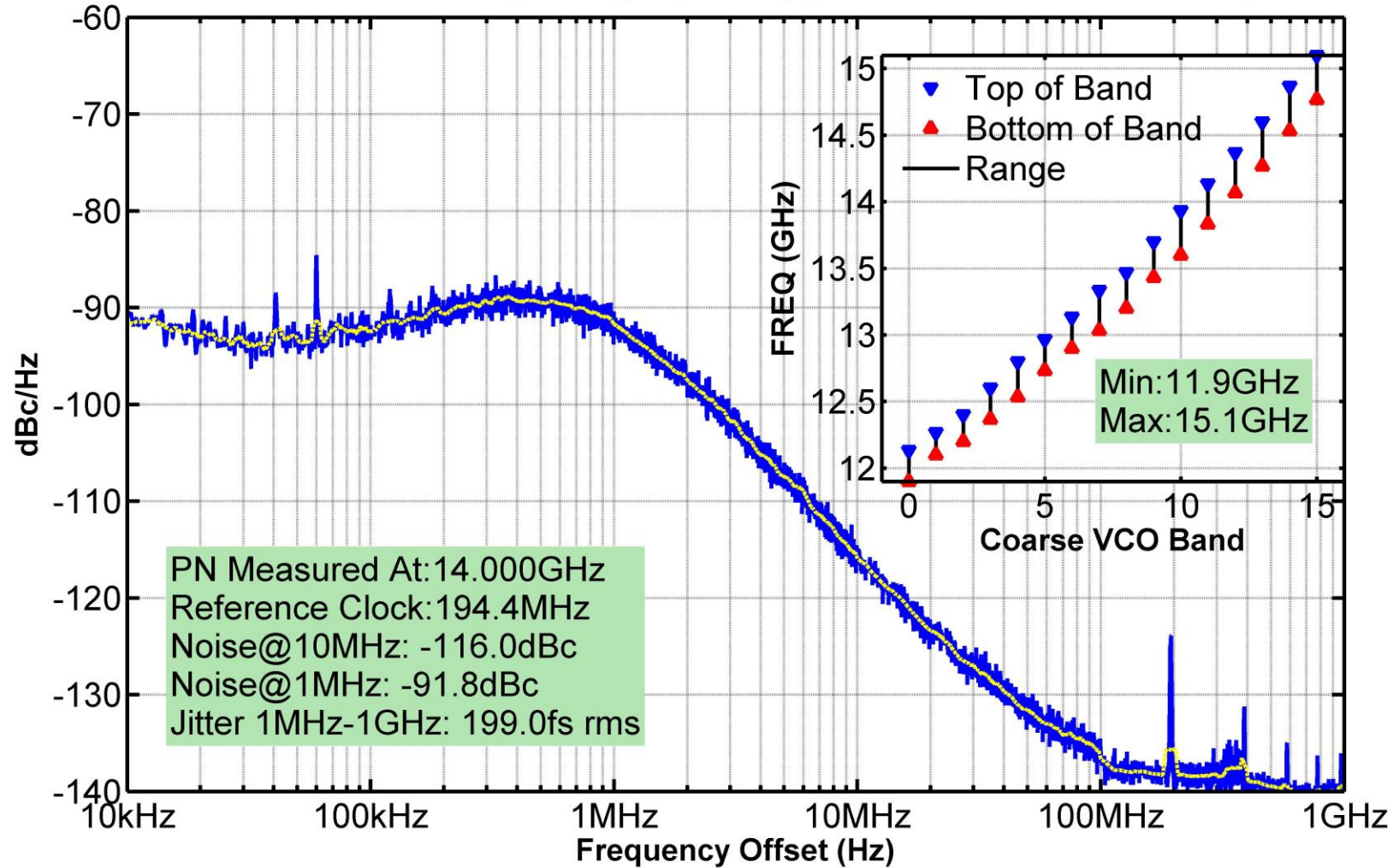


Performance Summary

Area (32nm CMOS)	0.0225mm ²
Power	31mW from 1V
Frequency range	23.8-30.2GHz
Phase noise @10MHz	-110dBc/Hz
Phase noise @1MHz	-86dBc/Hz*

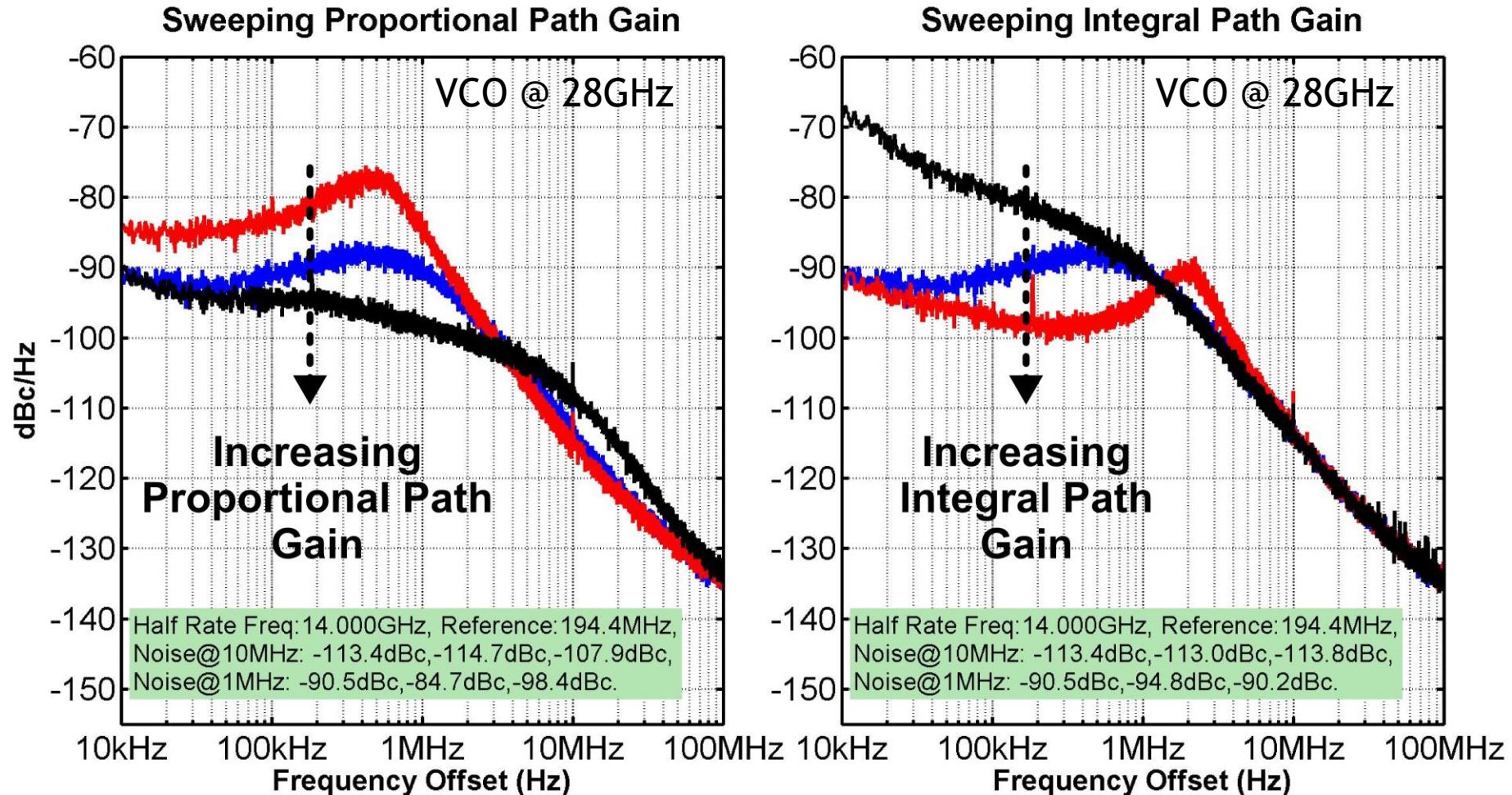
*Varies with bandwidth

PLL phase noise at 28GHz and VCO tuning range (inset) [measured at half rate]



For equivalent full rate phase noise, add 6dB
[-110dBc/Hz @10MHz from 28GHz]

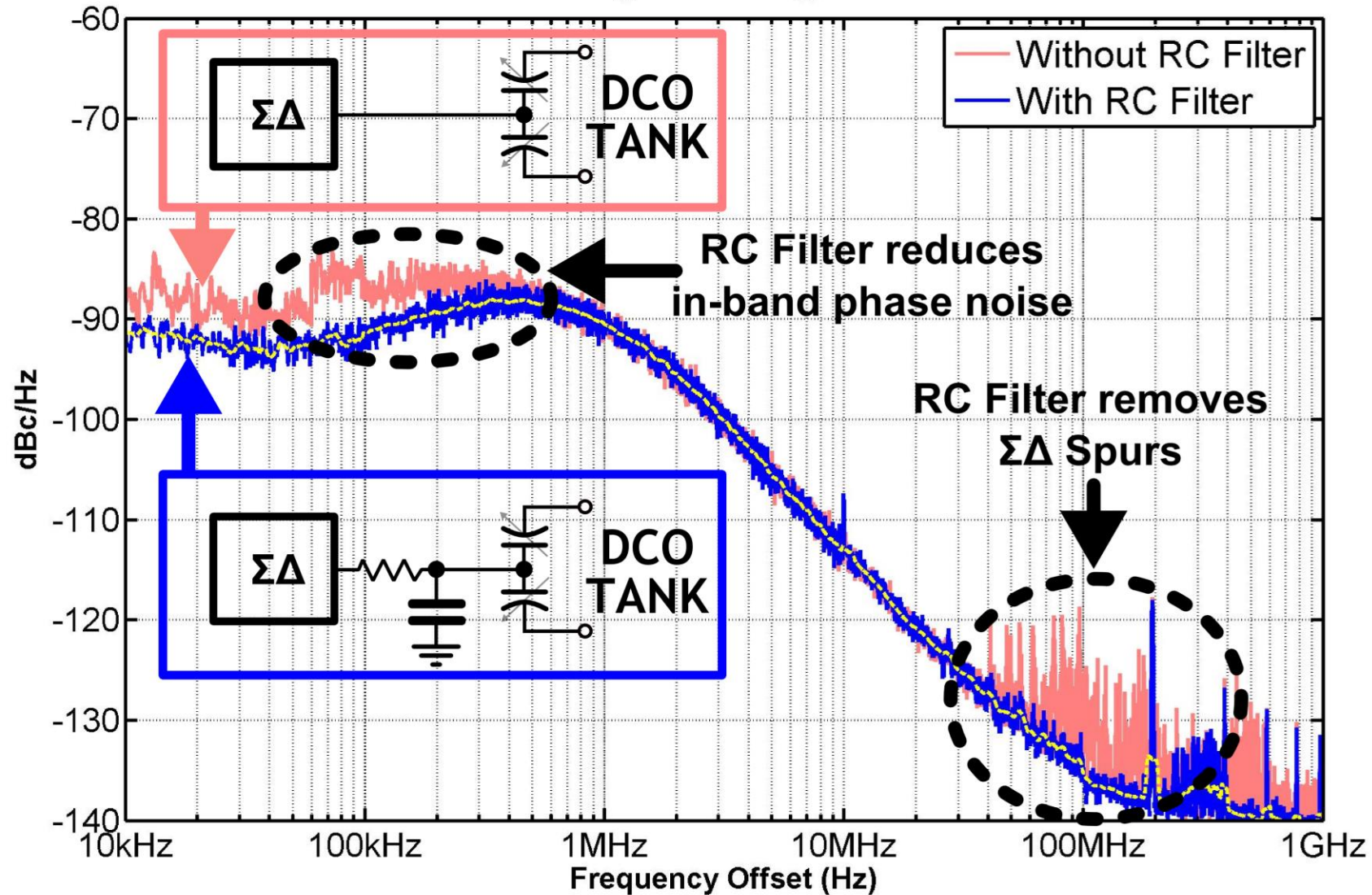
Demonstration of independent control of proportional and integral path gains



Hybrid PLL responds to changes in proportional/integral path gains in a similar fashion as a dual path analog PLL

Measured effects of RC filter on $\Sigma\Delta$ output

Filtering the Integral Path



Conclusion: Initial High Performance Hybrid PLL Implementation

Key results

- A 28GHz, low noise hybrid PLL drawing 31mW from 1V demonstrated in 32nm CMOS
- Compact, digital friendly implementation comparable to that of digital PLL achieved
- Linear phase response and spurious spectral content similar to that of all analog PLL achieved

Challenges

- Integral path redundant numbering implementation still problematic
- Does not really exploit opportunities presented by hybrid architecture

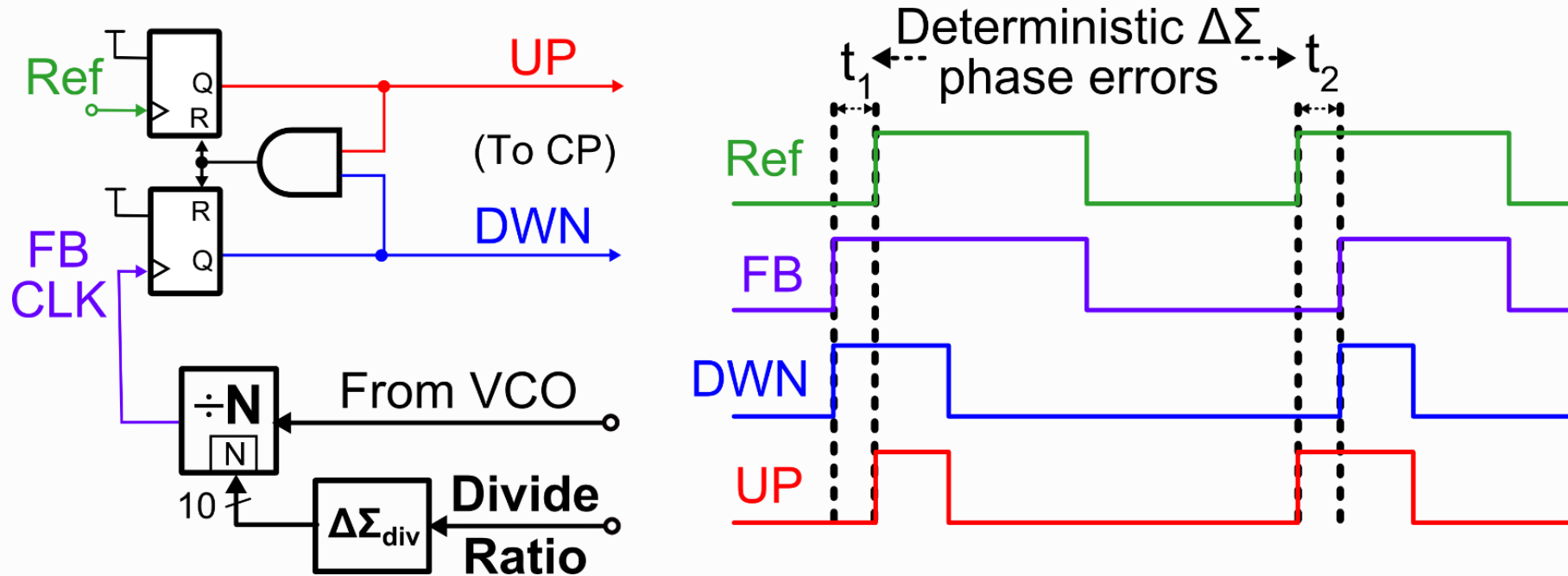
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Fractional-N Hybrid PLL

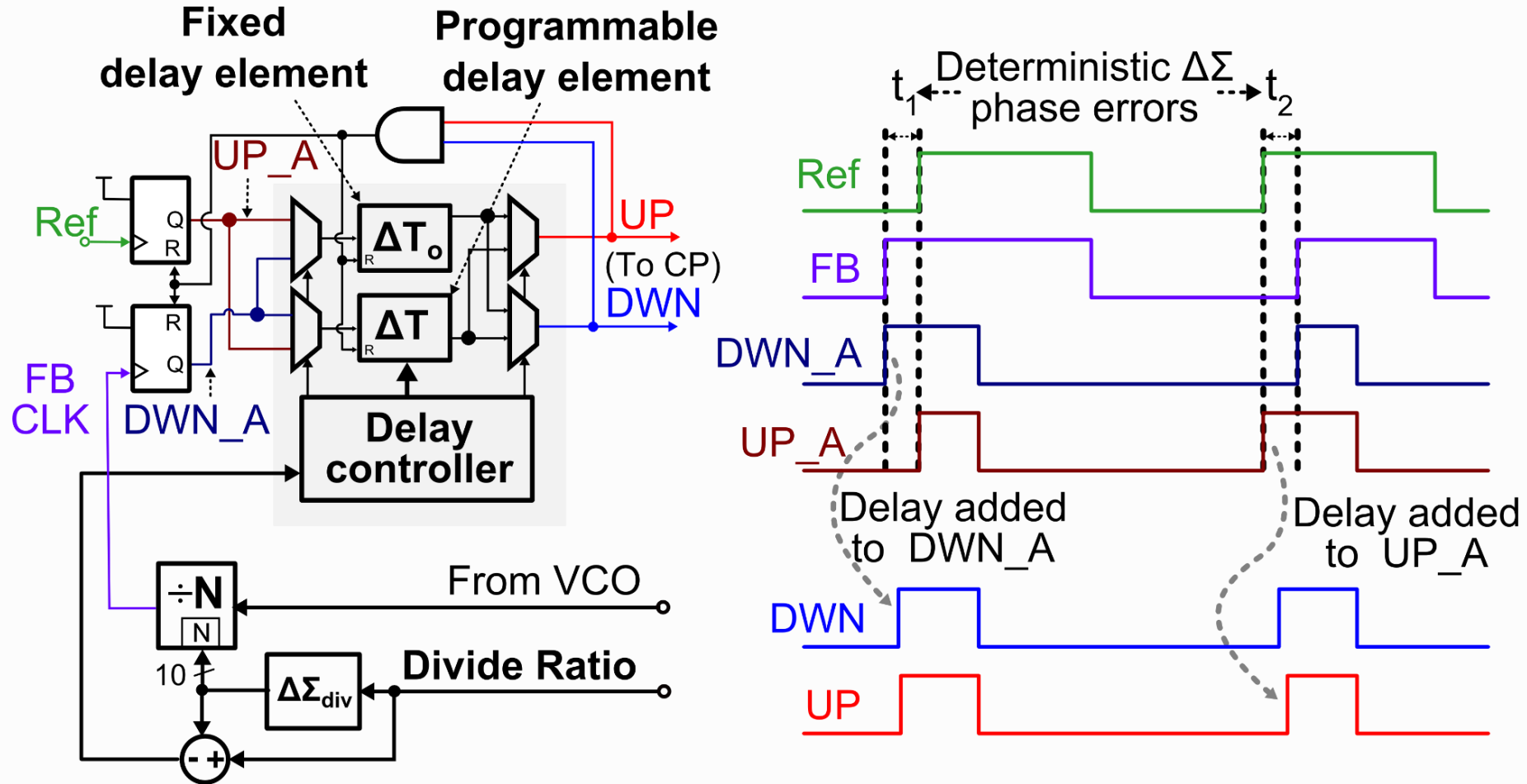
- Objective: demonstrate frac-N synthesizer with integrated noise cancellation compatible with hybrid PLL architecture, and demonstrate new features enabled by the architecture
- Approach
 - Introduce proportional path digital-to-time conversion infrastructure
 - Introduce integral path scale/ignore infrastructure
 - Explore use of replay to support fast hopping
- Key challenges
 - Introduction of new elements
 - Support background calibration of digital-to-time converter

Classic $\Delta\Sigma$ Problem



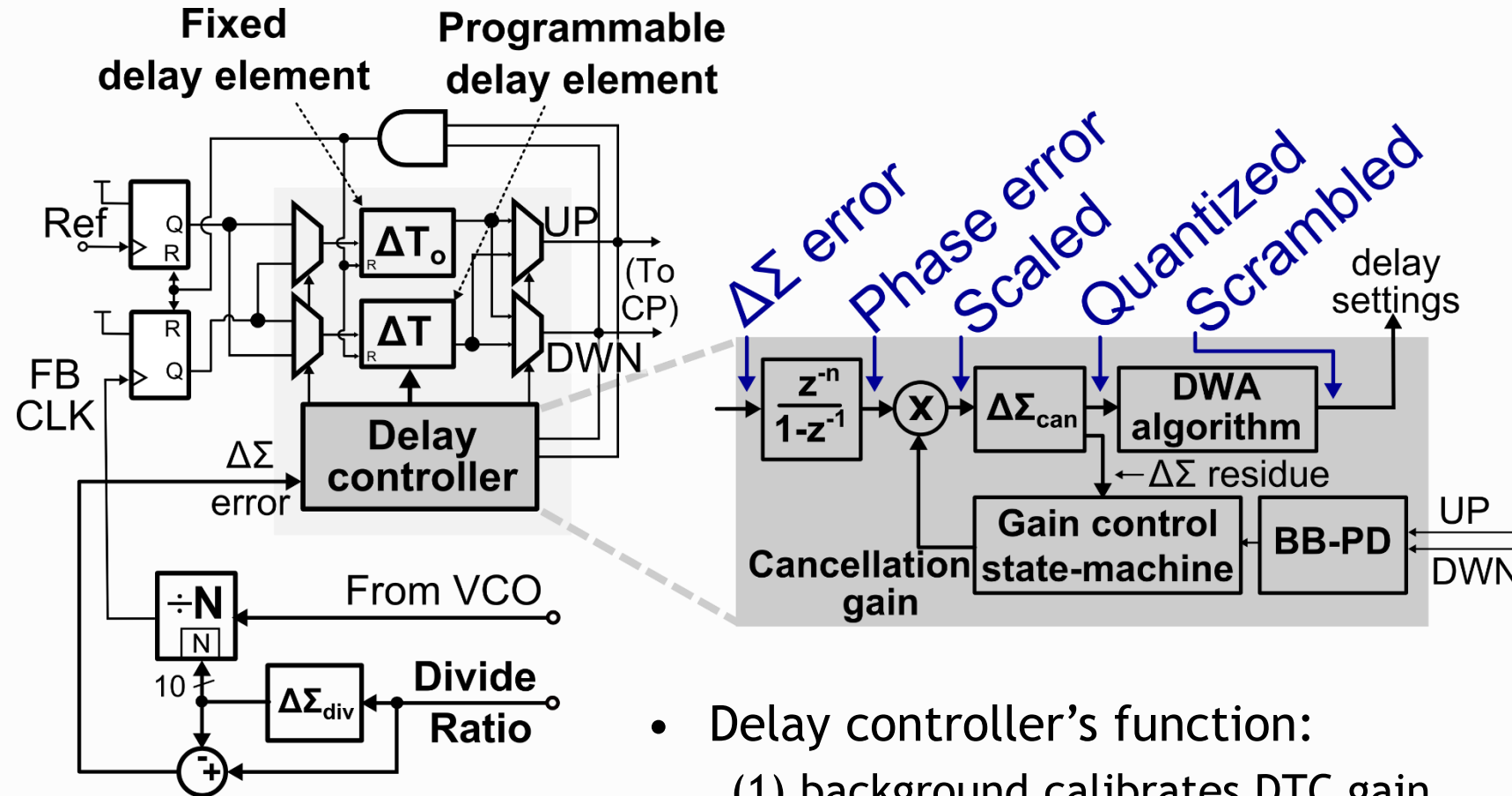
- Divider's $\Delta\Sigma$ dithers PLL's feedback (FB) clock
- $\Delta\Sigma$ noise contributes to PLL's phase noise

Time-based Cancellation Concept



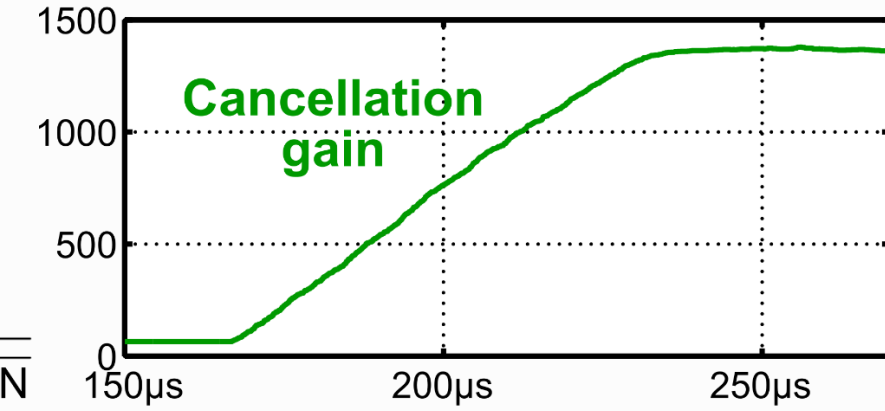
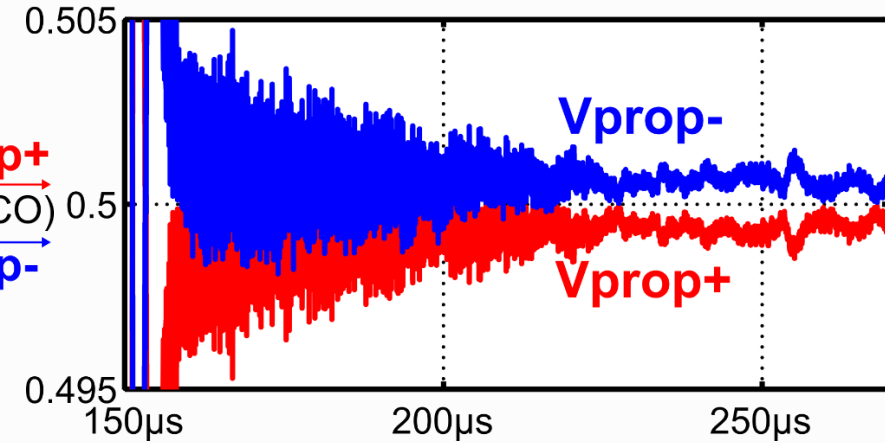
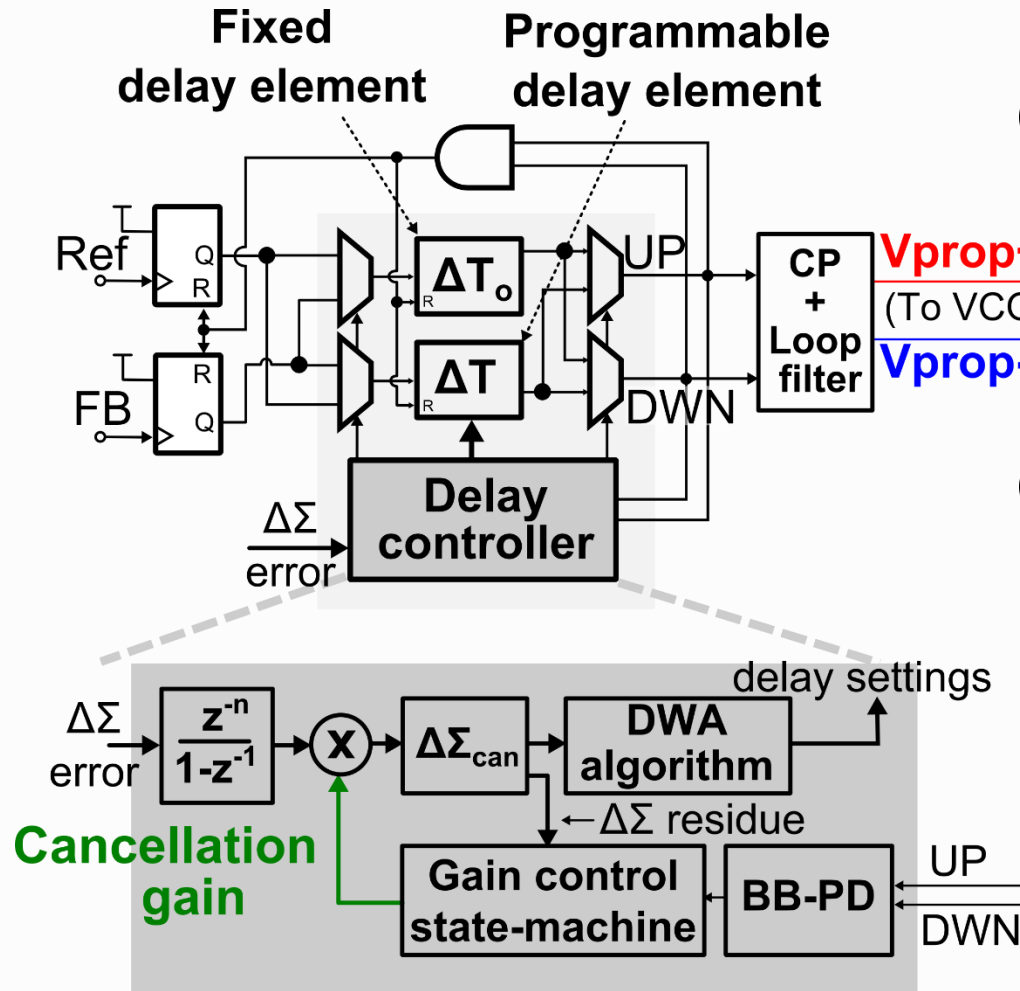
- Digital-to-time based delay scheme used *on analog path*
 - Utilizes loop filter's low pass response to remove delay path quantization noise \rightarrow do not need fine quantization step.

Delay Controller Architecture

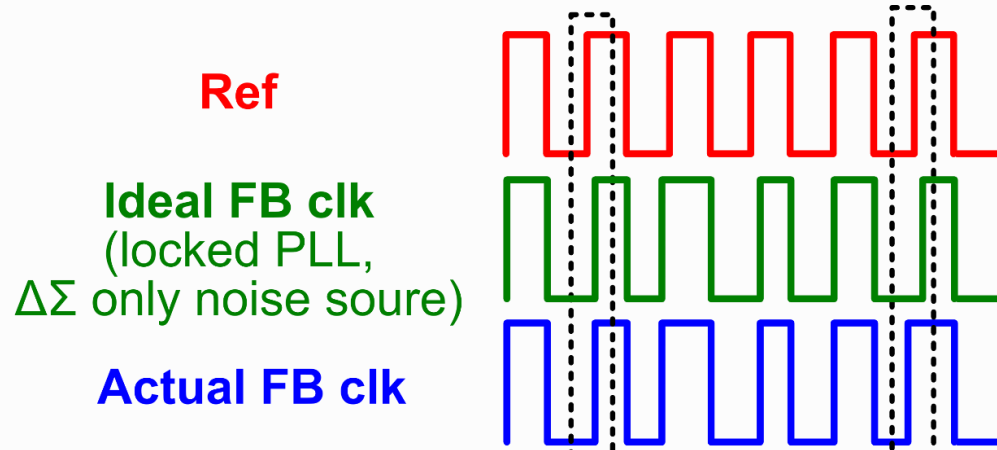


- Delay controller's function:
 - (1) background calibrates DTC gain
 - (2) shapes ΔT quantization error
 - (3) scrambles mismatch error

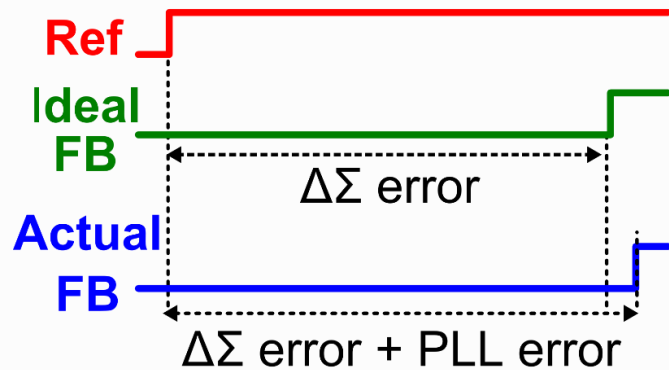
Delay Controller Operation Simulation



Integral Path Prediction Concept

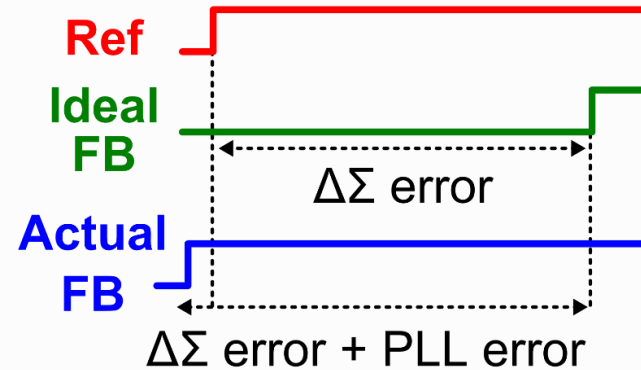


Case 1: IGNORE
Early/Late = prediction



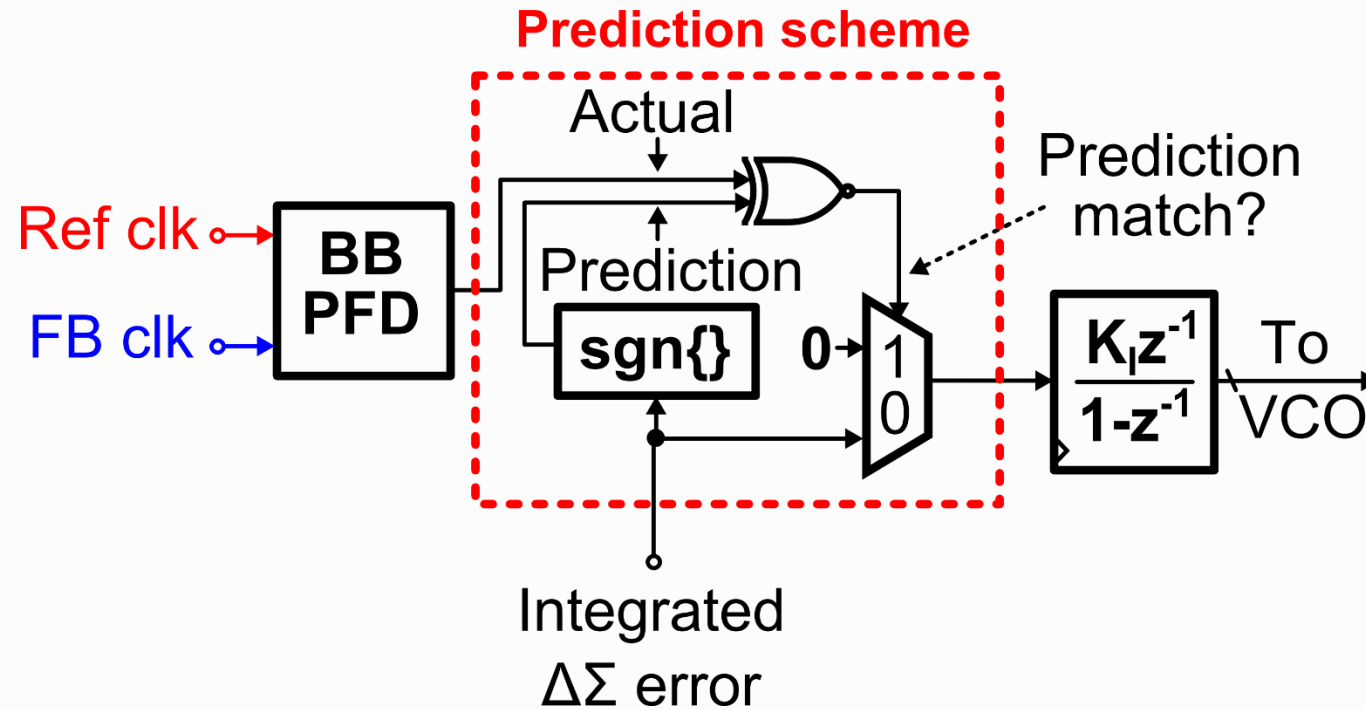
No phase error detected

Case 2: SCALE
Early/Late \neq prediction



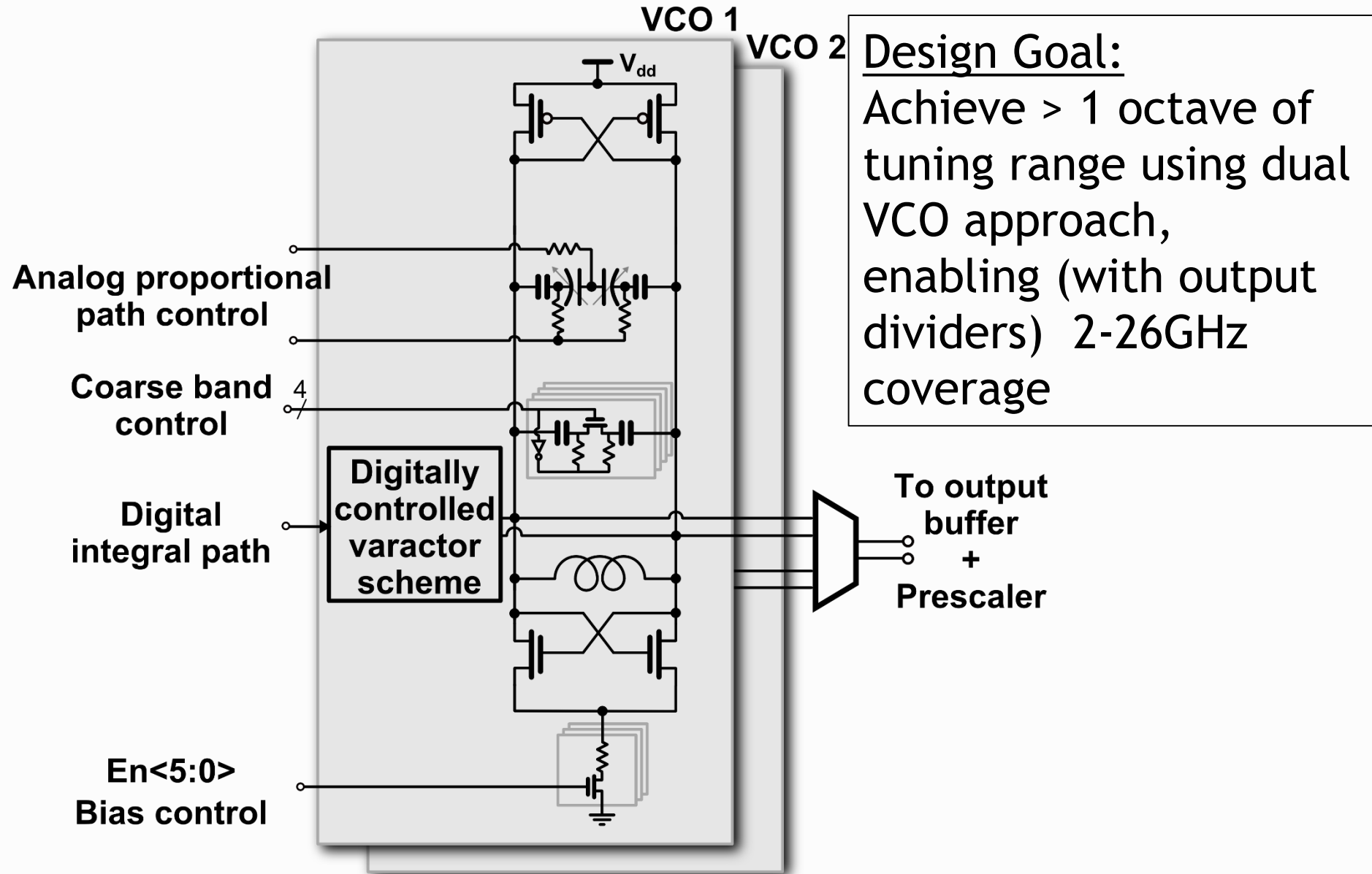
Phase error $\geq \Delta\Sigma$ error

Integral Path Prediction Circuit



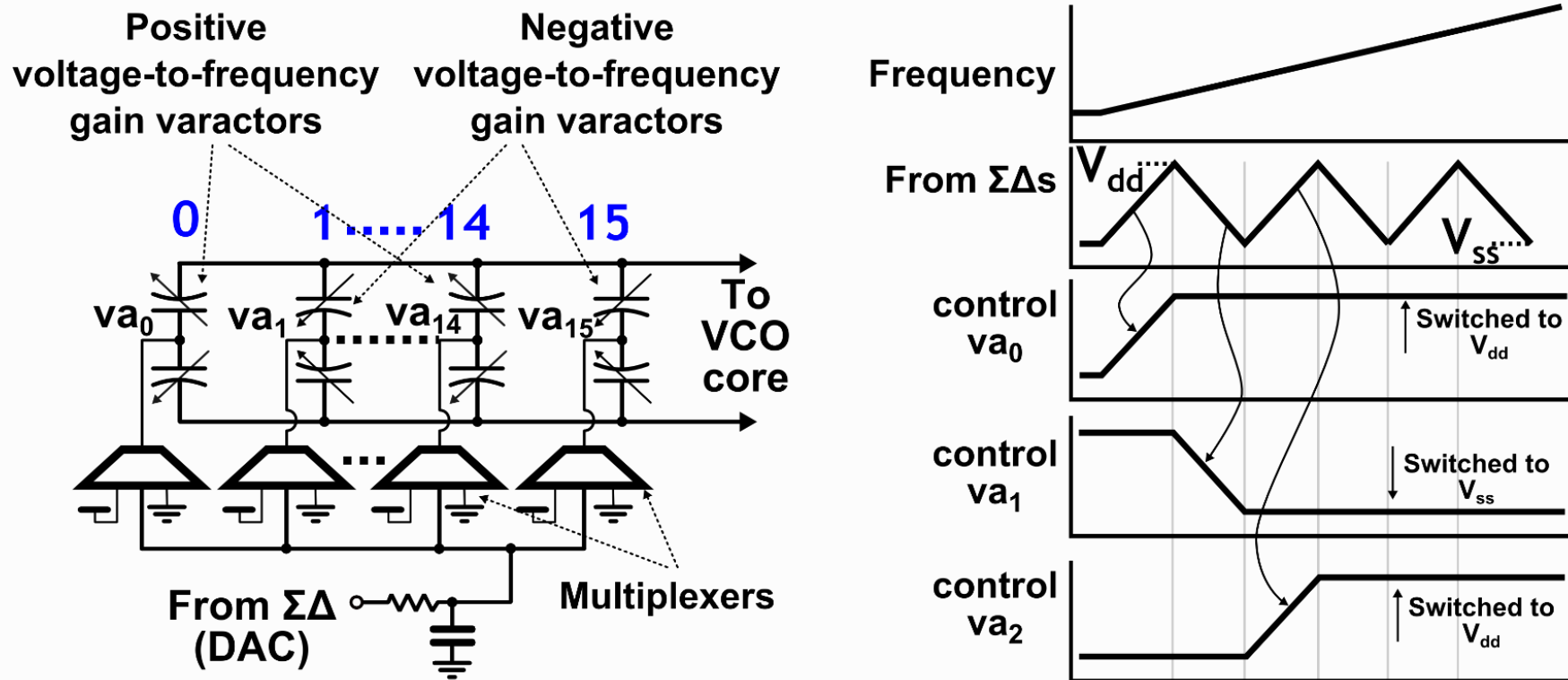
- Integral path operates from single BB phase detector
 - Works in parallel with the analog proportional path
- Ignores BB results that match prediction

Dual D/VCO Scheme



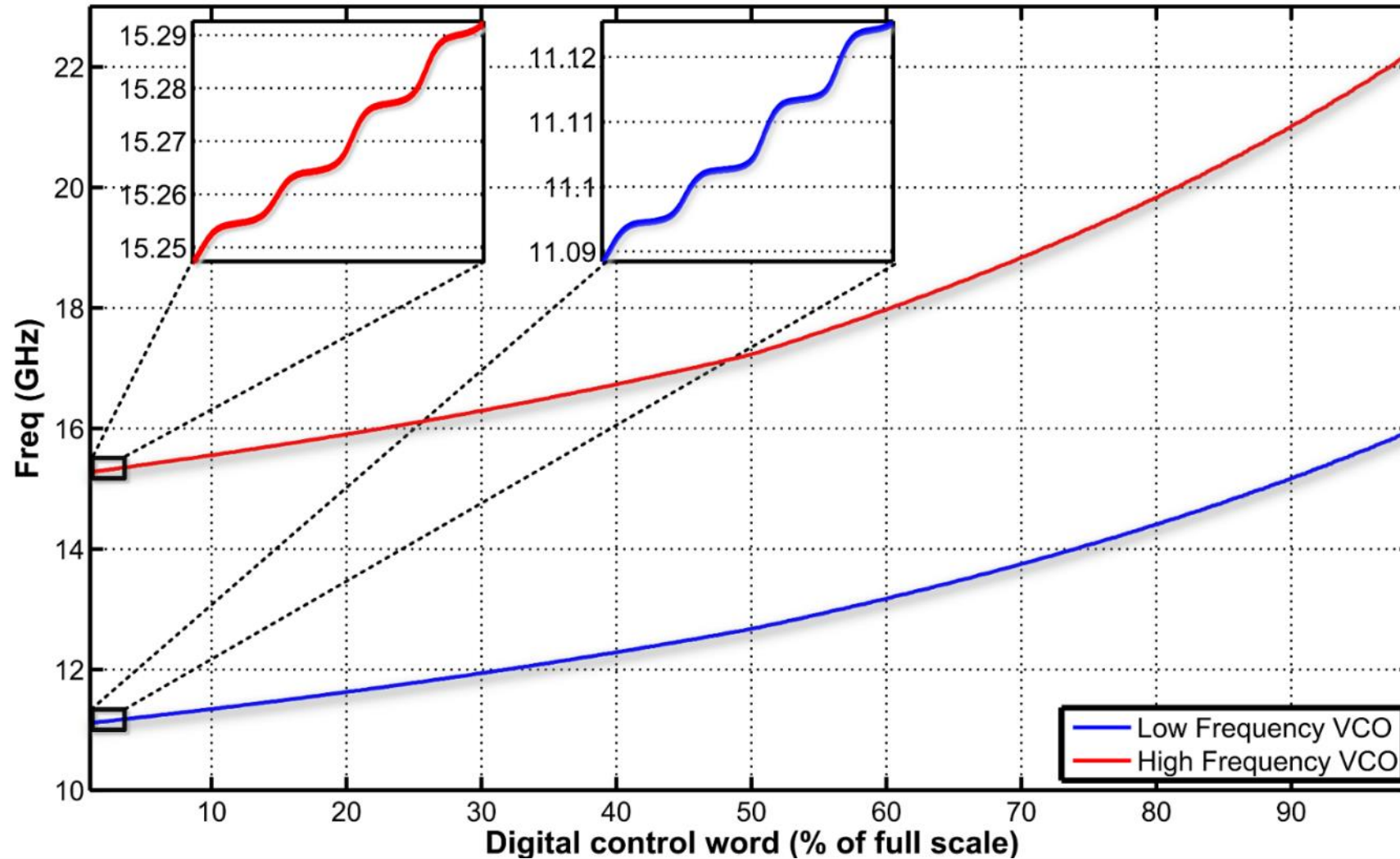
Improving the Integral Path: Introduction to Varactor Folding

Objective: address disturbance that occurs in previous implementation's redundant numbering control scheme during digital switching

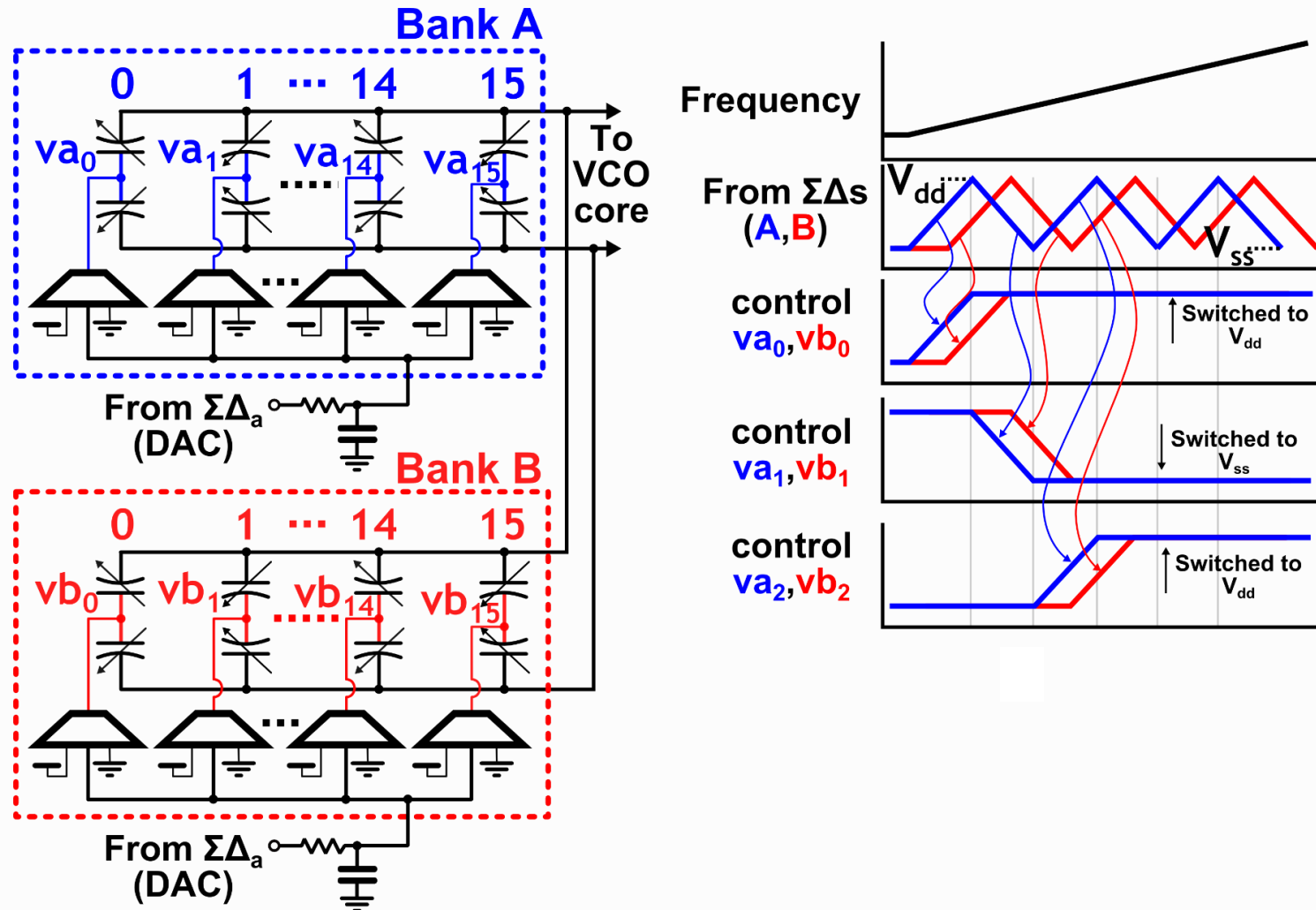


Similar concept used in P. Wang, et al., JSSC 2009
IBM Research - IEEE SSCS DL

VCO Linearization Challenge

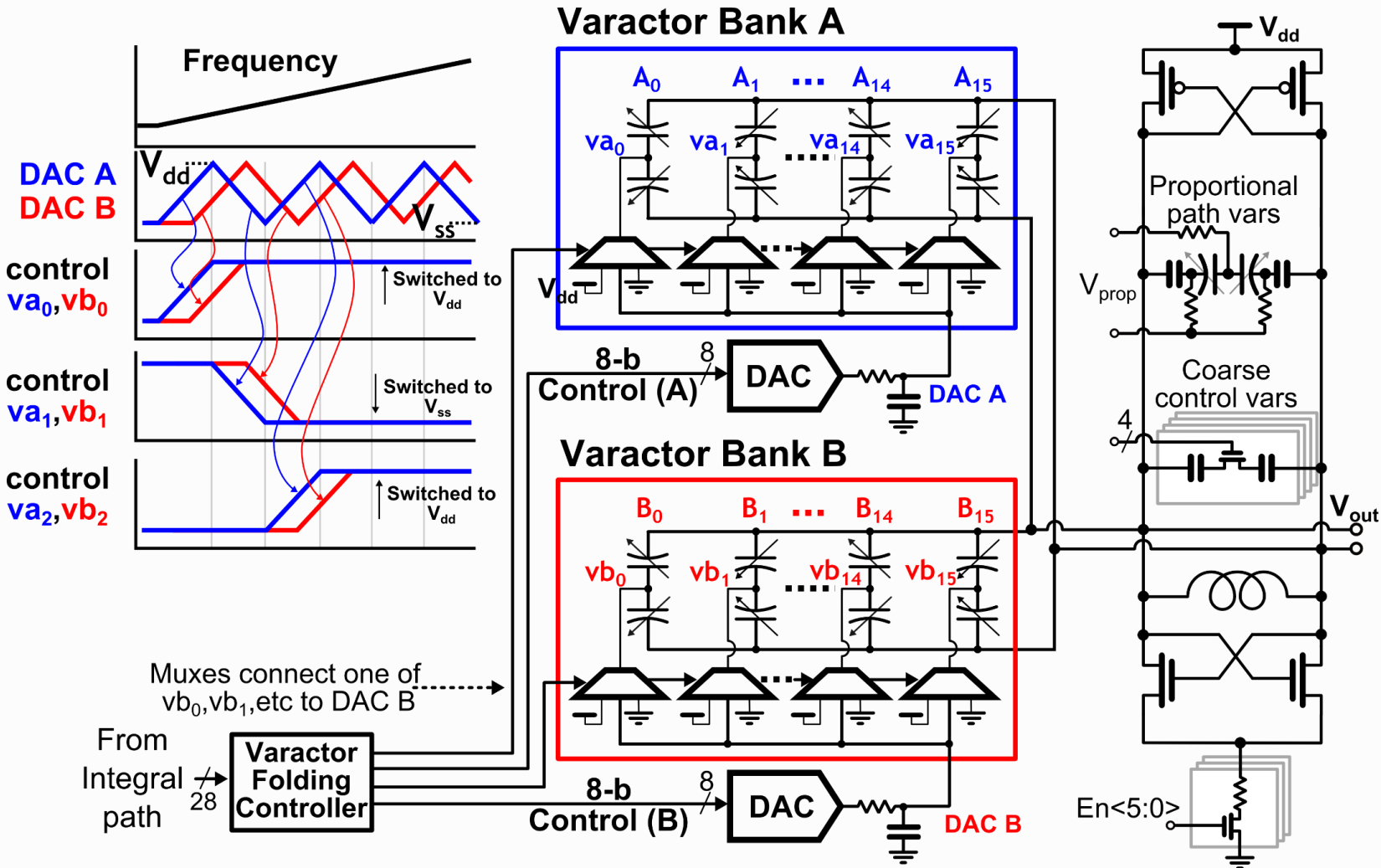


Linearization in the Varactor Folding Design

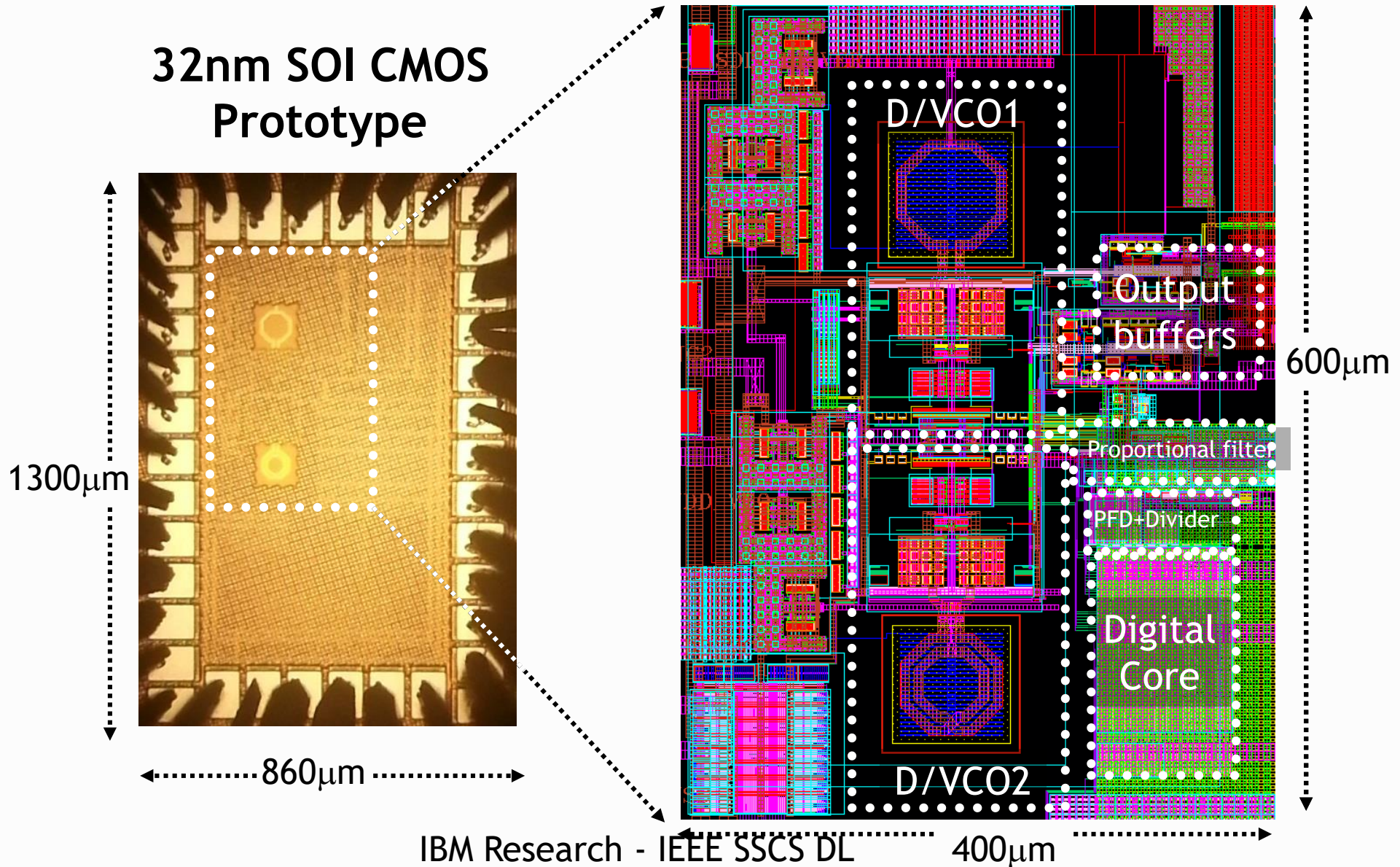


Concept: Introduce two parallel paths with offset control vectors that are combined in the D/VCO; the resulting transfer characteristic is a combination of the offset banks yielding linearization

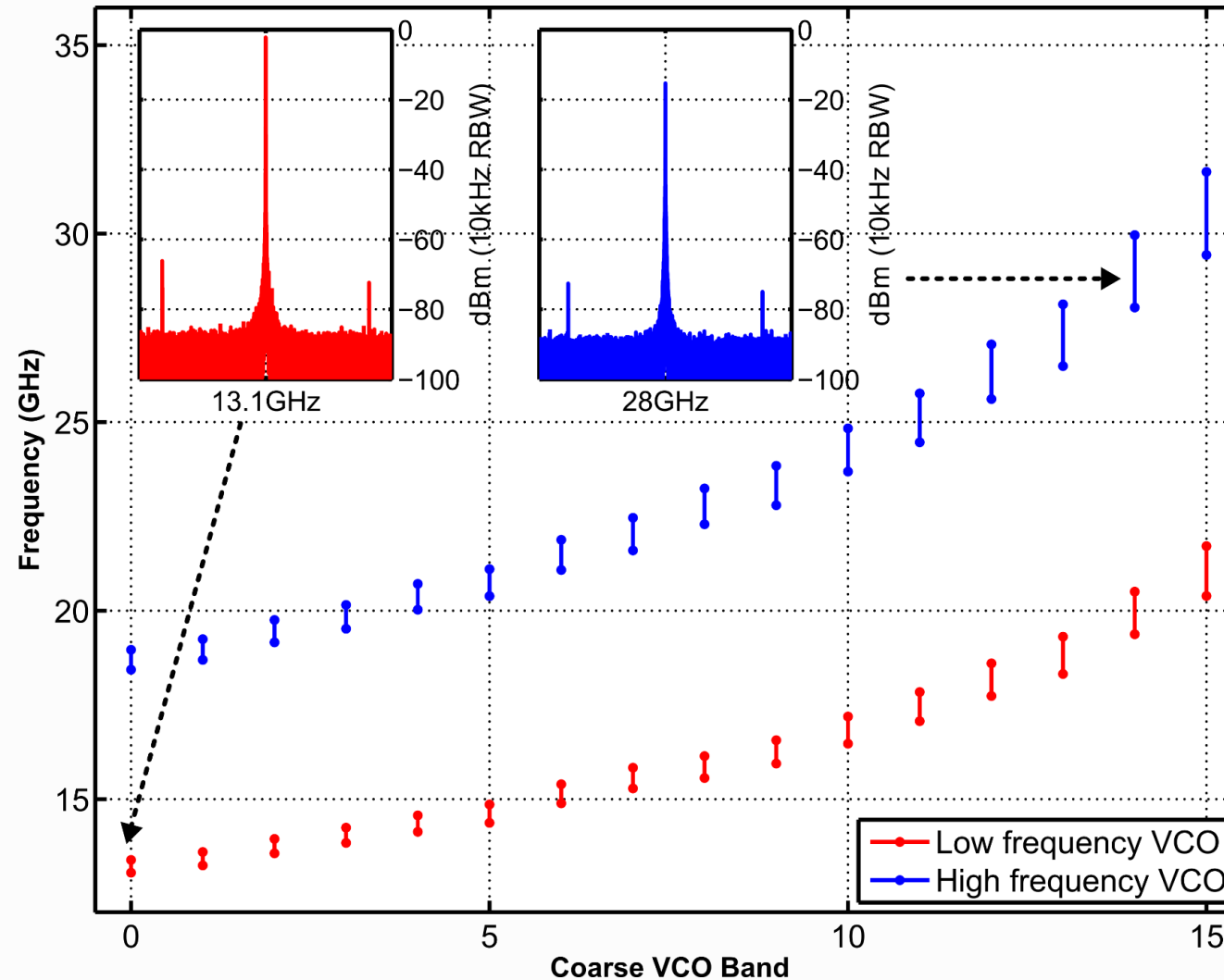
Varactor Folding and Linearization in the Full PLL Context



Die Photo with Layout



Dual D/VCO Tuning Characteristic

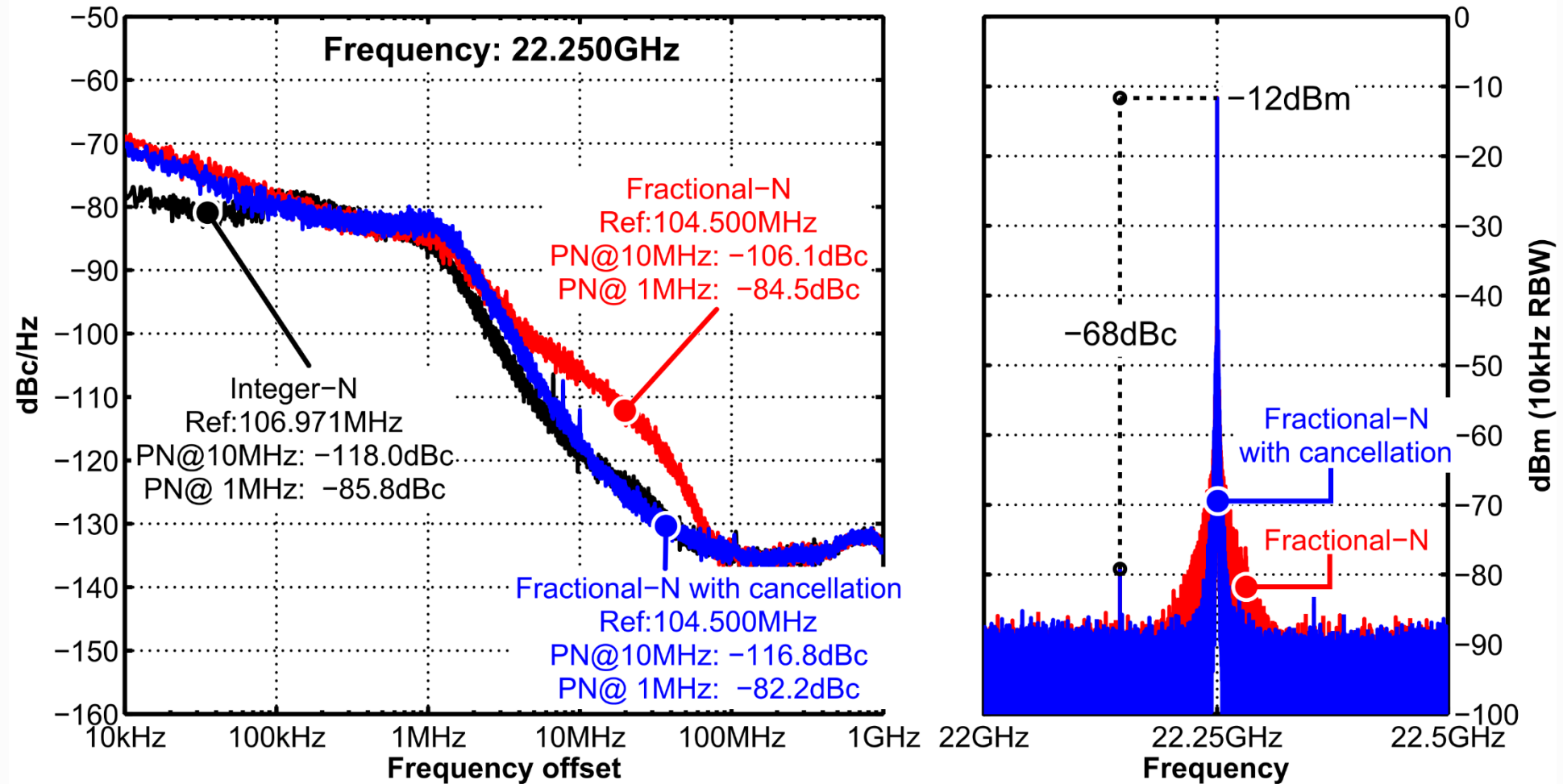


PLL's frequency range is 13.1GHz to 28GHz

M. Ferriss et al, ISSCC15 (D/VCO max frequency is 31GHz)

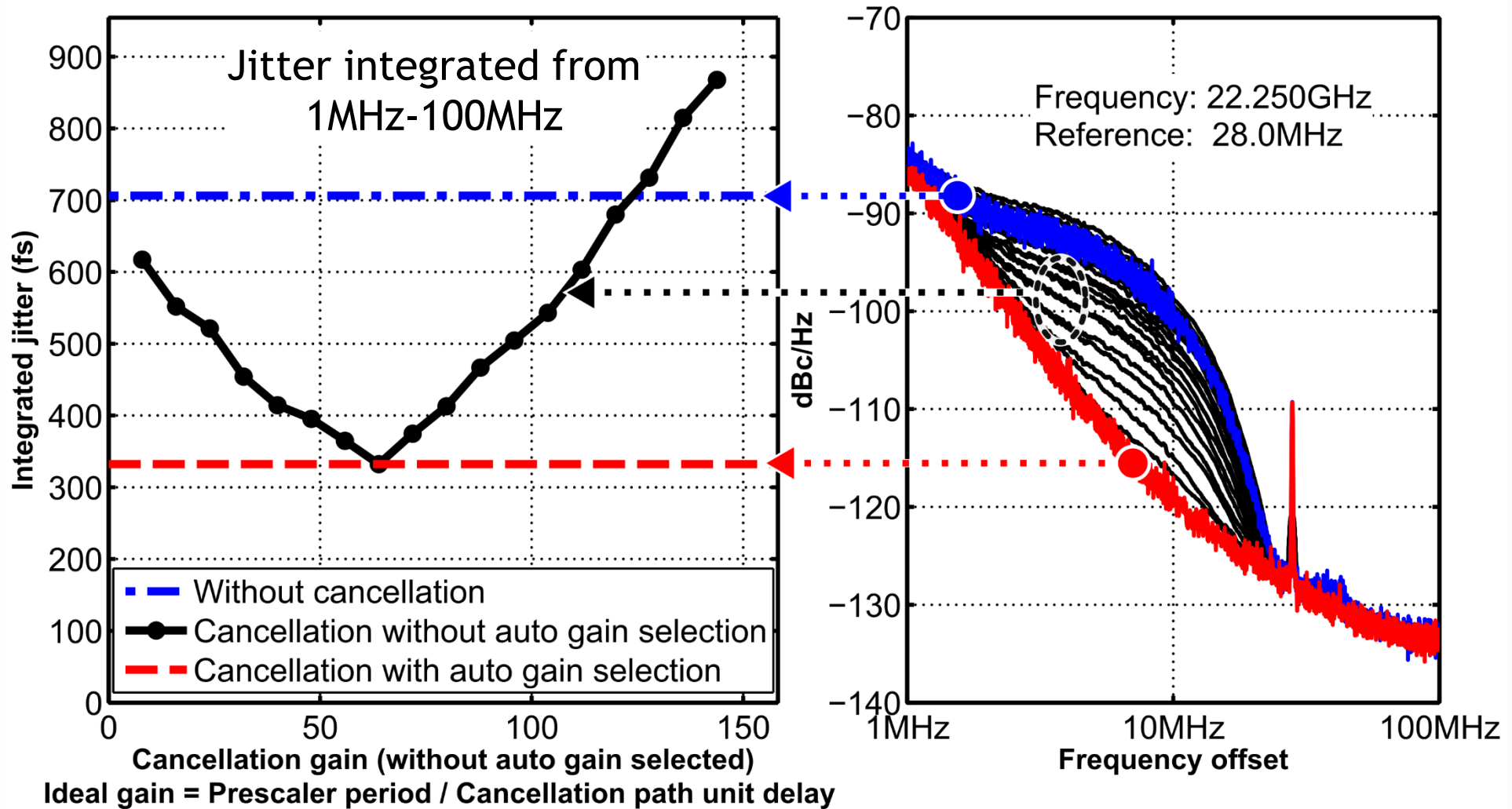
IBM Research - IEEE SSCS DL

Measured Phase Noise and Output Spectrum



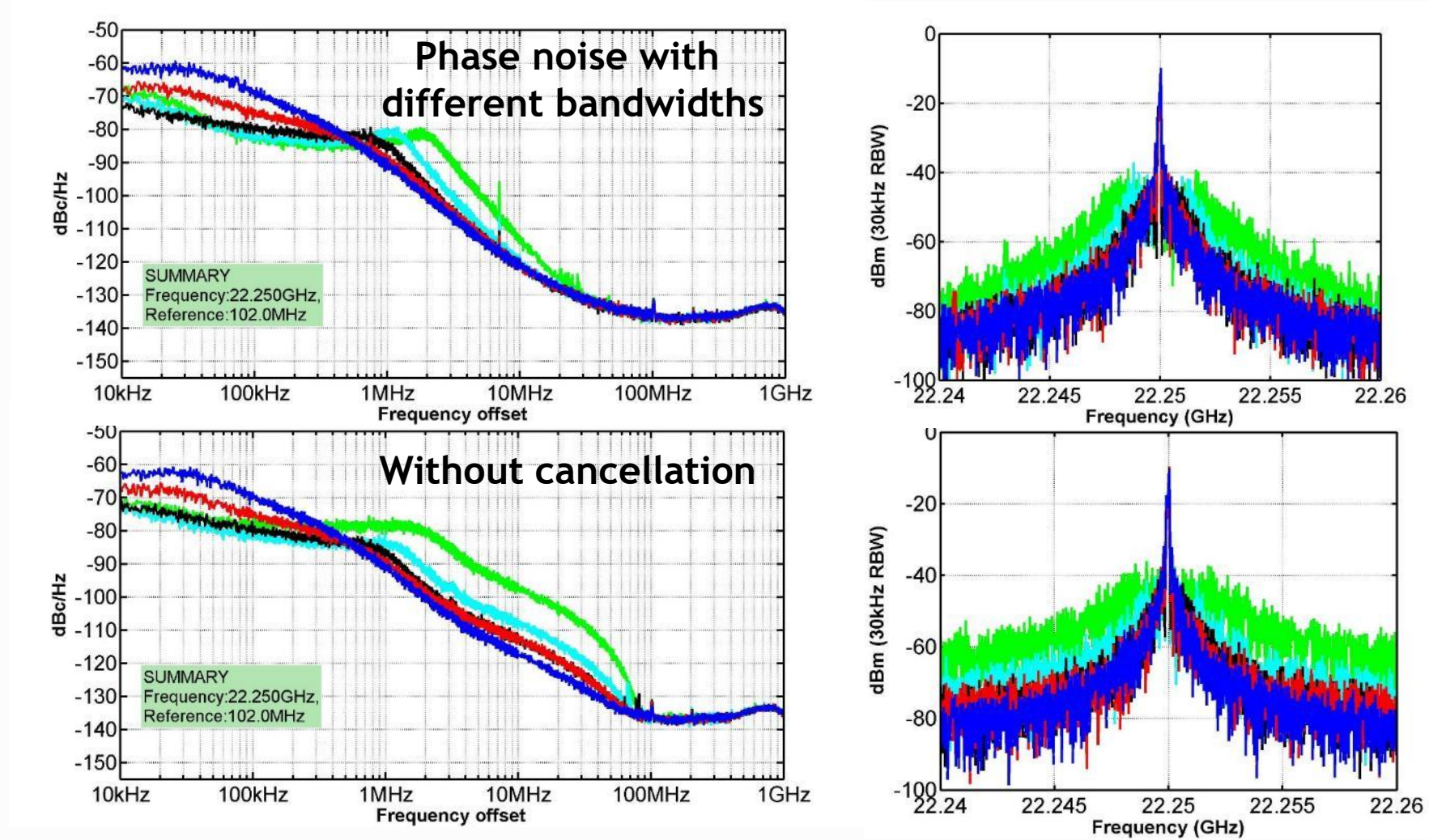
M. Ferriss et al, ISSCC15

Demonstration of DTC Background Cal



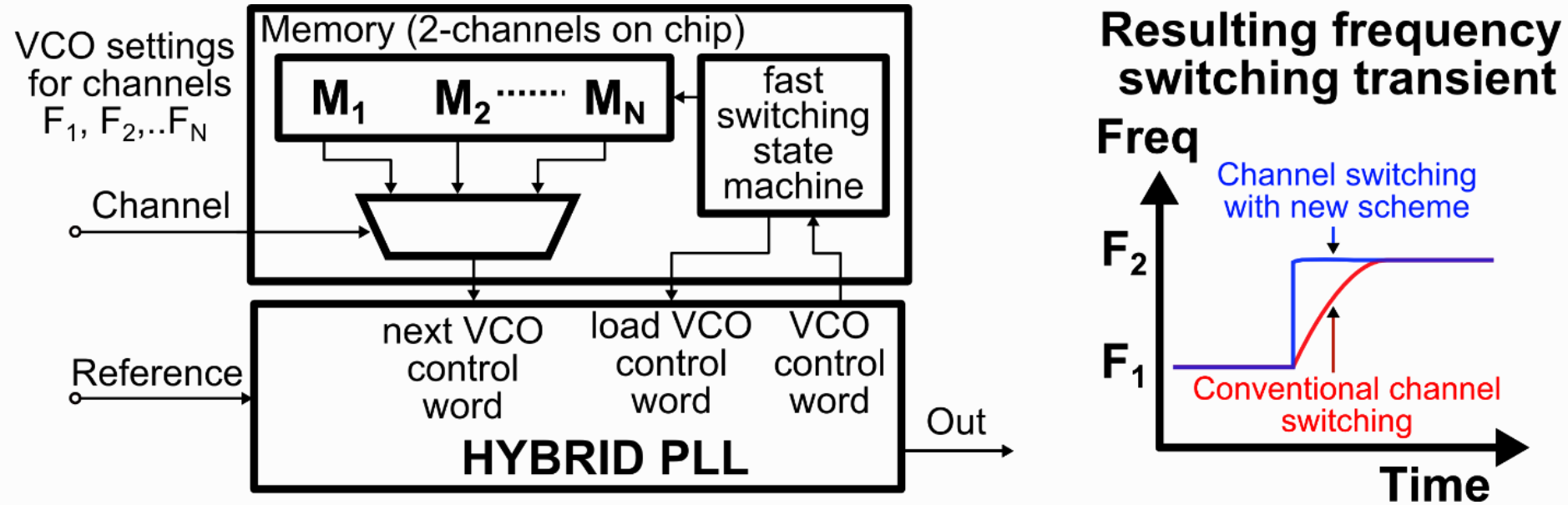
Background calibration engine finds the optimum setting

Trading off High Offset (>1MHz) Noise with Low Offset Noise: PLL Enables Flexible Bandwidth Control



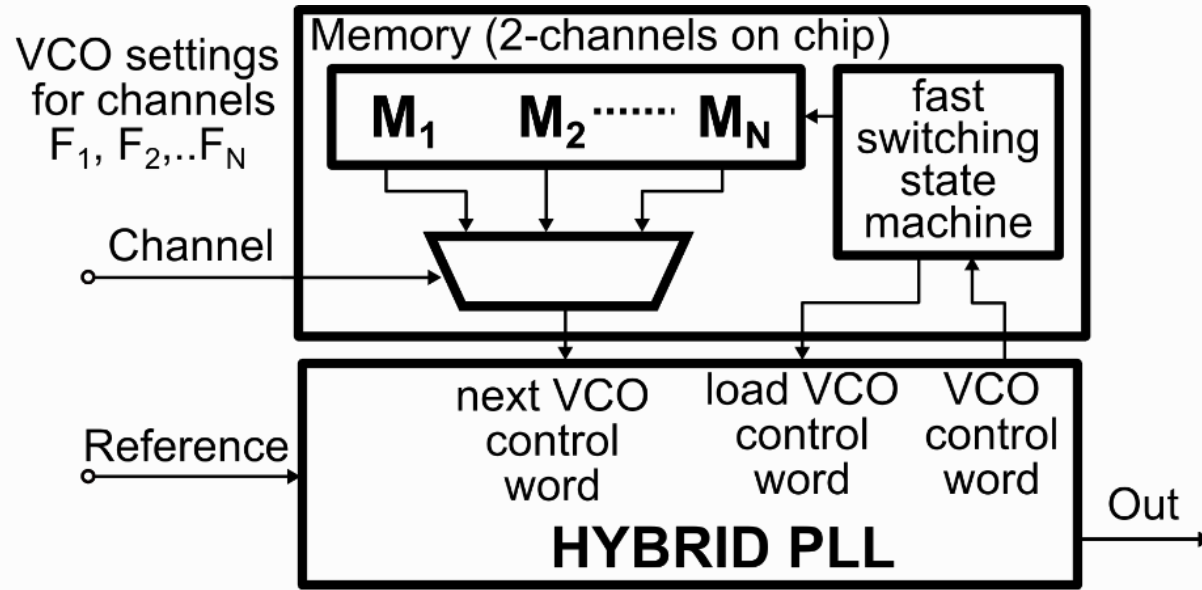
Noise cancellation scheme demonstrated independent of bandwidth (*BW range does not affect dynamic range requirements on cancellation path*)

Fast Hopping with Hybrid PLL: Infrastructure

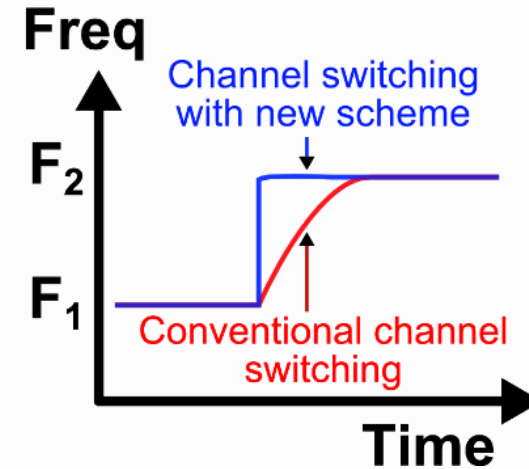


- Memory space to hold digital state information associated with a second frequency
- Fast switching state machine to support transition between active and stored frequency state words
- Within state machine, configurable delays to enable enhanced management of frequency transition

Fast Hopping with Hybrid PLL: Use Model

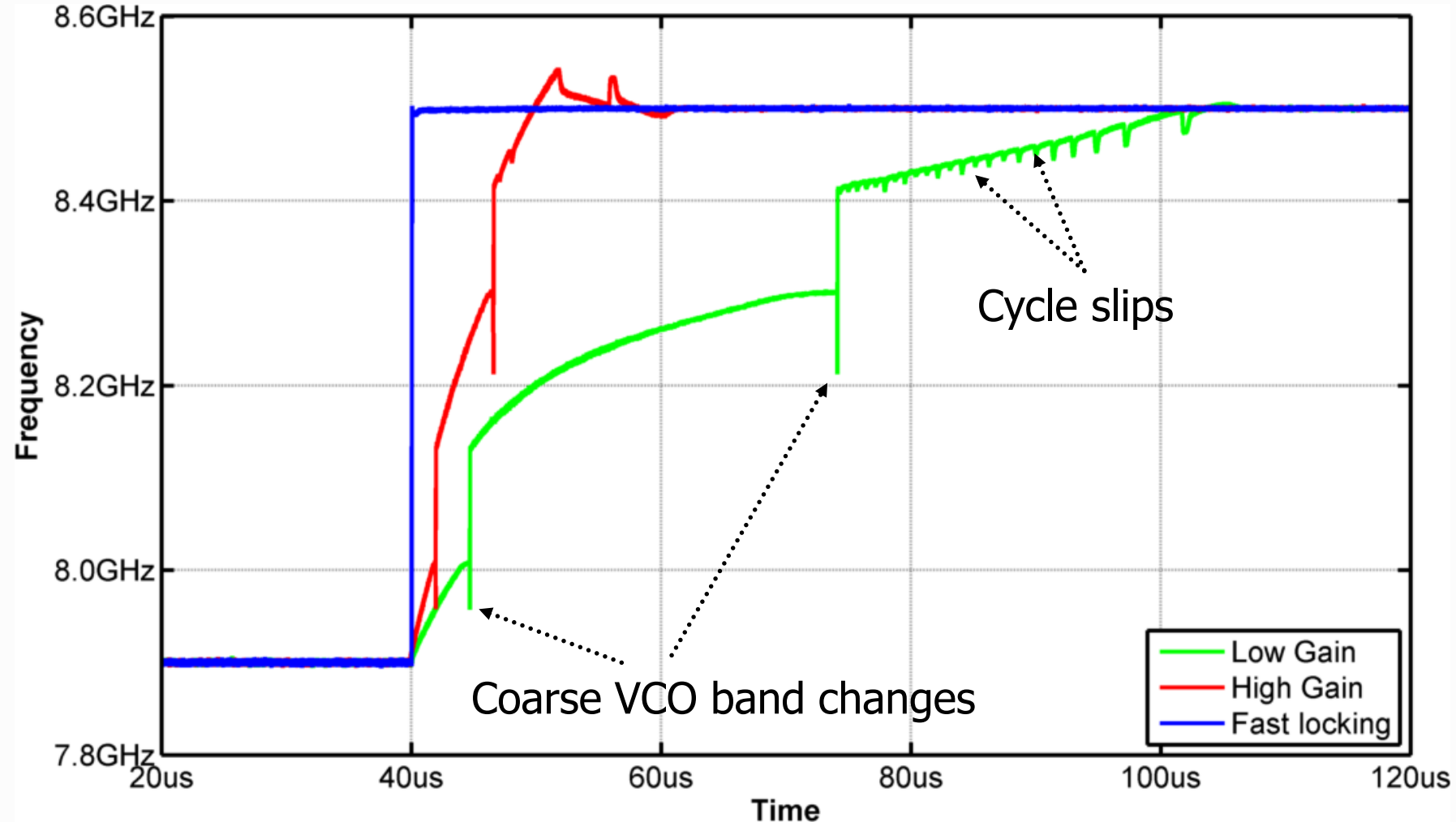


Resulting frequency switching transient



- Two frequency case (simplest, illustrated on next chart):
 - Initialization: Lock to f_1 , store PLL state, then lock to f_2
 - Hopping: on each transition, load stored state for new frequency and store current state for future use
- General case
 - Initialization: Lock to f_1, \dots, f_n , store PLL states in external memory using serial interface
 - Hopping: (1) load future target state from serial interface prior to hop request; (2) execute hop as in 2-frequency case; (3) store updated state information for last frequency used in external memory using serial interface

Transient Locking



Measured response to step in division ratio (1) with different integral path gain settings (green, red), and (2) with direct loading of digital control word as in control scheme described in previous charts (blue)

Conclusion: Frac-N, Fast-Hopping Hybrid PLL Implementation

Key results

- A 13.1-28 GHz, frac-N, low noise hybrid PLL drawing 31mW from 1V demonstrated in 32nm CMOS
- Design features analog proportional path, and (mostly) digital $\Delta\Sigma$ cancellation and integral paths
- Supports reference frequencies from 15-400MHz and includes infrastructure for fast hopping

Challenges and opportunities

- Further improve integral path
- Can we do something about banded nature of design?

Outline

- Introduction and motivation: hybrid architectures
- Initial implementation: proof-of-concept
- Flexible synthesizer: frac-N w/ noise cancellation
- **Flexible synthesizer: coarse band elimination**
- Flexible synthesizer: flicker noise suppression exploration
- Summary/conclusion

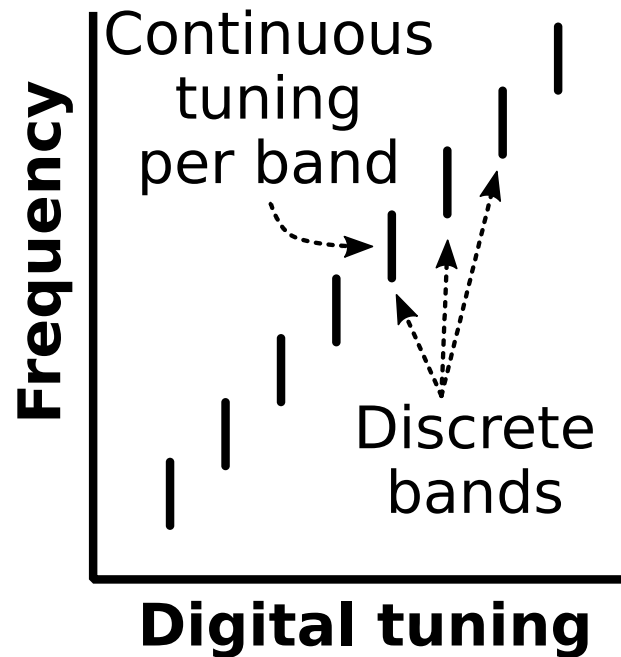
Fractional-N Hybrid PLL with Coarse Band Elimination

- Objective: retain benefits and capabilities of hybrid frac-N design, and remove need for VCO frequency banding without sacrificing noise performance
- Approach
 - Extend varactor folding concept to include coarse band capacitance
 - Enhance integral path design to improve performance
- Key challenges
 - Switched capacitor element choice
 - Introduction of enhanced control scheme

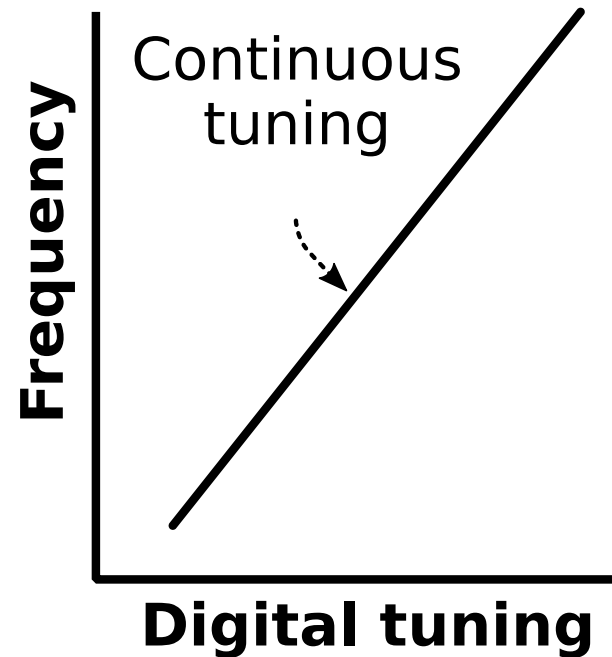
Motivation

- Objective: Remove coarse bands of CMOS oscillators
- Impact: extends PLL lock range to entire VCO tuning range, allowing, for example, improvement in lock maintenance in wireline applications and enabling fast wide-range chirp generation for wireless/radar

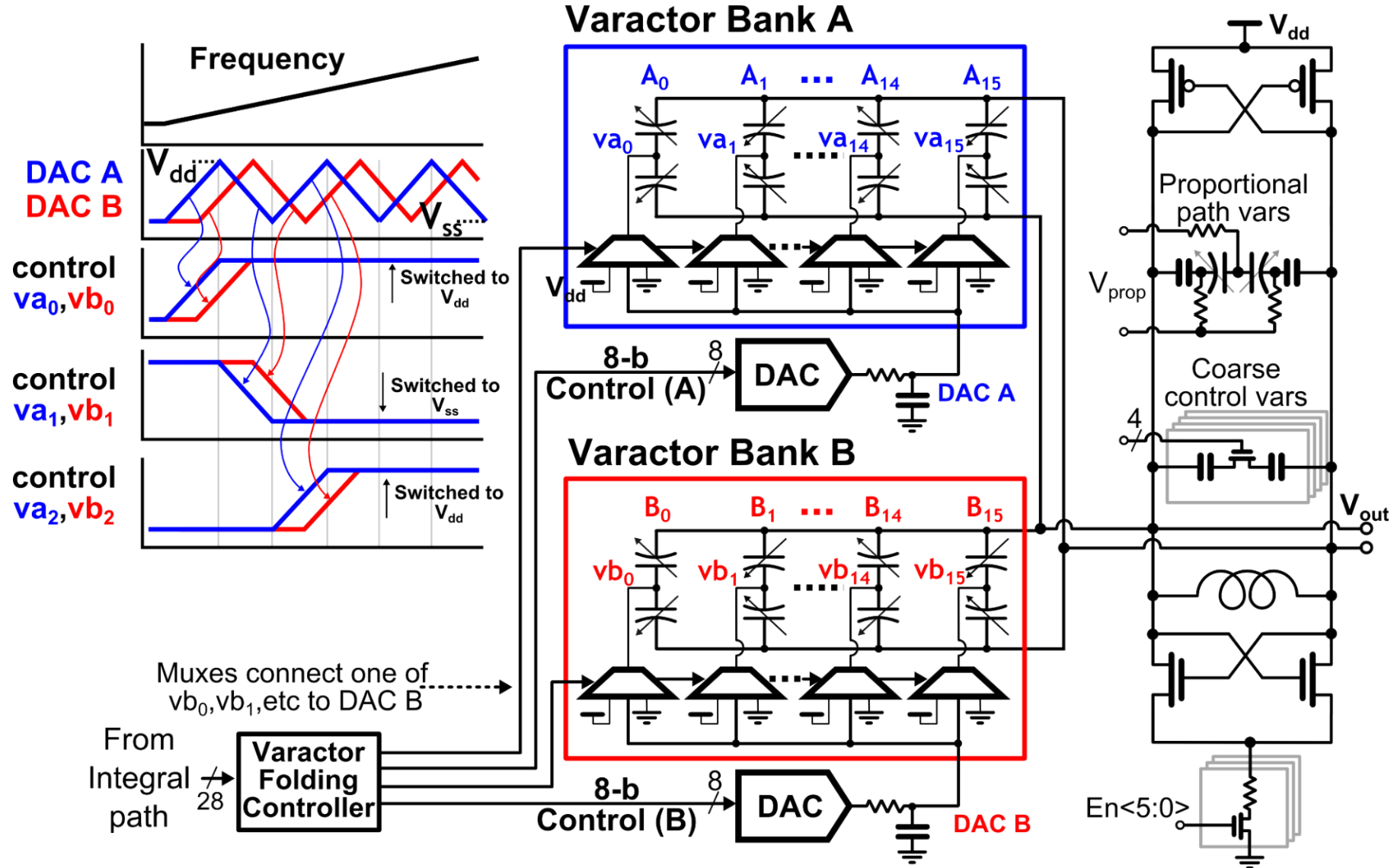
**Typical VCO
tuning scheme**



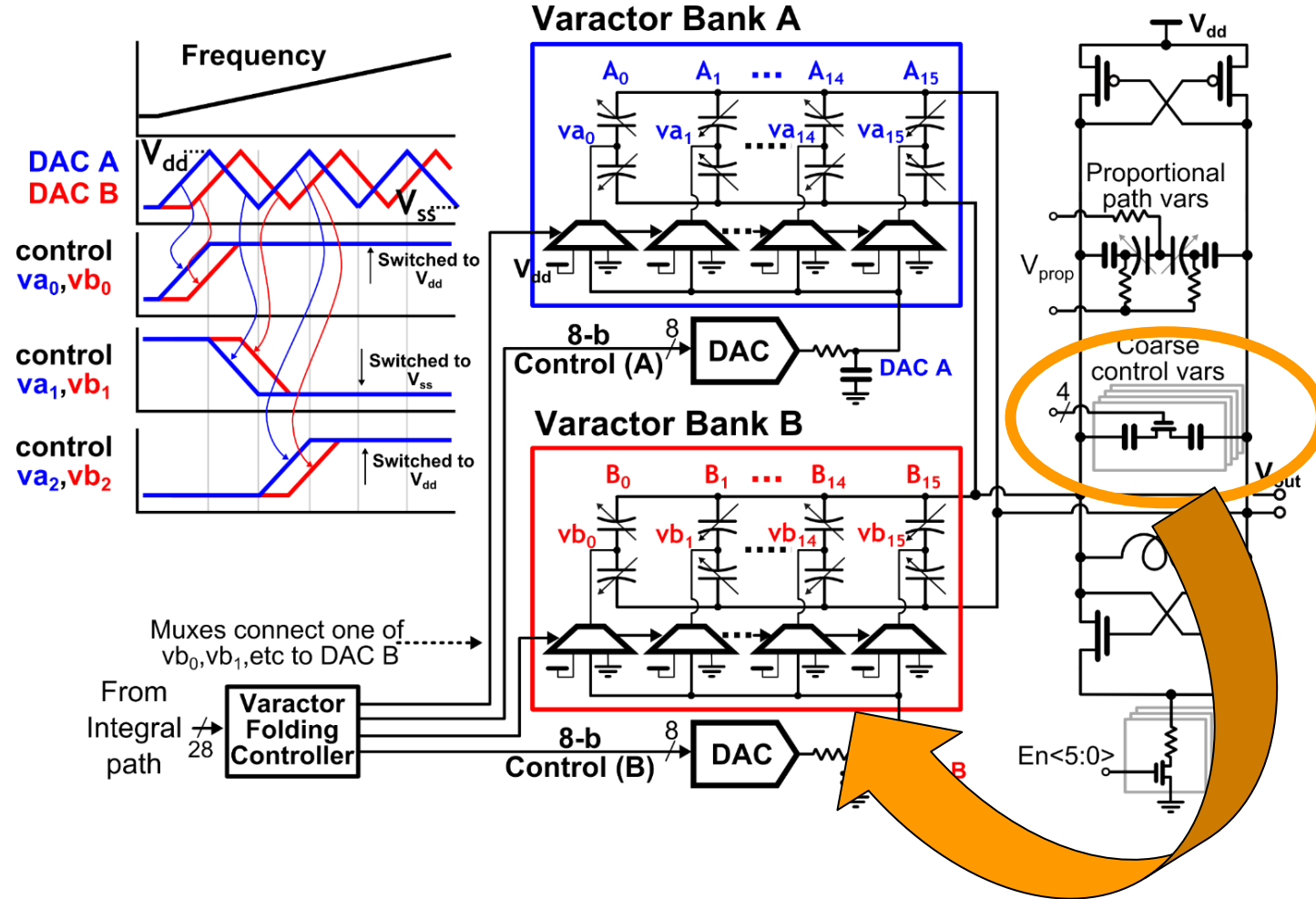
Objective



Varactor Folding in the Full PLL Context: Reminder

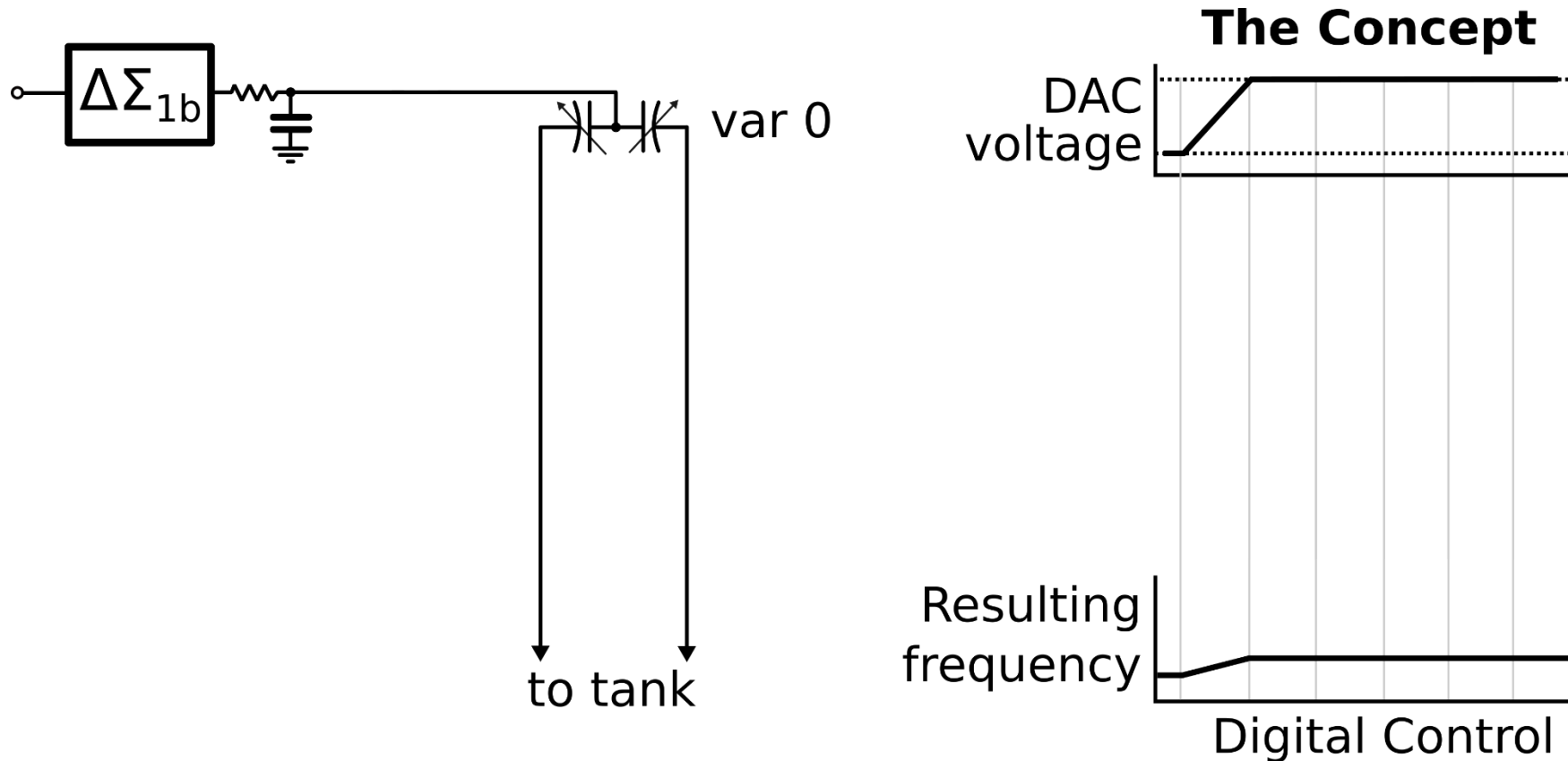


Coarse Band Elimination in VCO Design Context



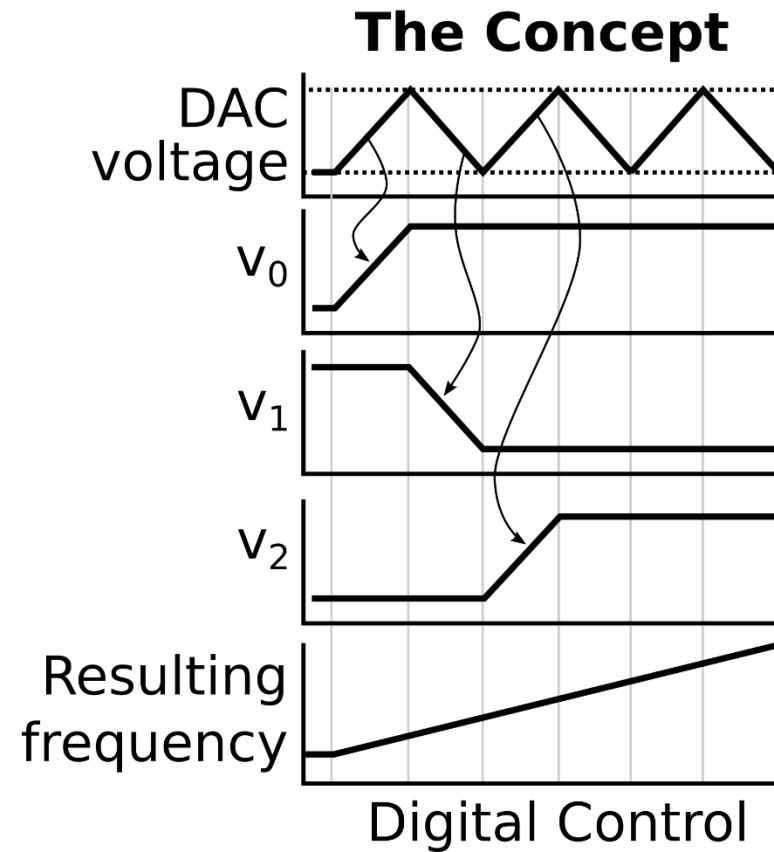
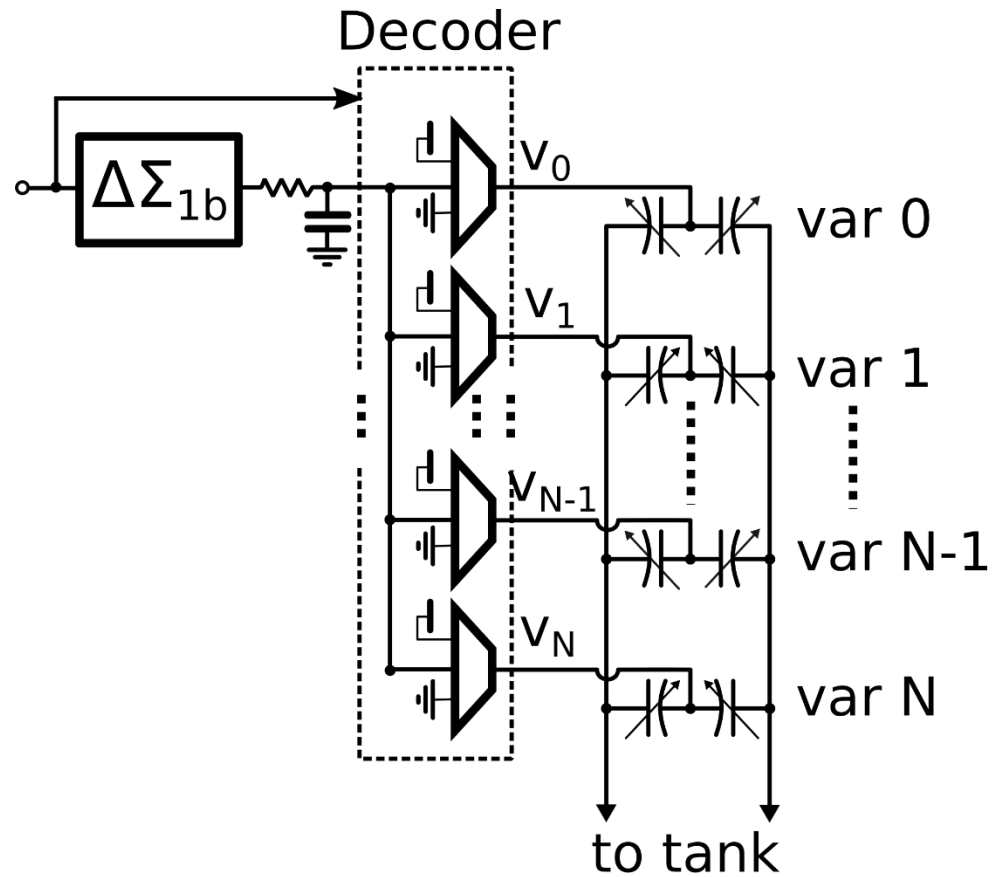
Key goal: move all coarse varactor capacitance into integral path varactor folding infrastructure

Digital control of a varactor



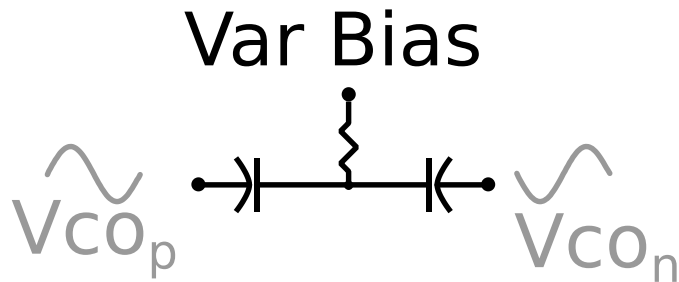
Trade off between $\Sigma\Delta$ noise and gain/tuning range

Extending the range: varactor folding (review)

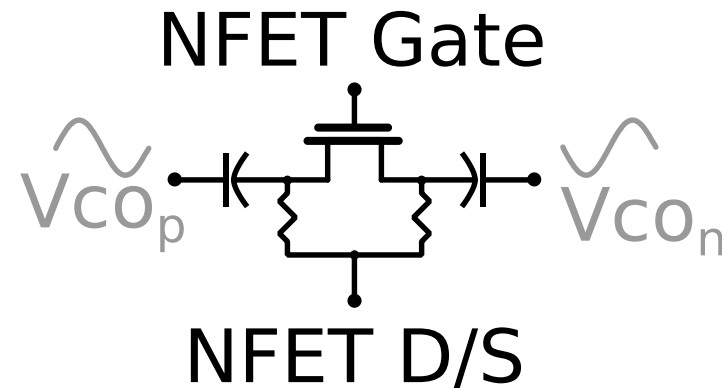


Comparing typical tuning mechanisms

Continuous tuning:
UGN varactor

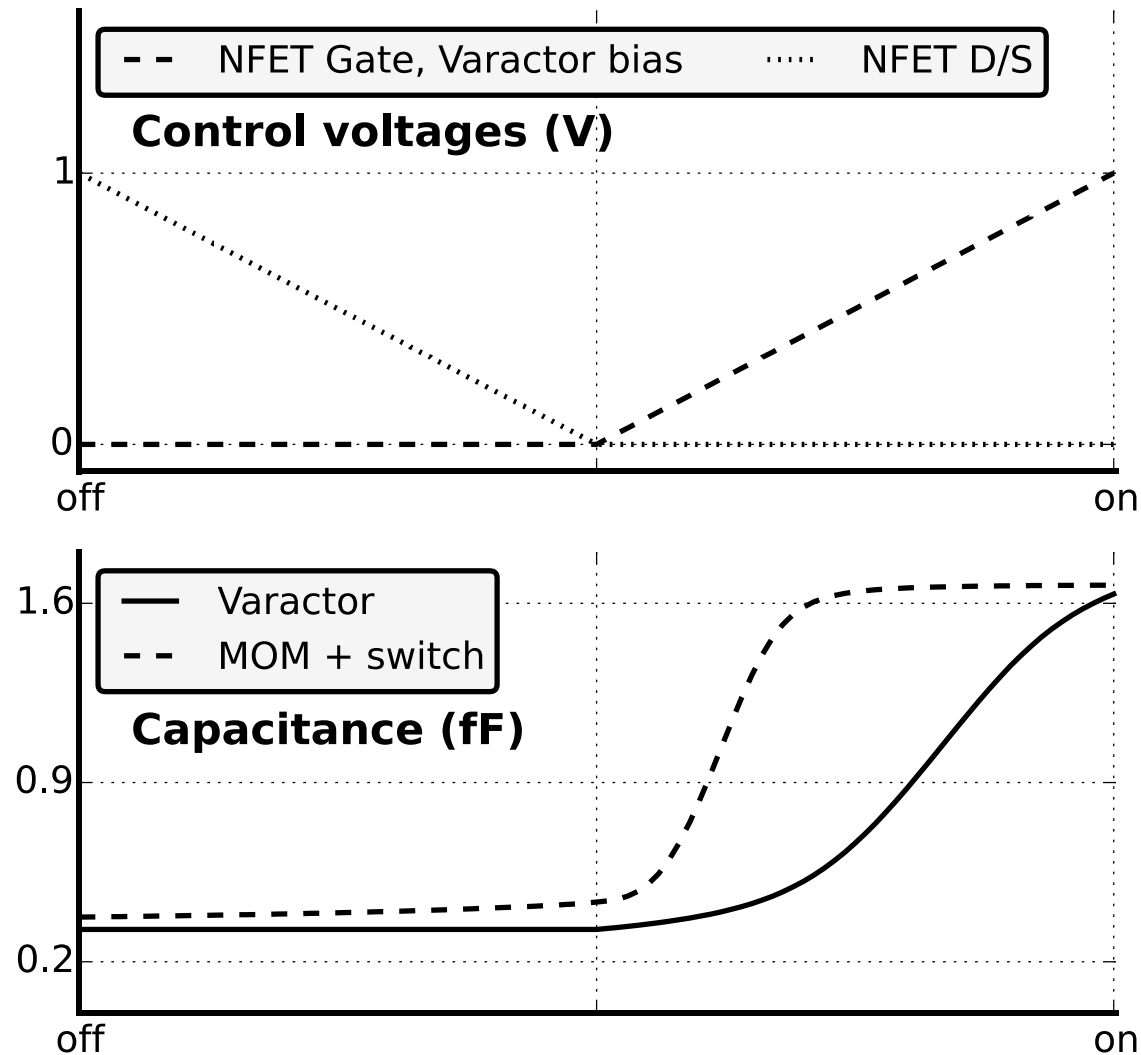


Discrete tuning:
MOM + Switch



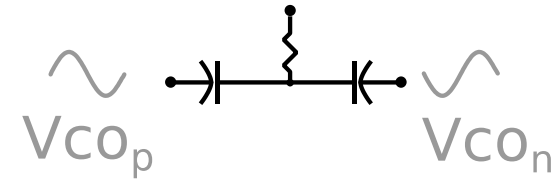
Can we use MOM+switch for continuous tuning?

Varactors vs MOM+switch (Cap)



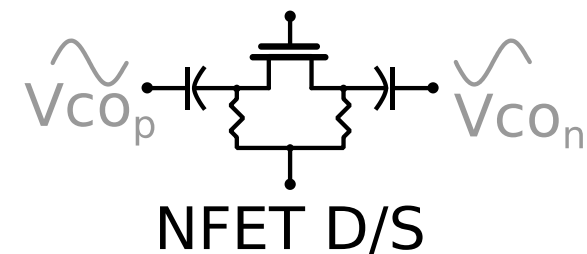
UGN varactor

Var Bias

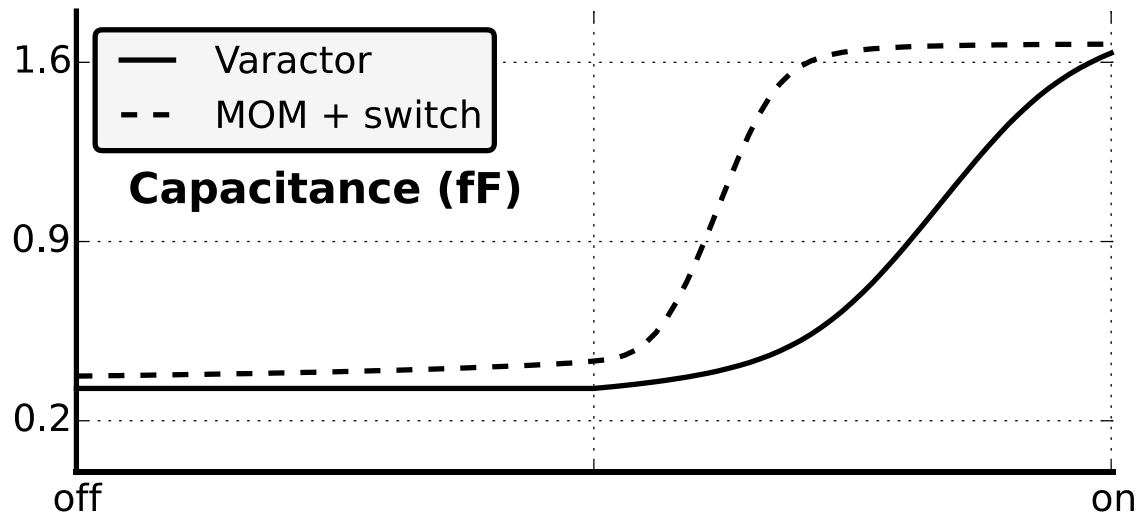
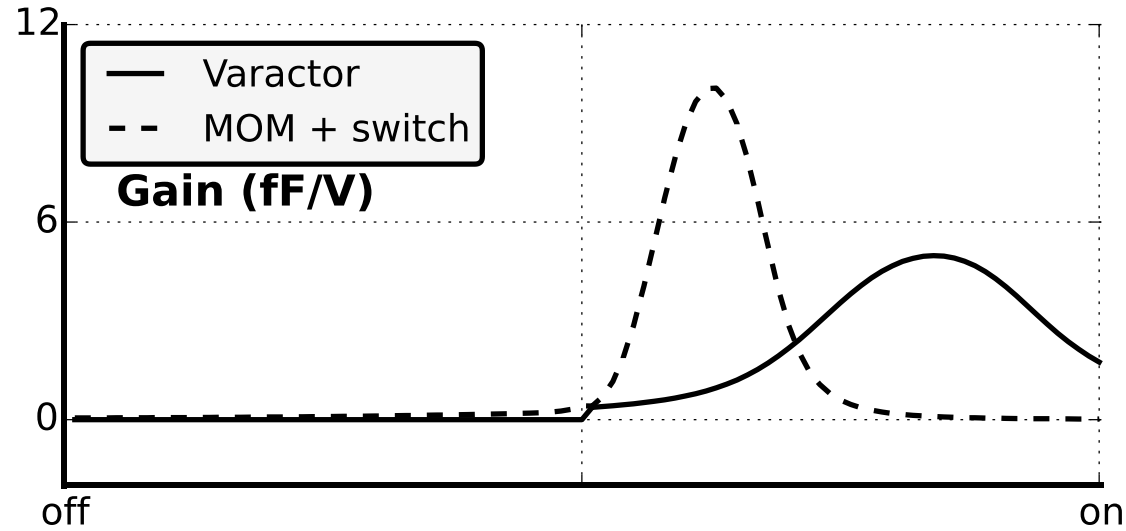


MOM + Switch

NFET Gate

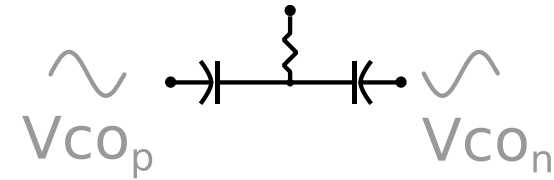


Varactors vs MOM+switch (Gain)



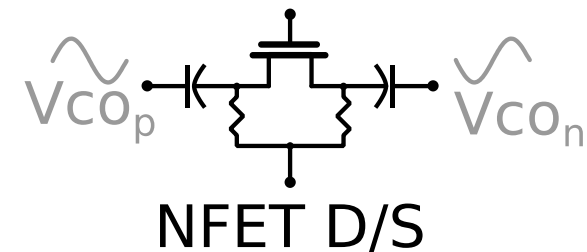
UGN varactor

Var Bias

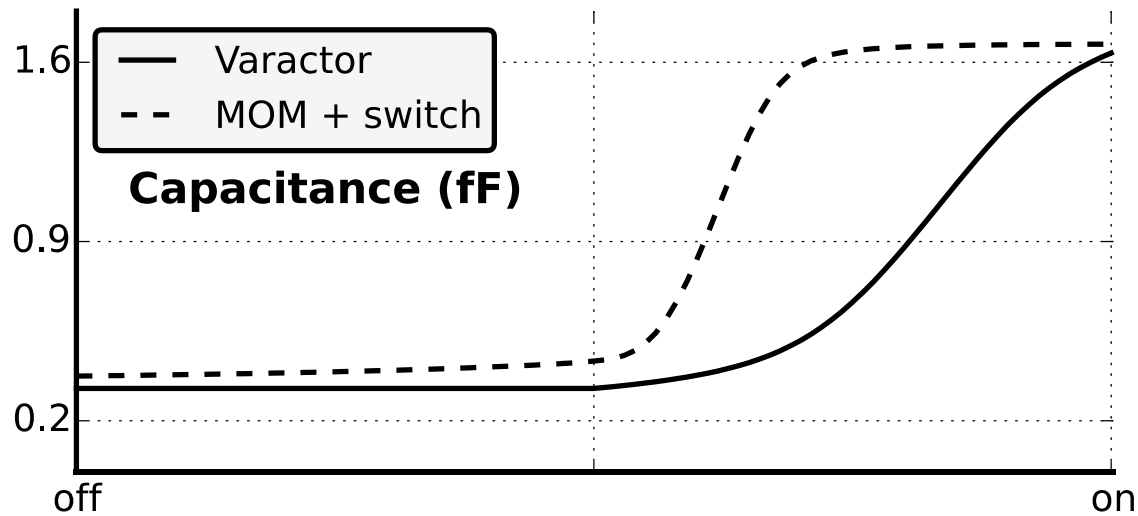
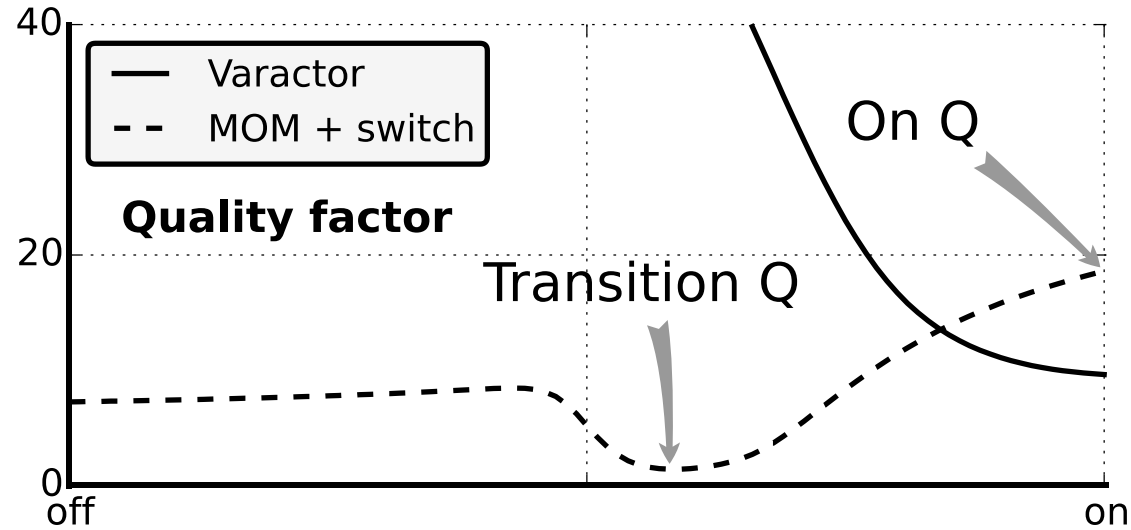


MOM + Switch

NFET Gate

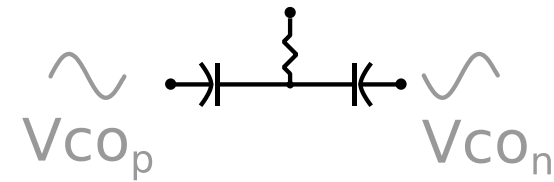


Varactors vs MOM+switch (Q)



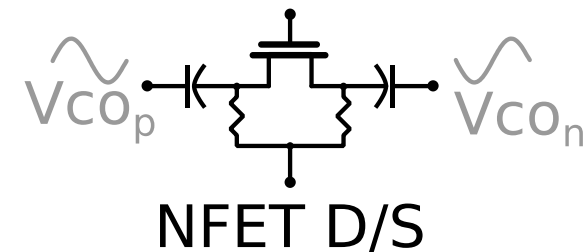
UGN varactor

Var Bias

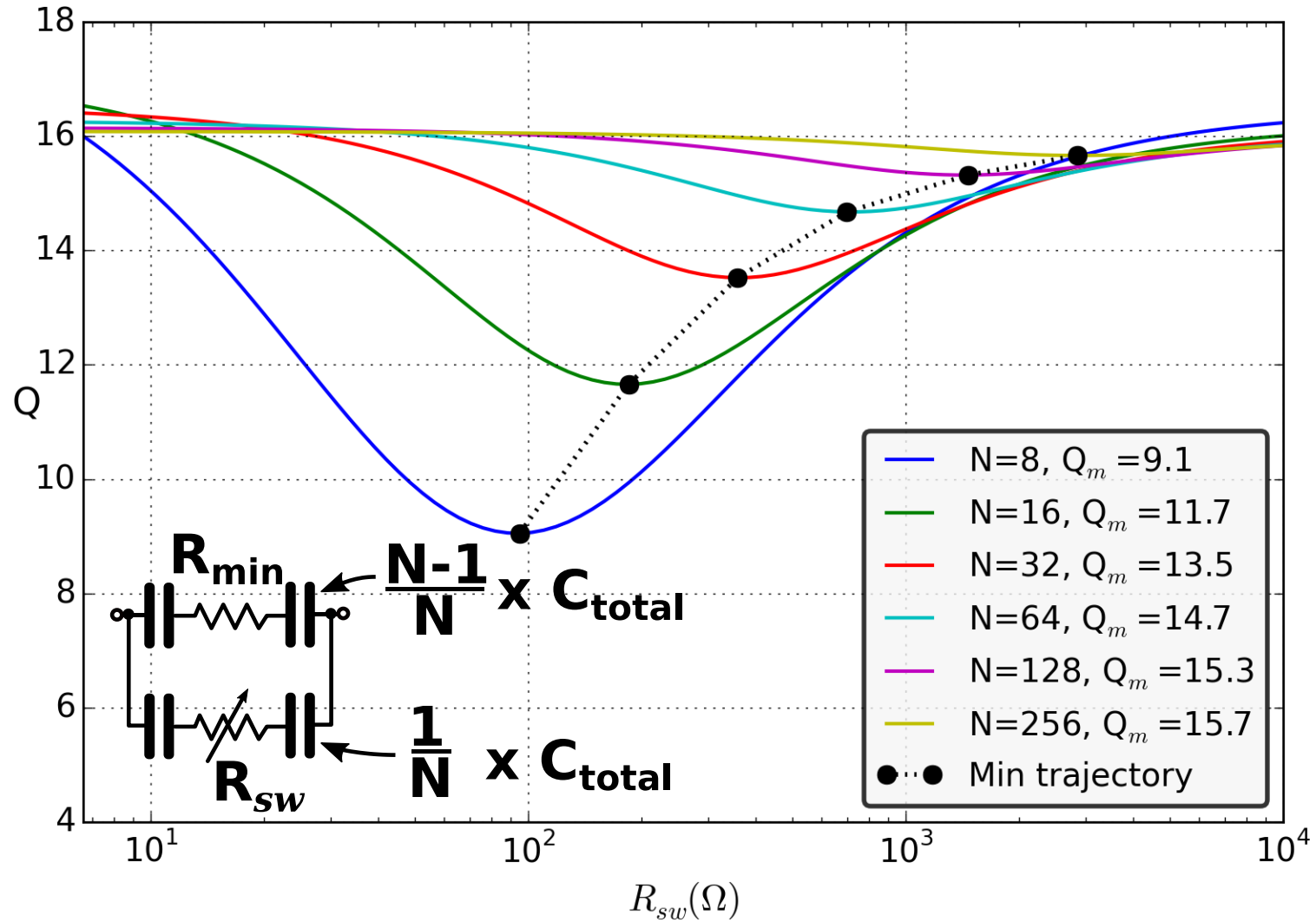


MOM + Switch

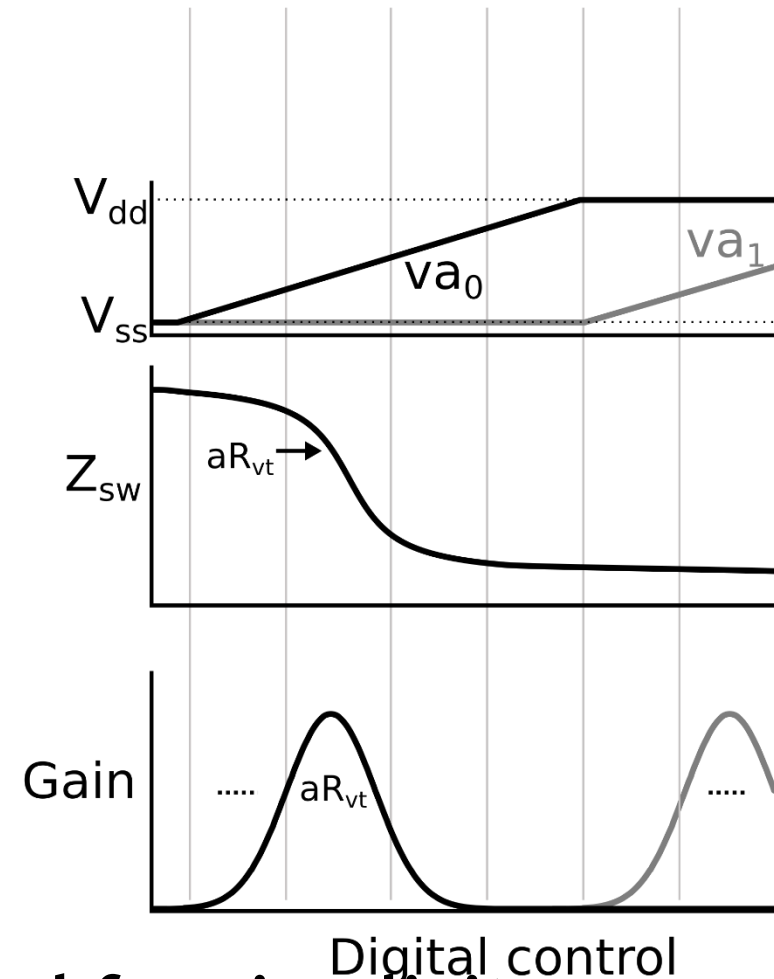
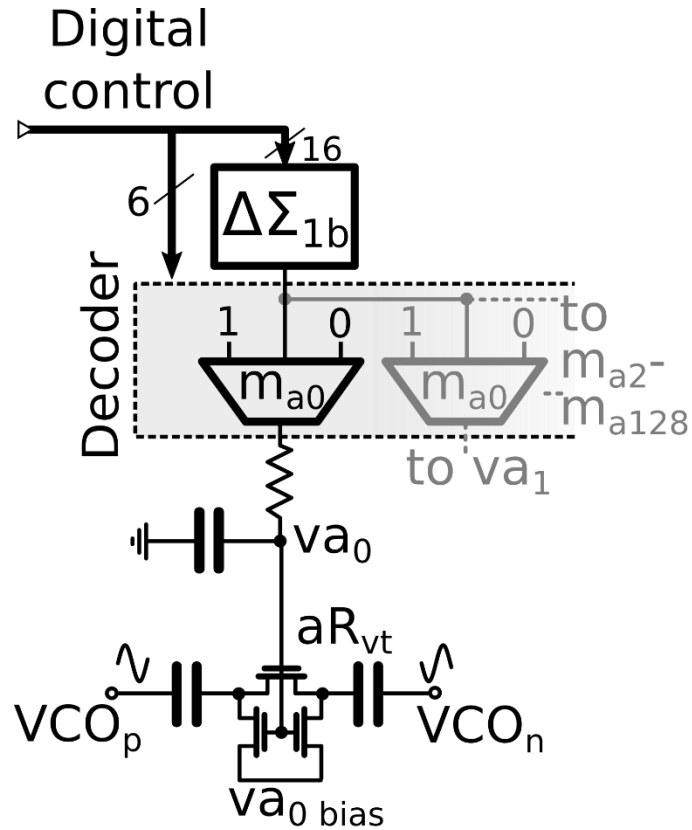
NFET Gate



Q degradation

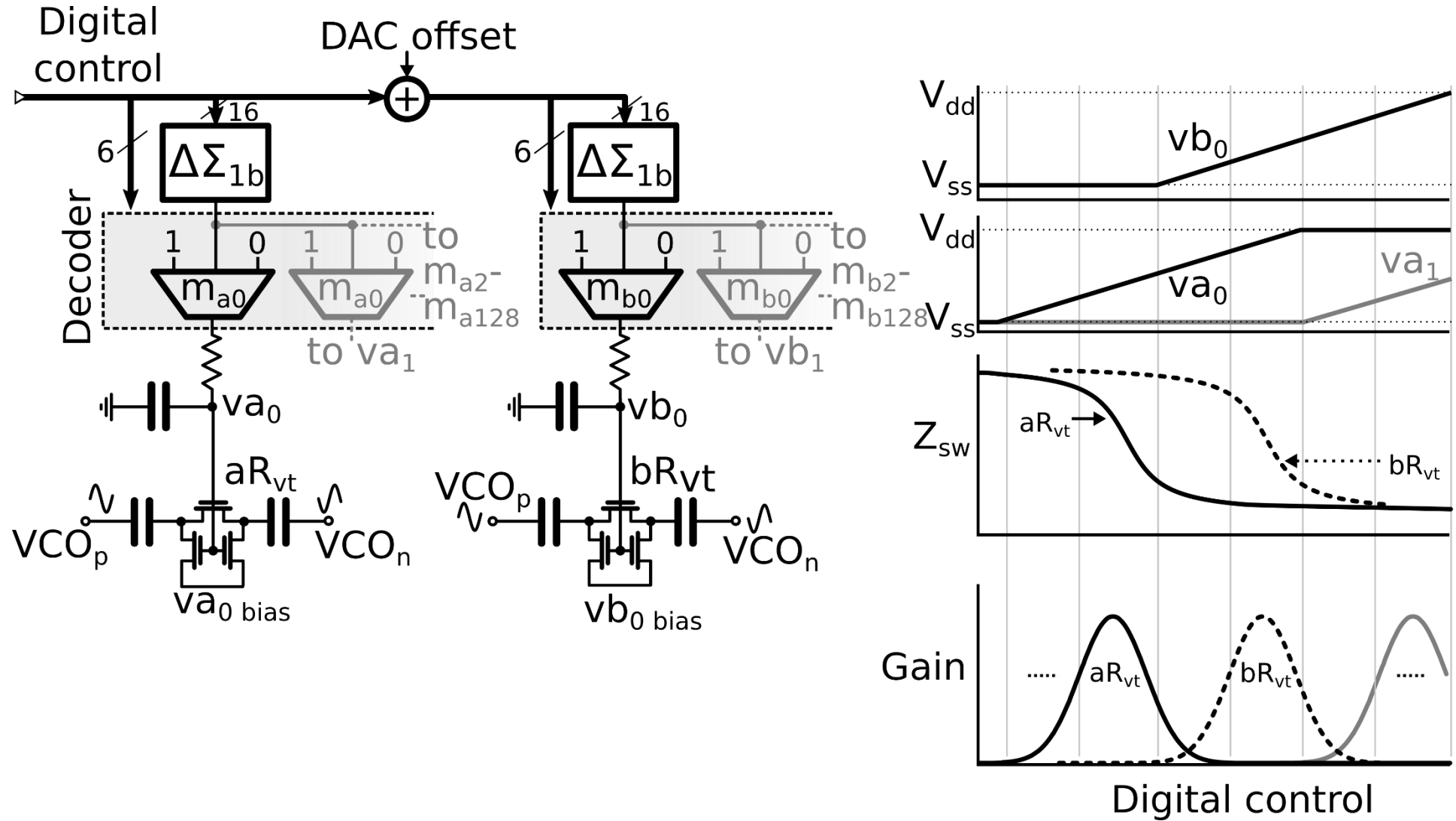


One band



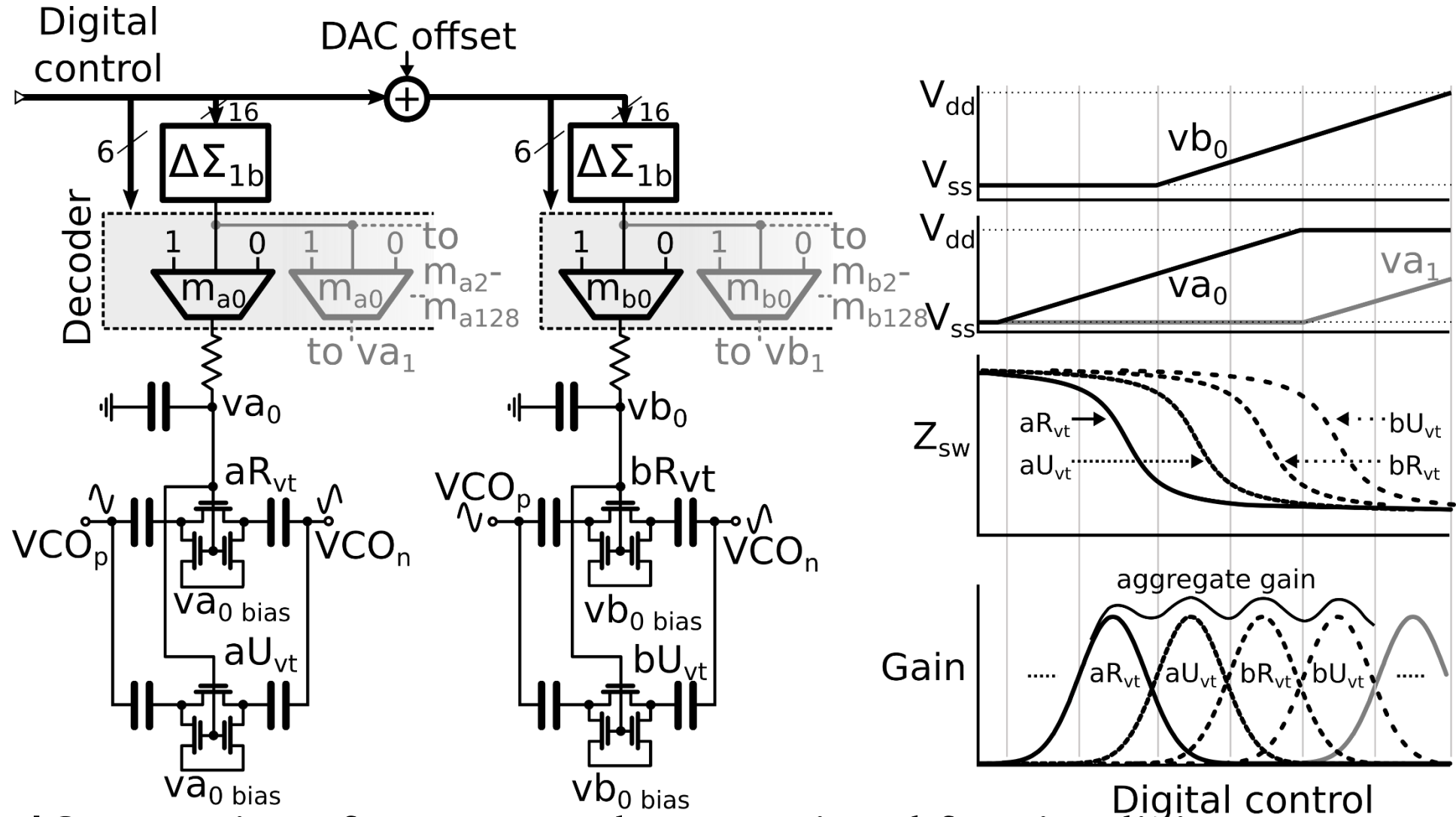
*Connections for va_0 bias omitted for simplicity

Two bands with offset



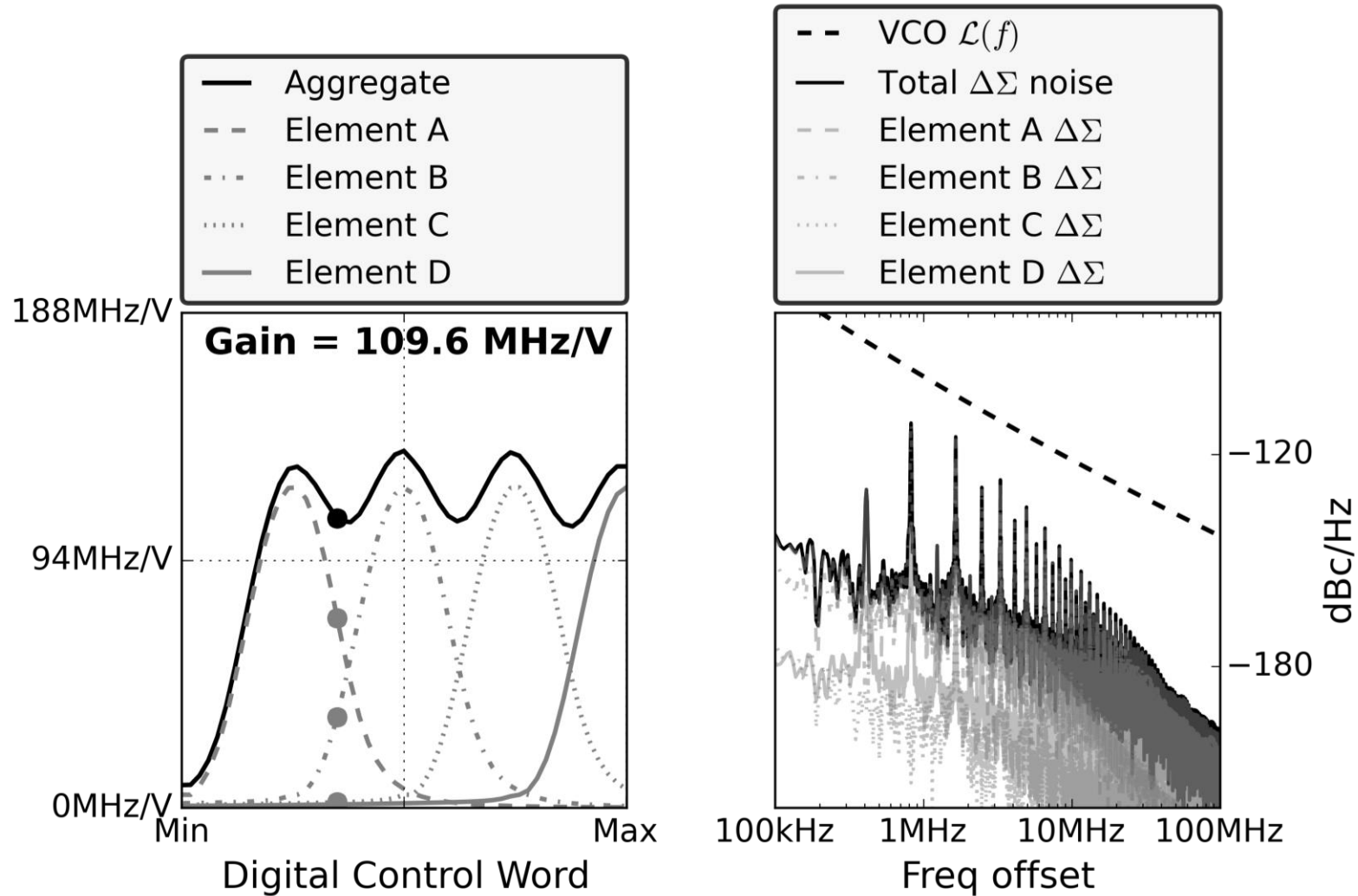
*Connections for va_0 bias, vb_0 bias omitted for simplicity

Two bands and two thresholds

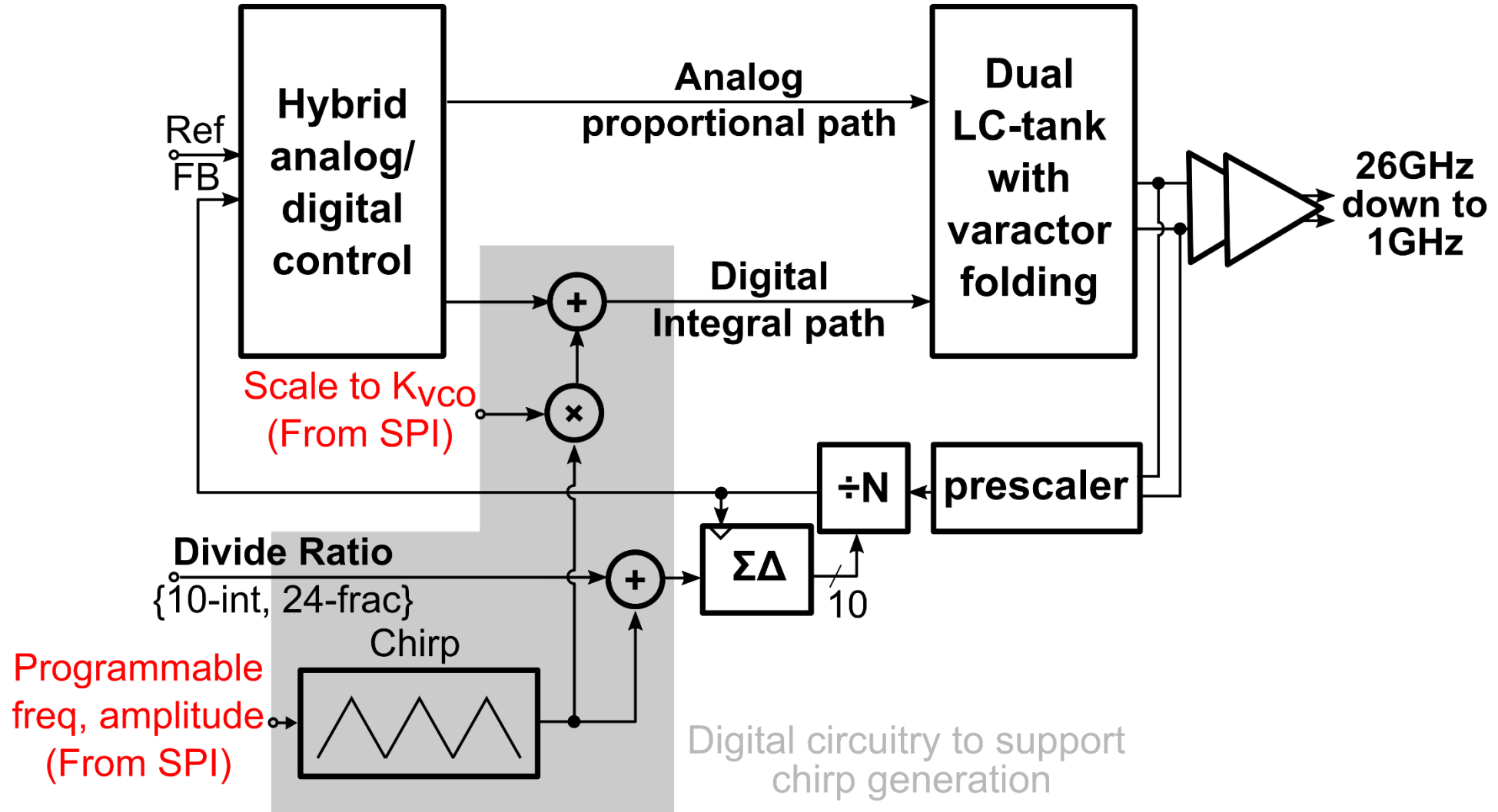


***Connections for va_0 bias, vb_0 bias omitted for simplicity**

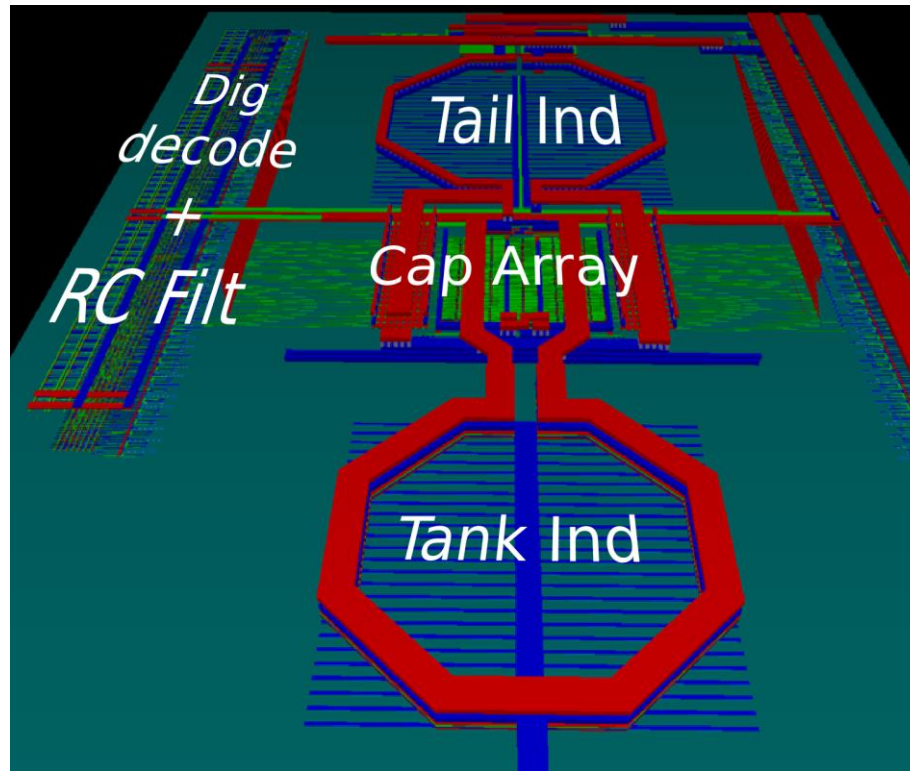
Varactor gain versus frequency



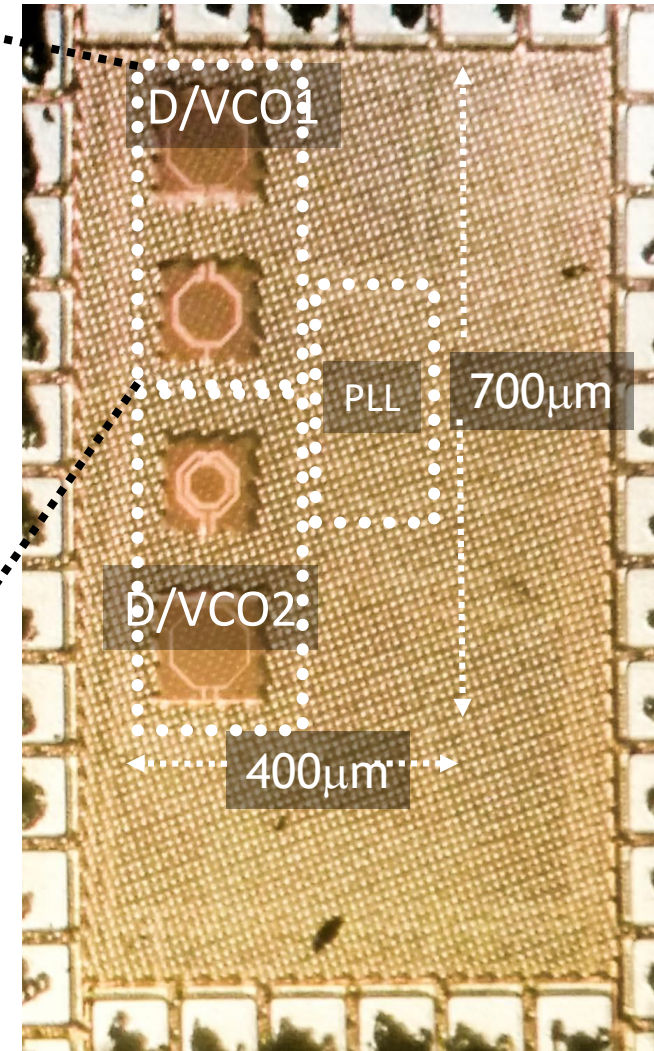
PLL architecture



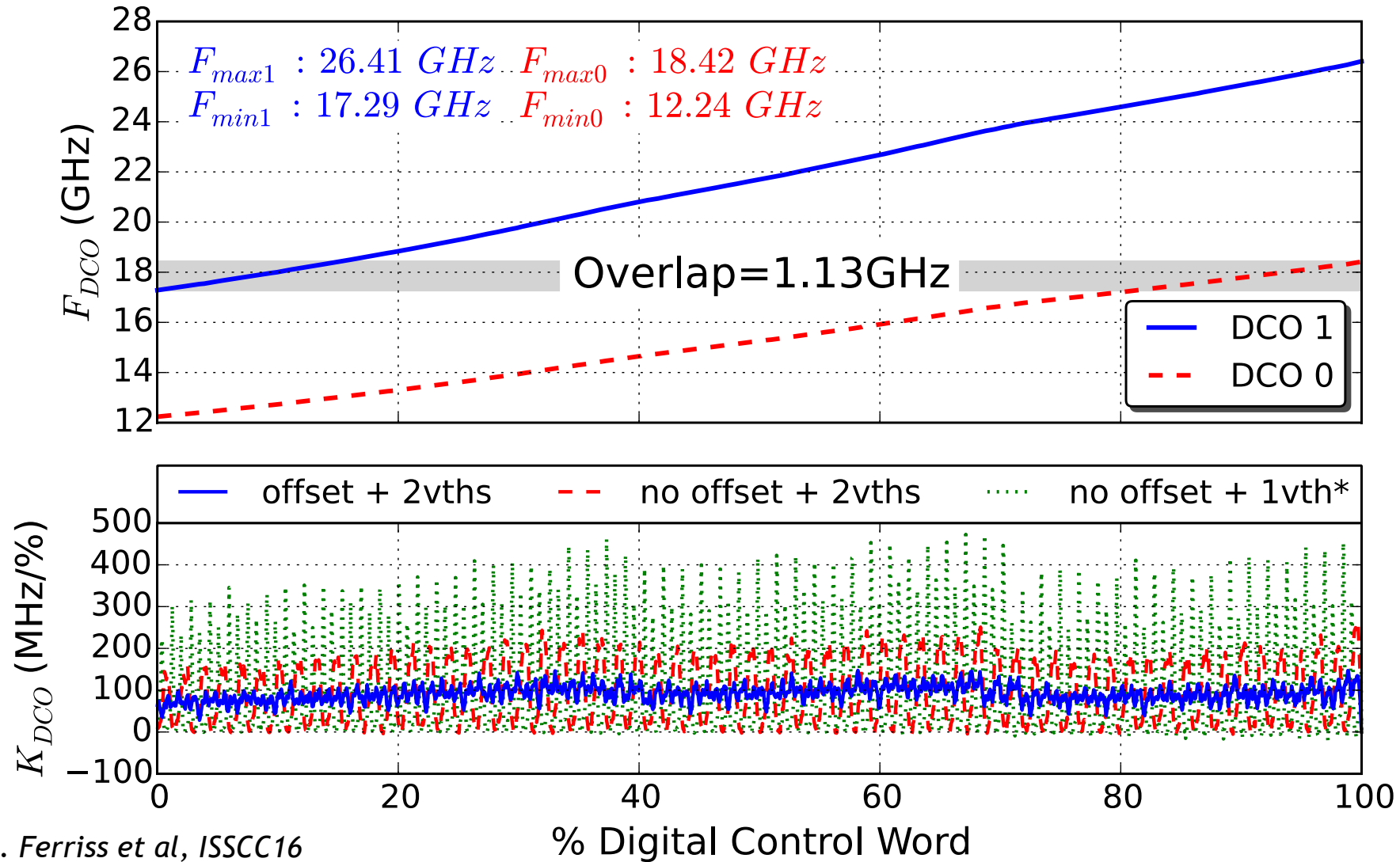
32nm SOI CMOS prototype



Visualization with GDS3D

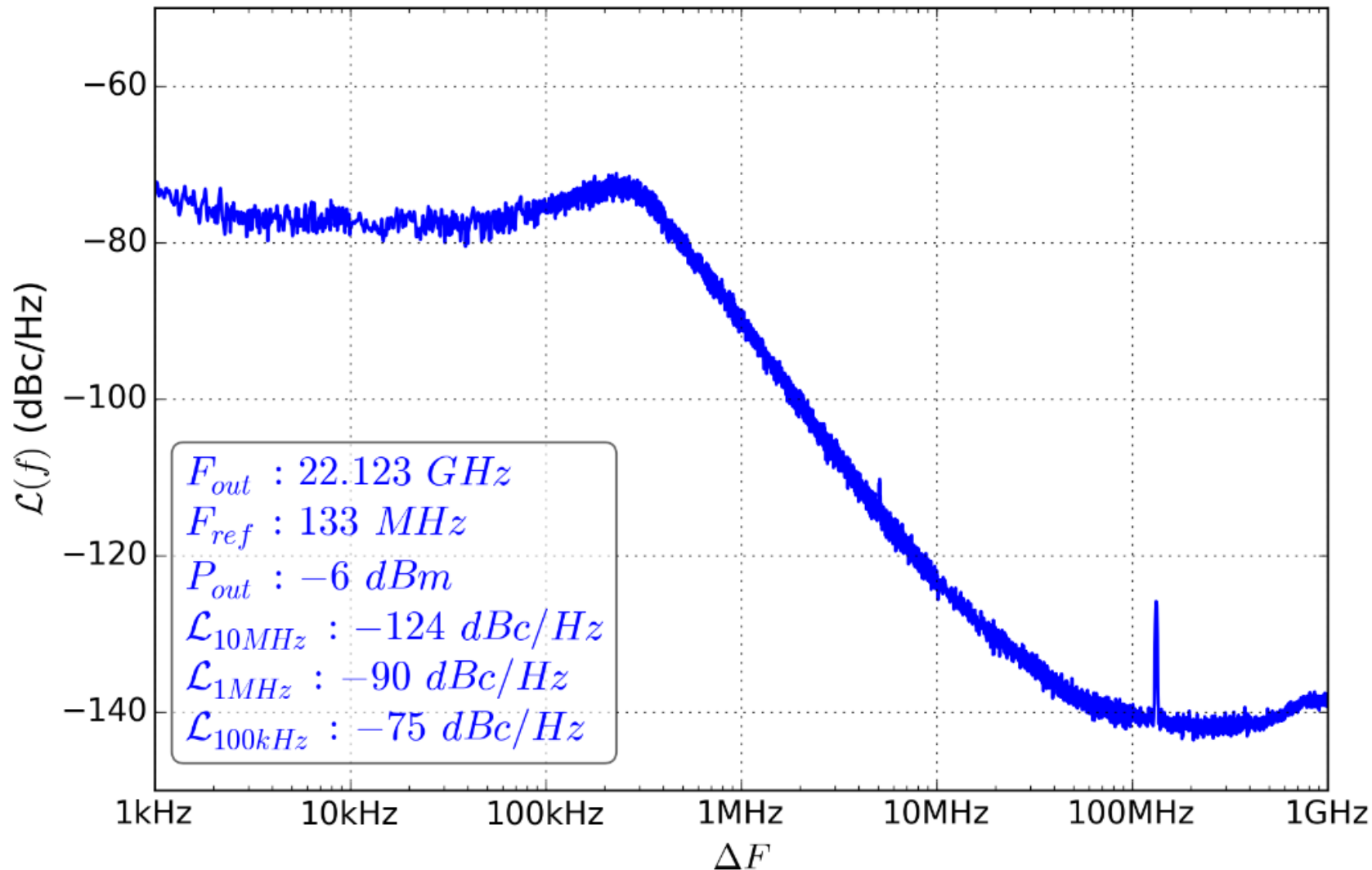


Measured tuning range and gain



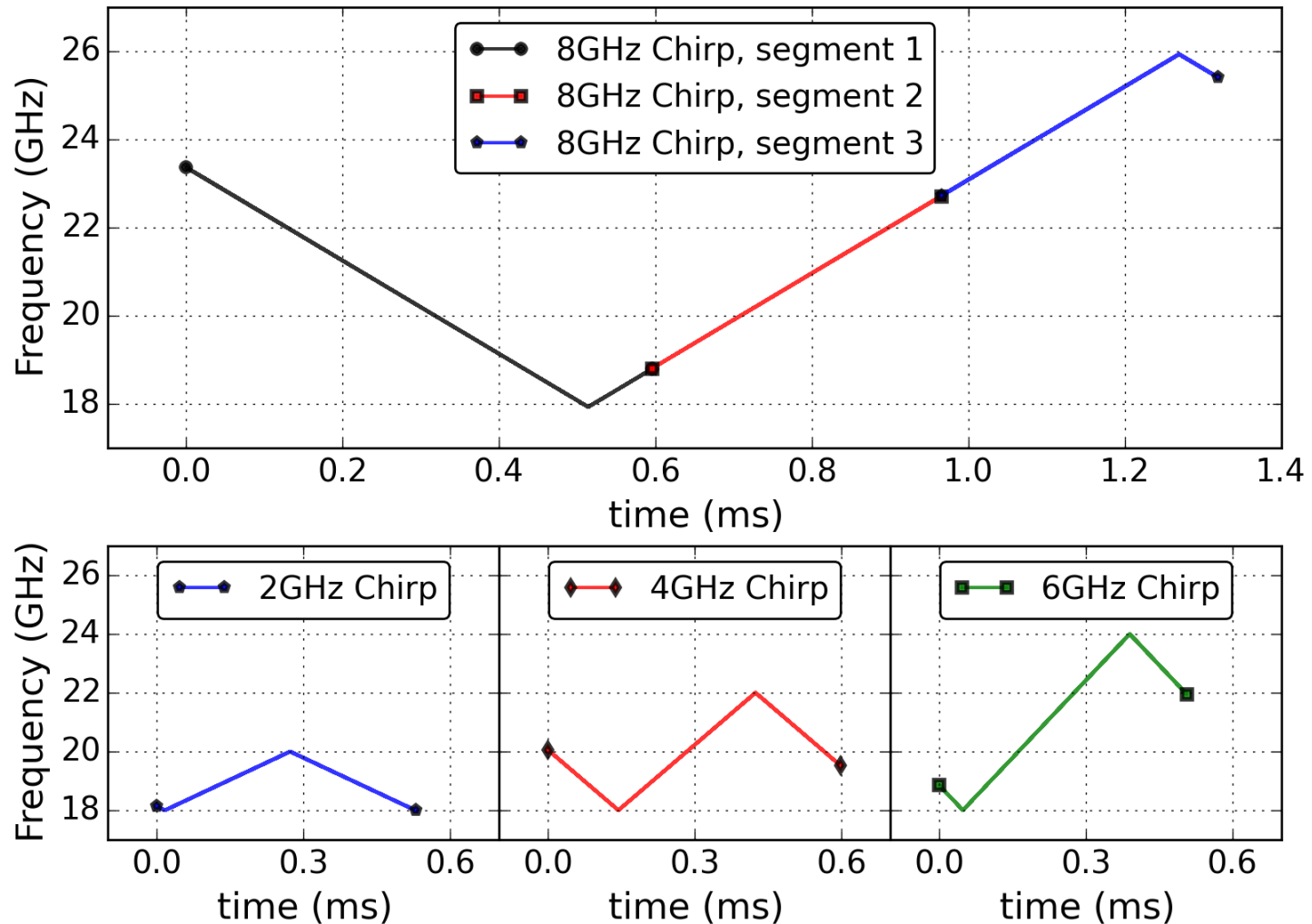
M. Ferriss et al, ISSCC16

Measured phase noise at 22GHz



VCO's FOM = 181dBc/Hz, FOMT = 188dBc/Hz @10MHz offset

Measured transient frequency

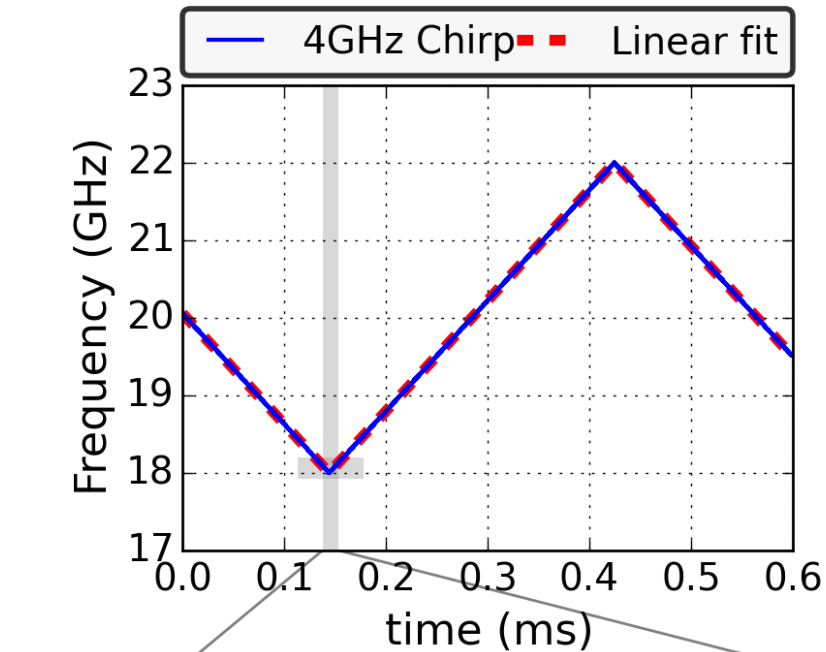


An 80GHz oscilloscope directly samples PLLs output.

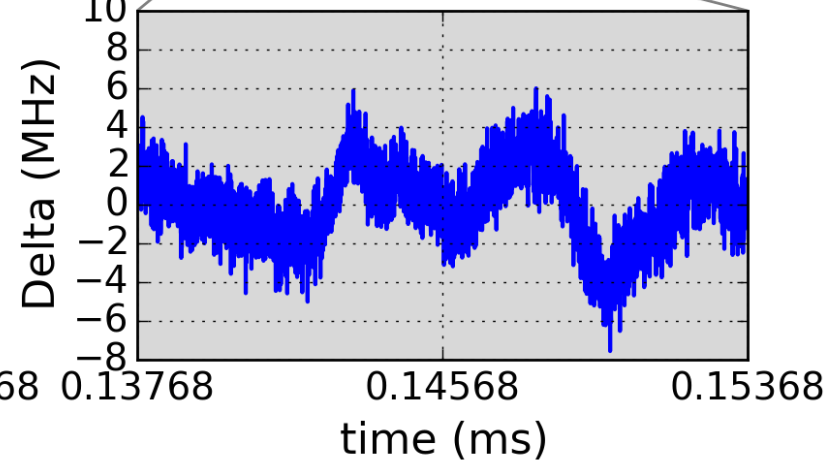
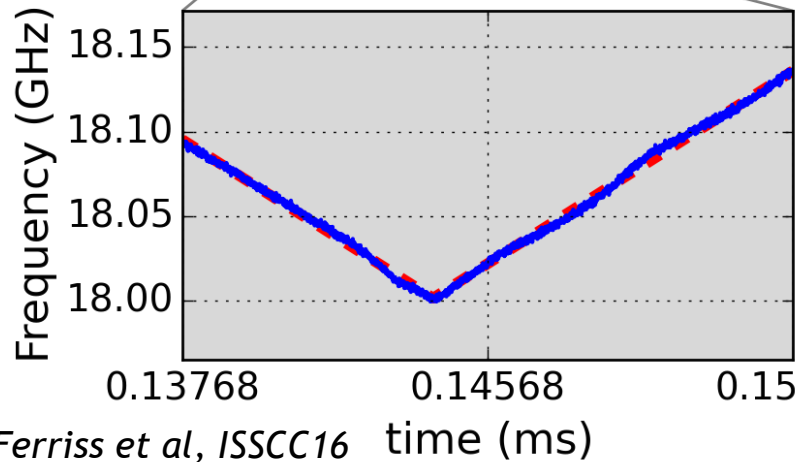
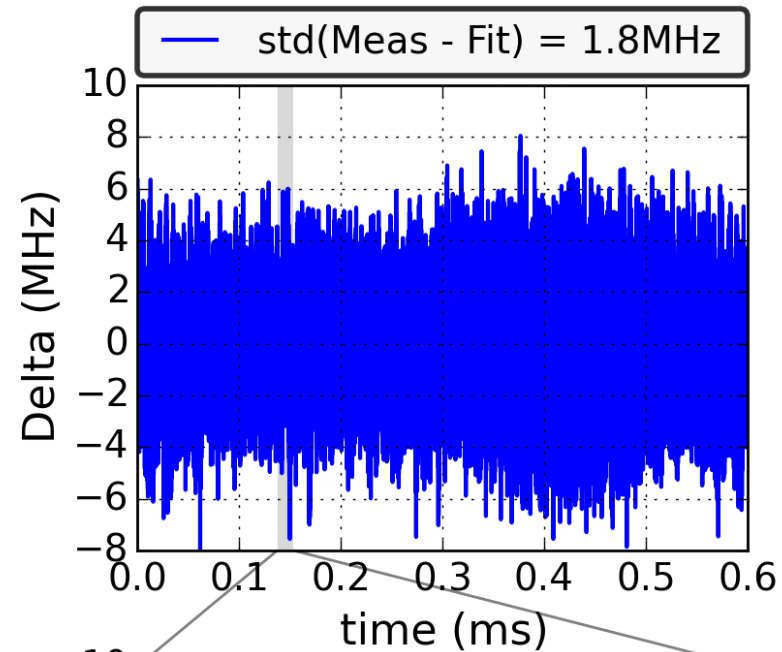
The 8GHz chirp was measured in segments due to scope memory limitations.

Chirp frequency errors

Measured Frequency



Frequency Error



M. Ferriss et al, ISSCC16

Conclusion: Frac-N Hybrid PLL with Coarse Band Elimination

Key results

- Can support wide-range designs within integral path loop
- Linearization enhancement demonstrated
- Features of previous versions maintained

Outline

- Introduction and motivation: hybrid architectures
- Initial implementation: proof-of-concept
- Flexible synthesizer: frac-N w/ noise cancellation
- Flexible synthesizer: coarse band elimination
- **Flexible synthesizer: initial thoughts on flicker noise suppression**
- Summary/conclusion

Hybrid PLL and upconversion noise suppression

Recent Advances in CMOS oscillator flicker noise suppression

Strategy: Add phase shift to VCO loop [Pepe, et al., JSSC 2013]

- ✓ Simple implementation.
- × Magnitude of phase shift depends on absolute component values.

Strategy: Add tank resonance modes at second / third harmonics. [Shahmohammadi, et al., JSSC 2016]

- ✓ Dramatic improvement in phase noise.
- × Depends on component matching / difficult to precisely model impedances at very high harmonic frequencies

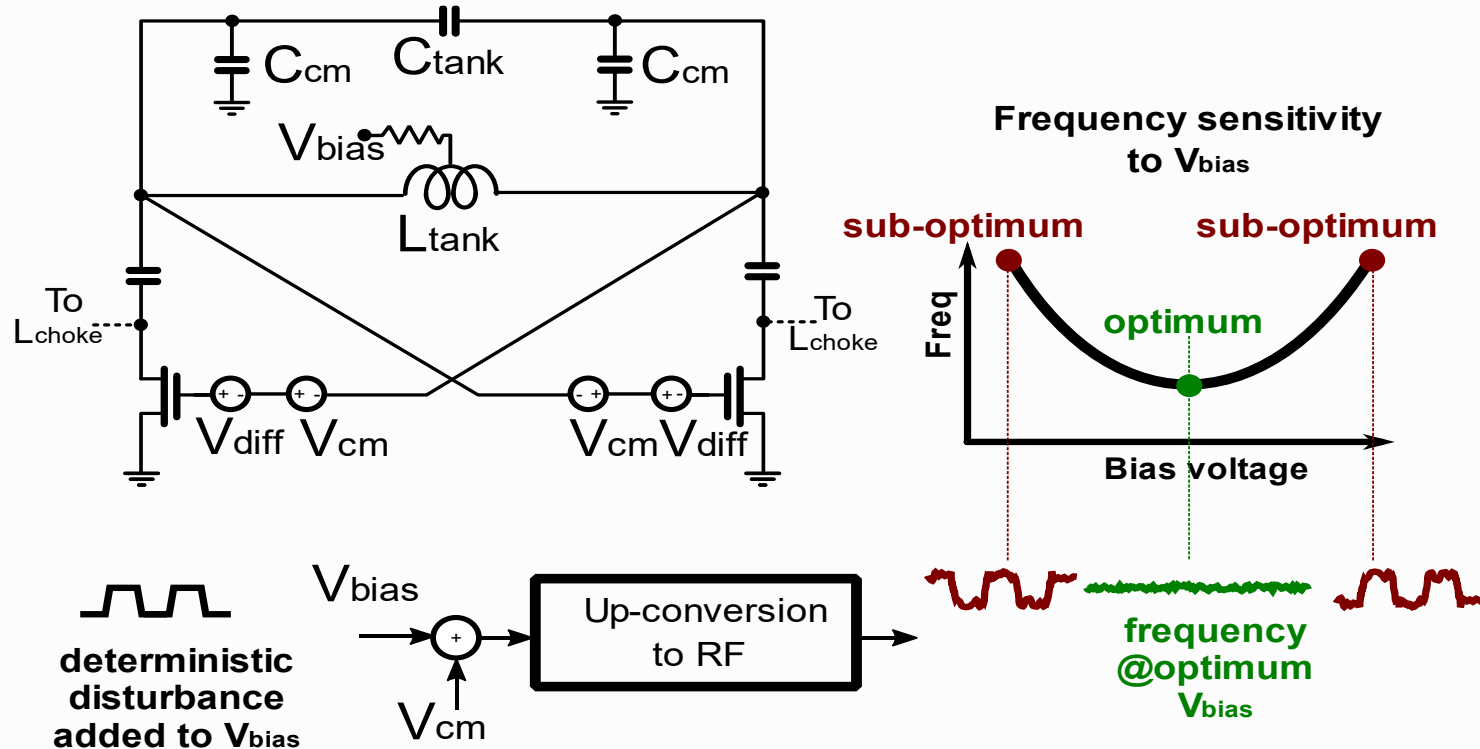
Opportunity: suppression of up-conversion mechanisms in a closed loop

An optimizing scheme is proposed that:

- Suppresses VCO upconverted noise
- Does not rely on absolute values of components
- Does not require accurate control of higher order resonance modes

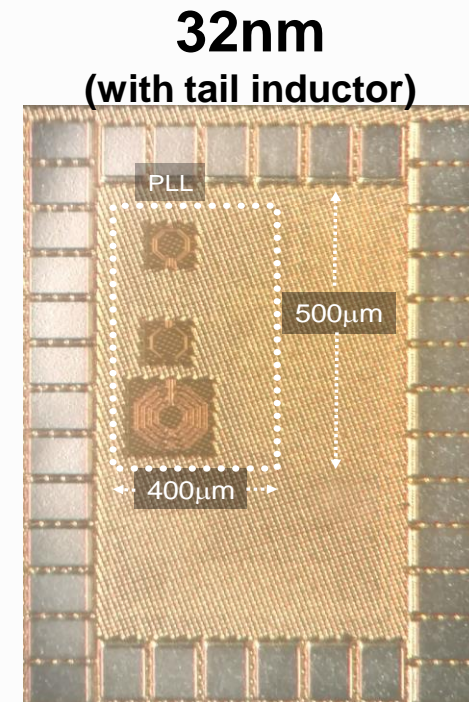
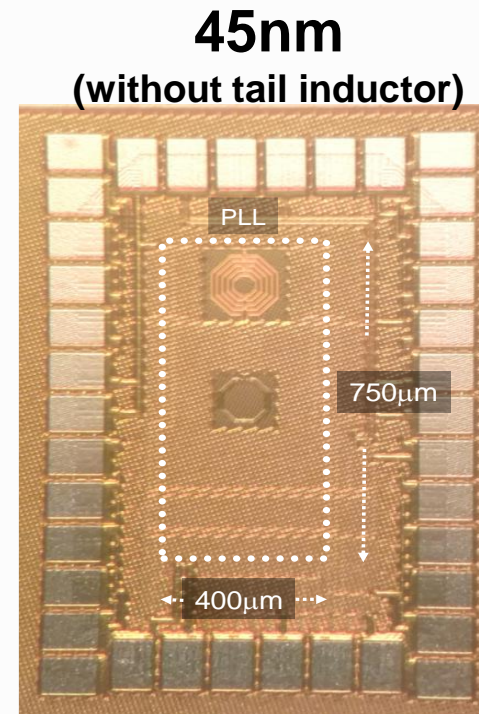
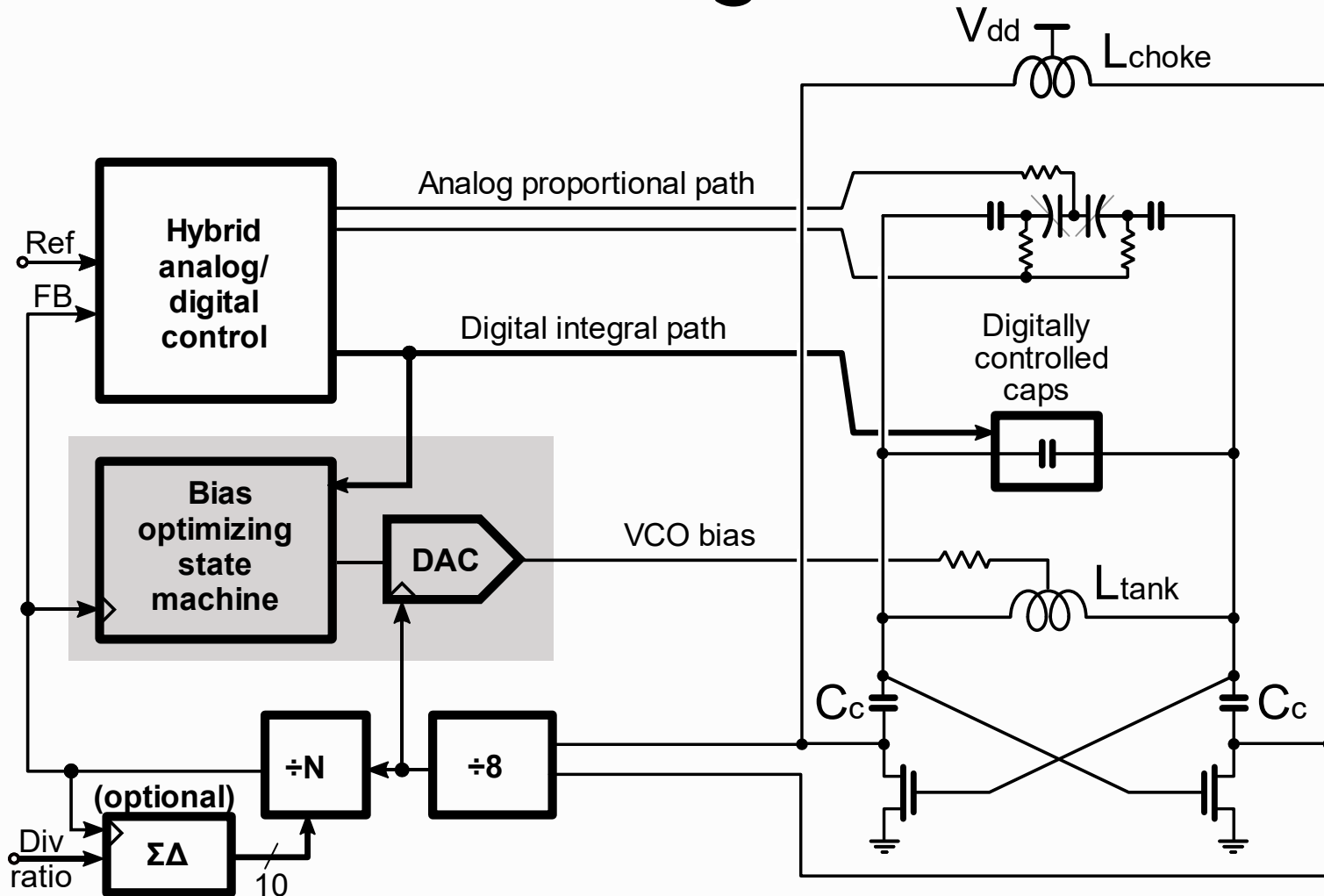
M. Ferriss et al, RFIC 2018

Noise and bias up-conversion gain



Same up-conversion mechanism for V_{cm} and V_{bias}
Minimizing bias-to-frequency gain minimizes noise up conversion

Design and Architecture

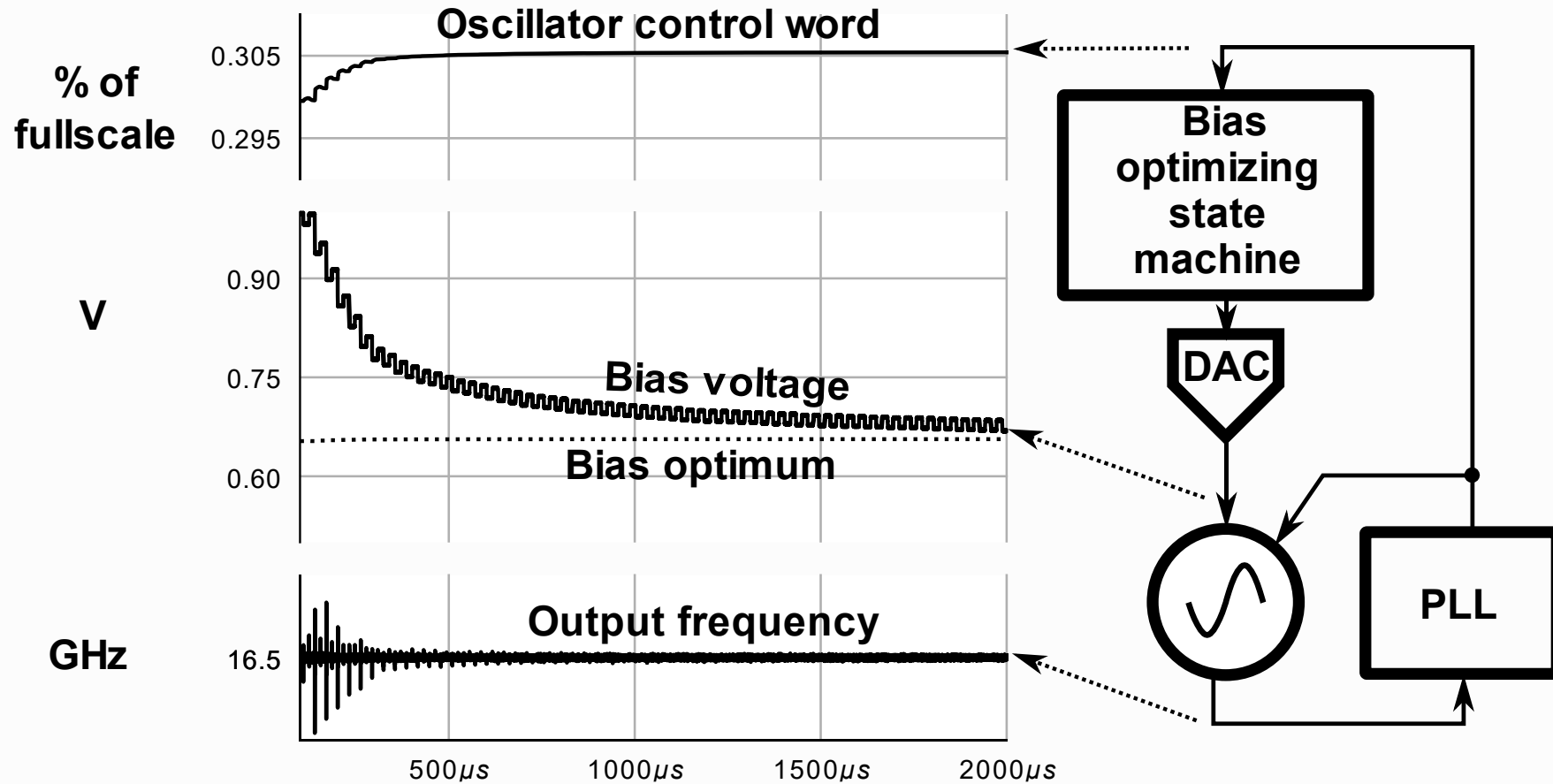


Hybrid PLL's bias optimizing state machine

Monitors digital control word for frequency

Actuates on bias point of transconducting transistors in VCO

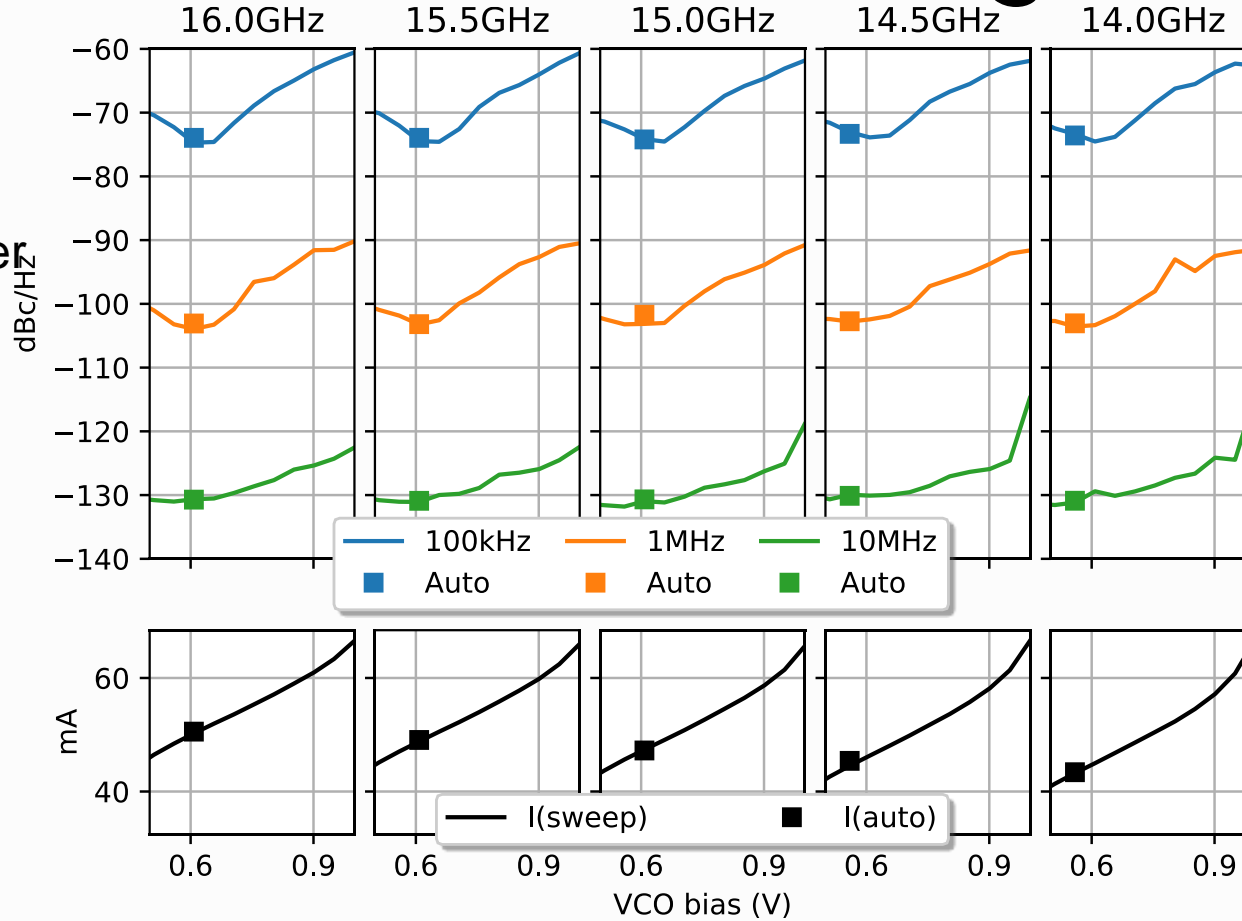
Behavioral sim shows the optimizer converging



Disturbance is added to bias voltage and detected on oscillator control word
As bias approaches optimum, frequency disturbance disappears

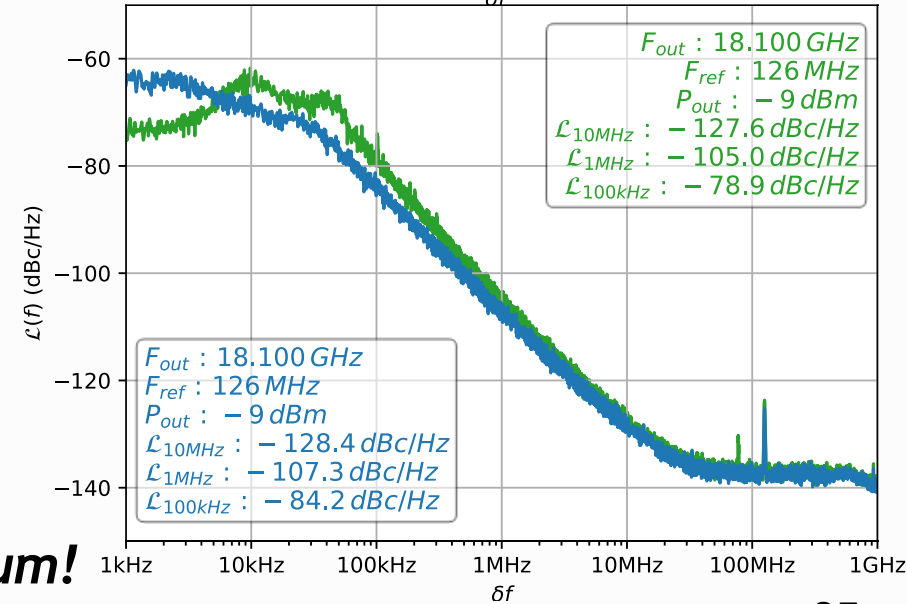
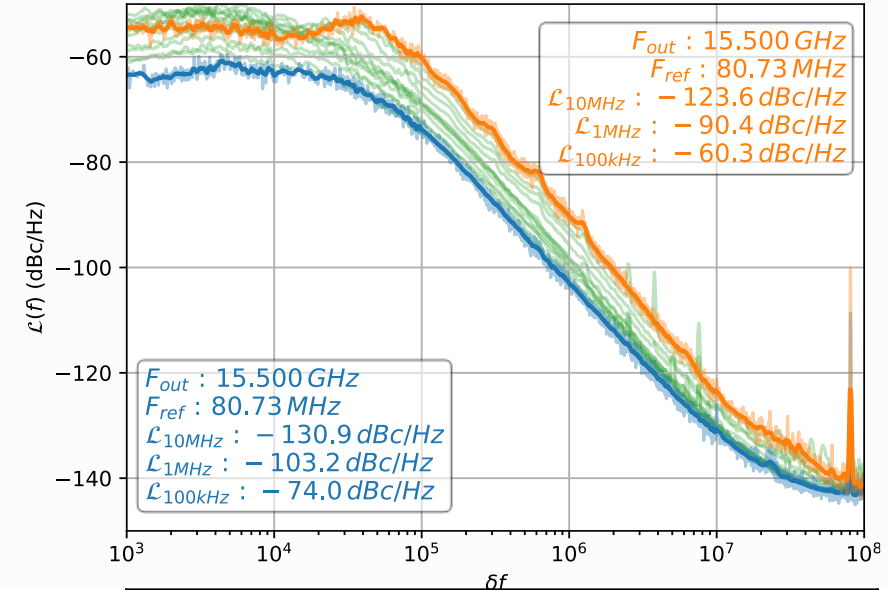
Phase noise versus bias voltage

Squares (■) →
with optimizer
Solid lines →
without optimizer



Result:
True closed loop system; no external calibration.
Prototypes in two different technologies: 45nm and 32nm

The VCO topology enables phase noise optimization, and
the optimization state-machine finds that phase noise minimum!



Outline

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- Flexible synthesizer: coarse band elimination
- Flexible synthesizer: flicker noise suppression exploration
- **Summary/conclusion**

Summary: Flexible Synthesizer Features Achieved Using Hybrid PLL Approach

Characteristic	Objectives	Implementation Approach
Tuning range 2-26GHz	Continuous tuning range to maximum frequency	Wide-range dual linearized transconductance VCO complex
Loop transfer function control	High programmability over wide range through digital control	Leverage highly digital architecture of dual-path HPLL
Supported reference rate	Flexible without sacrificing performance	Fractional-N synthesis
Fractional-N quantization noise	Active noise cancellation scheme that does not limit bandwidth	Proportional & integral path highly digital cancellation architecture
Area	Less than 1 mm ² total	Single PLL with wide-range dual VCO complex
Fast frequency hopping	Fast settling time based on digital memory	Leverage digital memory/parameter replay
Spurious content	Minimize to enable broader use model	Reduced by utilization of digital/predictive techniques
Extended range in main loop	Eliminate need for coarse bands in supporting wide tuning range	Enhance and extend digital integral path approach to include full VCO range
Flicker noise suppression	Reduce low offset noise in CMOS PLLs	Closed-loop algorithm acting on noise proxy; <i>more research required!</i>

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- Technical contributors and management support
 - Mark Ferriss
 - Bodhisatwa Sadhu
 - Alexander Rylyakov
 - Jose Tierno
 - Herschel Ainspan
 - Alberto Valdes Garcia
 - Daniel Friedman
 - Mehmet Soyuer

References

- [1] W. Yin, R. Inti, A. Elshazly, B. Young, P. Hanumolu, "A 0.7-to-3.5 GHz 0.6-to-2.8 mW Highly Digital Phase-Locked Loop With Bandwidth Tracking", *IEEE JSSC* Vol. 46, No. 8, August, 2011, pp. 1870-1880.
- [2] M. Ferriss, A. Rylyakov, H. Ainspan, J. Tierno and D. Friedman, "A 28GHz hybrid PLL in 32nm SOI CMOS," *2013 Symposium on VLSI Circuits*, Kyoto, 2013, pp. C198-C199.
- [3] A. Rylyakov, J. Tierno, H. Ainspan, J. O. Plouchart, J. Bulzacchelli, Z. T. Deniz, and D. Friedman, *ISSCC Dig. Tech. Papers*, pp. 94-95, Feb. 2009.
- [4] N. Da Dalt, *IEEE Trans. Circuits Syst. II*, vol. 53, no. 11, pp. 1195-1199, Nov. 2006.
- [5] M.Z. Straayer and M.H. Perrott, *IEEE JSSC*, vol. 43, no. 4, pp. 805-814, Apr. 2008.
- [6] J. Zhuang, Q. Du and T. Kwasniewski, *CICC Dig. Tech, Papers*, pp. 543-546, 2007.
- [7] M. Ferriss et al "A 28GHz Hybrid PLL in 32nm SOI CMOS," *JSSC*, vol. 49, pp. 1027 - 1035 Dec. 2014.
- [8] D. Tasca, et al, "A 2.9-4.0-GHz Fractional-N Digital PLL With Bang-Bang Phase Detector and 560- Integrated Jitter at 4.5-mW Power," *JSSC*, vol. 46, pp. 2745 - 2758, Dec. 2011.

References

- [9] A. Swaminathan, et al, “A Wide-Bandwidth 2.4 GHz ISM Band Fractional-N PLL with Adaptive Phase Noise Cancellation,” JSSC, vol. 42, pp. 2639 - 2650, Dec. 2007.
- [10] M. Ferriss et al., “10.9 A 13.1-to-28GHz fractional-N PLL in 32nm SOI CMOS with a $\Delta\Sigma$ noise-cancellation scheme,” ISSCC Dig. Tech. Papers, Feb. 2015.
- [11] B. Sadhu et al., “A linearized, low-phase-noise VCO-based 25-GHz PLL with autonomic biasing,” IEEE J. Solid-State Circuits, vol. 48, no. 5, May 2013.
- [12] P. Wang et al., “A Digital Intensive Fractional-N PLL and All-Digital Self-Calibration Schemes,” IEEE J. Solid-State Circuits, vol. 44, no. 8, Aug. 2009.
- [13] T. Mitomo et al., “A 77 GHz 90 nm CMOS Transceiver for FMCW Radar Applications,” IEEE J. Solid-State Circuits, vol. 45, no. 4, Apr. 2010.
- [14] A. Rylyakov, J. Tierno, H. Ainspan, J. O. Plouchart, J. Bulzacchelli, Z. T. Deniz, and D. Friedman, “Bang-bang digital PLLs at 11 and 20 GHz with sub-200fs integrated jitter for high-speed serial communication applications,” in IEEE ISSCC Dig. Tech. Papers, Feb. 2009, pp. 94-95.
- [15] R. He, C. Liu, X. Yu, W. Rhee, J.-Y. Park, C. Kim, Z. Wang, “A low-cost, leakage-insensitive semi-digital PLL with linear phase detection and FIR-embedded digital frequency acquisition,” *2010 IEEE Asian Solid-State Circuits Conference*, Beijing

References

- [16] Y. Sun, Z. Zhang, N. Xu, M. Wang, W. Rhee, T.-Y. Oh, Z. Wang, "A 1.75 mW 1.1 GHz Semi-Digital Fractional-N PLL With TDC-Less Hybrid Loop Control," in IEEE Microwave and Wireless Components Letters, vol. 22, no. 12, pp. 654-656, Dec. 2012.
- [17] N. Xu, W. Rhee and Z. Wang, "A Hybrid Loop Two-Point Modulator Without DCO Nonlinearity Calibration by Utilizing 1 Bit High-Pass Modulation," in IEEE Journal of Solid-State Circuits, vol. 49, no. 10, pp. 2172-2186, Oct. 2014.
- [18] N. Da Dalt, "Markov chains based derivation of the phase detector gain in bang-bang PLLs," IEEE Trans. Circuits Syst. II , vol. 53, no. 11, pp. 1195-1199, Nov. 2006.
- [19] M.Z. Straayer and M.H. Perrott, "A 12-bit 10 MHz bandwidth, continuous-time delta-sigma ADC with a 5-bit, 950-MS/s VCO-based quantizer," IEEE J. Solid-State Circuits, vol. 43, no. 4, pp. 805-814, 2008.
- [20] R. Beards and M. Copeland, "An oversampling delta-sigma frequency discriminator," IEEE Trans. Circuits Syst. II , vol. 41, no. 1, pp. 26-32, Jan. 1994.
- [21] C. Venerus and I. Galton, "Delta -Sigma FDC based fractional-PLLs," IEEE Trans. Circuits Syst. I, vol. 60, no. 5, pp. 1274-1285, May 2013.
- [22] M. Lee and A. Abidi, "A 9 b, 1.25 ps resolution coarse-fine time-to-digital converter in 90 nm CMOS that amplifies a time residue," IEEE J. Solid-State Circuits, vol. 43, no. 4, pp. 769-777, Apr. 2008.

References

- [23] V. Kratyuk, P. Hanumolu, K. O, ,U.-K. Moon, and K. Mayaram, “A digital PLL with a stochastic time-to-digital converter,” *IEEE Trans. Circuits Syst. I*, vol. 56, no. 8, pp. 1612-1621, Aug. 2009.
- [24] M. Perrott, Y. Huang, R. Baird, B. Garlepp, D. Pastorello, E. King, Q. Yu, D. Kasha, P. Steiner, L. Zhang, J. Hein, and B .delSignore, “A 2.5-Gb/s multi-rate 0.25- μ m CMOS clock and data recovery circuit utilizing a hybrid analog/digital loop filter and all-digital referenceless frequency acquisition,” *IEEE J. Solid-State Circuits*, vol. 41, no. 12, pp. 2930-2944, Dec. 2006.
- [25] A. Sai, T. Yamaji, and T. Itakura, “A 570 fs rms integrated-jitter ring-VCO-based 1.21 GHz PLL with hybrid loop,” in *IEEE ISSCC Dig. Tech. Papers* , Feb. 2011, pp. 98-100.
- [26] J. A. Tierno, A. V. Rylyakov, and D. J. Friedman, “A wide power supply range, wide tuning range, all static CMOS all digital PLL in 65 nm SOI,” *IEEE J. Solid-State Circuits* , vol. 43, no. 1, pp. 42-51, Jan. 2008.
- [27] M. Ferriss, J. O. Plouchart, A. Natarajan, A. Rylyakov, B. Parker, J. Tierno, A. Babakhani, S. Yaldiz, A. Valdes-Garcia, B. Sadhu, and D. Friedman, “An integral path self-calibration scheme for a dual-loop PLL,” *IEEE J. Solid-State Circuits* , vol. 48, no. 4, pp. 996-1008, Apr. 2013.
- [28] Z. Ru, P. Geraedts, E. Klumperink, X. He, and B. Nauta, “A 12 GHz 210 fs 6 mW digital PLL with sub-sampling binary phase detector and voltage-time modulated DCO,” in *Symp. VLSI Circuits*, Jun.2013.
- [29] M. Ferriss, B. Sadhu and D. Friedman, "A Gradient Descent Bias Optimizer for Oscillator Phase Noise Reduction Demonstrated in 45nm and 32nm SOI CMOS," 2018 IEEE Radio Frequency Integrated Circuits Symposium (RFIC), Philadelphia, PA, 2018, pp. 344-347